# **FINAL REPORT**

# LARGE SCALE AND LIVE BED LOCAL PIER SCOUR EXPERIMENTS PHASE 2 LIVE BED EXPERIMENTS

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#### LIVE BED EXPERIMENTS

#### Introduction

The accurate prediction of sediment scour depths near bridge piers under design storm conditions is very important in bridge design. Under-prediction can result in costly bridge failure and possibly the loss of lives, while over-prediction can result in millions of dollars wasted on the construction of a single bridge. The physical processes involved are very complex and difficult to analyze, and thus most design scour depth predictive equations are based on laboratory scale experimental results. An ongoing bridge scour research program at the University of Florida is directed at increasing the understanding of scour processes and improving the accuracy of design scour depth predictions. Equations for predicting local scour depths were developed by the author early in this program. Additional data was needed to extend/verify these equations. Experiments to obtain this data were divided into two phases, 1) the large structure, clearwater scour phase and 2) the high velocity, live bed scour phase. The Phase 1 experiments were conducted by the author in the Hydraulics Laboratory at the Conte USGS-BRD Laboratory in Turners Falls, Massachusetts. The Phase 2 experiments were conducted by the author in the Hydraulics Laboratory at the University of Auckland in Auckland, New Zealand. Phase 1 has been completed and a technical paper on the results accepted for publication in the ASCE Journal of Hydraulic Engineering. A more complete description of this work can be found in a University of Florida Coastal Engineering Technical Report [Sheppard et al. (2002)]. Phase 2 of this work is the topic of this report.

#### **Research Objectives**

The research described in this report is part of a larger local sediment scour research effort being conducted by the author with funding from the Florida Department of Transportation. Early in this program predictive equations for local scour at single structures in cohesionless sediments were developed based on laboratory data obtained by the author at the University of Florida and data obtained by other researchers. Since the range of conditions (structure size, sediment size, flow velocity, etc.) used in the development of these equations was somewhat limited, additional data was needed to extend/verify the equations. To the knowledge of the author no single flume exists with

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the capability of producing all of the conditions needed to verify the equations. That is, no existing flume can test large, prototype size structures, produce high velocity flows and recirculate the sediment. For this reason a research plan consisting of two phases was proposed. The first phase was directed at the geometric scale issues (i.e. the size of the structures tested) and relatively low velocity, clearwater scour conditions. The maximum size structure that can be tested is a function of the width of the flume (the structure width should not exceed ~15% of the flume width). The Hydraulics Laboratory at the USGS-BRD Laboratory in Turners Falls, Massachusetts has a large (20 ft wide, 21 ft deep, 126 ft long) flow-through type flume that is used for fisheries research. A cooperative agreement was established between the University of Florida and the Conte USGS-BRD Laboratory to conduct clearwater local scour experiments with three different circular piles ranging in size from 4.5 inches to 36 inches in diameter. Three sediment sizes were used in the tests ( $D_{50} = 0.22 \text{ mm}$ , 0.8 mm and 2.9 mm) and a range of water depths and flow velocities. These tests achieved their objectives by providing data at large structure to sediment size ratios for a range of clearwater flow conditions.

Phase 2 of this research, which is the subject of this report, had three primary objectives: 1) to provide live bed scour data at larger structures, 2) to investigate the existence of a maximum (limiting) value of normalized local scour depth with increasing depth-averaged velocity and 3) if such a maximum exists, investigate the conditions under which the maximum occurs (at least for the range of conditions examined).

A survey of flumes in the United States and abroad that are capable of recirculating sediment and producing high velocity flows in the live bed scour range indicated that a flume in the Hydraulics Laboratory at the University of Auckland (UA) in Auckland, New Zealand was the most appropriate for the Phase 2 work. Arrangements were made for the author to conduct live bed scour experiments in this flume with the assistance of UA graduate students over a four month period (January-April) in 2002. This report presents a description of the facilities, instrumentation, and procedures used and the test results.

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#### **Facilities and Instrumentation**

## Facilities

All of the tests were conducted in a 5 ft wide, 4 ft deep, 148 ft long, tilting flume, located in the Hydraulics Laboratory at the University of Auckland in Auckland, New Zealand. The flume has a maximum tilt of 1%. It has two pumps for recirculating the water with a combined capacity of 42 cfs and a sediment pump with adequate capacity. The bed load sediment (sediment moving along the bottom) is trapped and is pumped to the flume entrance with the sediment pump. Suspended sediment is pumped with the water to the entrance with either or both of the water pumps. A photograph of the building in which the flume is located is shown in Figures 1. Photographs of the flume are shown in Figures 2-5. A schematic drawing of the flume is presented in Figure 5.



Figure 1. University of Auckland Engineering Building where the Hydraulics Laboratory and the flume used for the live bed scour experiments is located.



Figure 2. Side and top views of the 5 ft wide, 4 ft deep, 148 ft long flume used for the local scour tests





Figure 3 Water (left picture) and sediment (right picture) return entrance sections.



Figure 4 Data acquisition computers (left) and test pile installation (right).



Figure 5. Schematic drawing of the flume used for this research.

## Instrumentation

The instrumentation used in this research can be divided into two categories: 1) that which measures the flow parameters, and 2) that which measures scour depth. The flow parameters monitored were flow discharge (indirectly), velocity at specific locations, water depth, and temperature. The scour hole depth was monitored with internal video cameras and with arrays of acoustic transponders. The bed and water elevations at the walls of the flume were monitored with externally mounted cameras for some of the live bed tests.

Prior to starting the tests numerous vertical velocity profiles were measured and integrated to determine the flow discharge as a function of pump RPM (which can be precisely controlled). The velocity measurements were made with an acoustic Doppler velocimeter. During the tests the sectionally averaged velocity was estimated from the pump RPMs and the water depth at the section. Water temperature was measured with a glass thermometer. The water depth at the test section was measured using scales attached to the glass walls of the flume. A schematic drawing of the scour depth measuring instruments is presented in Figure 6. The 6 in diameter test cylinder with the scour depth instrumentation is shown in Figure 7. A photograph of the internal cameras and carriage is given in Figure 8 and a diagram of the external video cameras is shown in Figure 9. The external cameras were used to monitor the position of the bed on both sides of the flume during the live bed tests.



Test Piles with Scour Depth Instrumentation

Figure 6. Schematic drawing of the local scour depth measuring instruments.



Figure 7. Photograph of the internal video cameras traversing mechanism and the acoustic transponders used to measure scour depth.



Figure 8. Internal video cameras and housing for the 6 in. diameter test cylinder.



Flume Cross-Section

Figure 9. Cross-section of flume showing location of external video cameras used for monitoring the bed elevation during the live bed tests.

Three arrays of acoustic transponders were attached to the cylinder just below the water surface. Each array contained four crystals, which produced a 1 in. diameter acoustic

beam at the transducer. The spread angle of the beam was approximately 1.5 degrees. The footprint of the beam (area of the acoustic beam at the bed) varied with the water and scour hole depths. The time required for the acoustic pulse to travel to the bed and return to the transponder was measured and the distance from the transponder to the bed computed based on the speed of sound in water at that temperature. This system provided scour hole depth measurements at the 12 locations along three radial lines throughout the experiments.

For some of the tests an array of 22 acoustic transponders was used to measure the bedforms that propagated down the flume. A photograph of the array is shown in Figures 10 and 11. Personal computers were used to both control the instrumentation and to record the data.



Figure 10. Array of acoustic transducers used to measure bed forms (prior to installing drag reduction hydrofoils).





# **Experimental Procedure**

A summary of the experimental procedure used in performing the local sediment scour experiments is outlined below. The procedure is divided into the tasks performed before, during and after the experimental run.

## Pre-experiment

- 1. Compact and level the bed in the flume.
- 2. Fill the flume slowly and allow to stand until the air trapped in the sediment has escaped.
- 3. Take pre-experiment photographs.
- 4. Check all instrumentation.

# During experiment

- 1. Measure the scour depth as a function of time with acoustic transponders and video cameras.
- 2. Measure the velocity, water depth, and temperature.
- 3. Monitor bed elevation at flume walls in test section with external video cameras.
- 4. Monitor bed forms during live bed tests.

## Post-experiment

- 1. Take post-experiment photographs.
- 2. Observe and note bed condition throughout the flume (presence of bed forms, etc.)
- 3. Survey the scour hole with a point gauge.
- 4. Reduce and analyze the data.

## **Results and Conclusions**

# Results

A significant quantity of local sediment scour data and bedform information were gathered during this research program. Even though most of the tests were performed in the live bed scour range a few tests were conducted in the clearwater scour range to fill in gaps in the existing data set. The structure, sediment and flow conditions under which the tests were conducted are summarized in Table 1. The scour results are given in Table 2. The experiments conducted as part of this work were relatively long in duration (for live bed scour tests) and thus the scour depths were near equilibrium at the end of the test. Two different sediment sizes were used, one with a  $D_{50} = 0.27$  mm (and  $\sigma = 1.33$ ) and one with a  $D_{50} = 0.84$  mm (and  $\sigma = 1.32$ ). Photographs of the test pile during some of the higher velocity live bed scour tests are shown in Figures 12 and 13.



Figure 12. Flow around test pile during a live bed test viewed from upstream.



Figure 13. Flow around test pile during a live bed test viewed from down stream.

Before and after photographs of a live bed scour test are shown in Figures 14 and 15. Typical bed forms that occur during the live bed tests are shown in Figures 15-17.



Figure 14. Photograph of test pile prior to live bed scour test taken through the water from outside the flume.



Figure 15. Scour hole after live bed scour test with large bedforms.



Figure 16. Bed forms at the end of a live bed scour test. Flow was from right to left.



Figure 17. Downstream edge of a bedform during a live bed test.

		Sediment		Flow		Computed Parameters				
Test	Structure Diameter D (ft)	D <sub>50</sub> (mm)	σ	Water Depth	Velocity	Sediment	Live Bed			
						Critical	Peak	6	<b>.</b>	D /D
				$y_0$ (ft)		Velocity	Velocity	$y_0/D$	$V/V_c$	$D/D_{50}$
					(ft/s)	$V_c$	$V_{lp}$			
1	0.50	0.27		1.38	0.56	0.89	5.28	2.72	0.62	564.4
2	0.50	0.27		1.38	2 03	0.92	5.31	2 76	2 23	564 4
-	0.50	0.27		1.00	2.80	0.02	5 35	2 70	3.2	564.4
3	0.50	0.27		1.71	2.03	0.92	5.00	2.73	2.00	504.4
4	0.50	0.27		1.31	3.01	0.89	5.18	2.02	3.99	504.4
5A	0.50	0.27		1.31	4.13	0.89	5.18	2.62	4.59	564.4
5B	0.50	0.27		1.31	4.69	0.89	5.18	2.62	5.23	564.4
6	0.50	0.27		1.31	5.38	0.89	5.18	2.62	5.99	564.4
7A	0.50	0.27		0.66	1.80	0.82	4.03	1.31	2.18	564.4
7B	0.50	0.27		0.66	2.36	0.82	4.03	1.31	2.86	564.4
8	0.50	0.27		1.41	2.26	0.92	5.35	2.79	2.49	564.4
9	0.50	0.27		1.61	0.82	0.92	5.74	3.2	0.88	564.4
10	0.50	0.84		1.41	1.21	1.34	6.82	2.79	0.89	181.4
11	0.50	0.84		1.25	1.90	1.34	6.76	2.49	1.42	181.4
12	0.50	0.84		1.25	2.43	1.34	6.76	2.49	1.81	181.4
13	0.50	0.84		1.25	3.44	1.34	6.76	2.49	2.57	181.4
14	0.50	0.84		1.25	3.97	1.34	6.72	2.49	2.97	181.4
15	0.50	0.84		1.25	4.49	1.34	6.76	2.49	3.36	181.4
16	0.50	0.84		1.25	4.99	1.34	6.76	2.49	3.72	181.4
17	0.50	0.84		0.98	4.99	1.31	6.53	1.97	3.85	181.4
18	0.50	0.84		0.98	5.77	1.31	6.53	1.97	4.45	181.4
19	0.50	0.84		0.98	6.07	1.31	6.53	1.97	4.68	181.4
20	0.50	0.84		0.98	6.53	1.31	6.53	1.97	5.03	181.4
21	0.50	0.84		0.98	7.08	1.31	6.53	1.97	5.46	181.4
22	0.50	0.84		1.41	0.82	1.34	6.76	2.79	0.61	181.4

Table 1. Flow, sediment and structure parameters for tests.

					Equilibrium
	Scour				Scour
Test	Regime	<b>y</b> <sub>0</sub> / <b>D</b>	V/V <sub>c</sub>	D/D <sub>50</sub>	Depth
	itegine				<b>y</b> se
					(ft)
1	Clearwater	2.72	0.62	564.4	0.42
2	Live Bed	2.76	2.23	564.4	0.71
3	Live Bed	2.79	3.2	564.4	0.75
4	Live Bed	2.62	3.99	564.4	0.82
5A	Live Bed	2.62	4.59	564.4	0.89
5B	Live Bed	2.62	5.23	564.4	0.87
6	Live Bed	2.62	5.99	564.4	0.98
7A	Live Bed	1.31	2.18	564.4	0.59
7B	Live Bed	1.31	2.86	564.4	0.71
8	Live Bed	2.79	2.49	564.4	0.72
9	Clearwater	3.2	0.88	564.4	0.50
10	Clearwater	2.79	0.89	181.4	0.85
11	Live Bed	2.49	1.42	181.4	0.56
12	Live Bed	2.49	1.81	181.4	0.83
13	Live Bed	2.49	2.57	181.4	0.82
14	Live Bed	2.49	2.97	181.4	0.75
15	Live Bed	2.49	3.36	181.4	0.82
16	Live Bed	2.49	3.72	181.4	0.85
17	Live Bed	1.97	3.85	181.4	0.85
18	Live Bed	1.97	4.45	181.4	0.86
19	Live Bed	1.97	4.68	181.4	0.87
20	Live Bed	1.97	5.03	181.4	0.92
21	Live Bed	1.97	5.46	181.4	0.97
22	Clearwater	2.79	0.61	181.4	0.64

Table 2. Scour depth results.

There are a number of ways to present the data from the tests conducted as part of this study and to evaluate the scour prediction equations. Perhaps the best way is to plot normalized scour depth,  $y_{se}/D$ , versus normalized velocity,  $V/V_c$  for approximately constant values of  $y_0/D$  and  $D_{50}/D$ . All of the clearwater and live bed data from the New Zealand tests are presented in Figures 18-20. The scour prediction curves were evaluated and plotted along with the CSU equation presented in HEC-18 for the conditions of the experiments. These results are discussed in the conclusions section of this report.



 $y_s/D vs V/V_c$ ,  $D/D_{50} = 181$ ,  $y_0/D = 2$ 

Figure 18. Normalized equilibrium scour depth versus normalized velocity for five of the New Zealand tests. Scour depth predictions using Sheppard's Equations and the CSU Equation are also shown.



Figure 19. Normalized equilibrium scour depth versus normalized velocity for eight of the New Zealand tests. Scour depth predictions using Sheppard's Equations and the CSU Equation are also shown.





Figure 20. Normalized equilibrium scour depth versus normalized velocity for two of the New Zealand tests. Scour depth predictions using Sheppard's Equations and the CSU Equation are also shown.

#### **Conclusions**

The objectives of the project were achieved. A number of clearwater and live bed scour tests were successfully conducted and Sheppard's predictive equations verified in the live bed scour range (covered by the experiments). Even though it was not a direct component of the scope of work for this project, sediment bed form data was also obtained for a range of flow conditions. When analyzed the bed form data will be useful in improving the accuracy of design scour depth predictions for bridge foundations and other structures.

One of the main objectives of this work was to provide data for testing/verifying Sheppard's single structure, scour depth prediction equations in both the clearwater and live bed scour ranges. Minor adjustments to the equations were made as a result of the data obtained in this study. The adjustments were, however, in the clearwater scour range as opposed to the higher velocity, live bed scour range which was the main thrust of this work. The resulting single structure equilibrium scour depth prediction equations are presented below:

Clearwater Scour  $0.47 \le \frac{V}{V_c} \le 1.0$ 

$$\frac{d_{se}}{D} = K_{s} 2.5 \left\{ tanh \left[ \left( \frac{y_{0}}{D} \right)^{0.4} \right] \right\} \left\{ 1 - 1.75 \left[ ln \left( \frac{V}{V_{c}} \right) \right]^{2} \right\} \left\{ \frac{D/D_{50}}{0.4 \left( D/D_{50} \right)^{1.2} + 10.6 \left( D/D_{50} \right)^{-0.13}} \right\}$$

Live Bed Scour  $1.0 \le \frac{V}{V_c} \le \frac{V_{lp}}{V_c}$ 

$$1.0 \le \overline{V_c} \le \overline{V_c}$$

$$\frac{\mathbf{d}_{se}}{\mathbf{D}} = \mathbf{K}_{s} \mathbf{f}_{1} \left( \frac{\mathbf{y}_{0}}{\mathbf{D}} \right) \left[ 2.2 \left( \frac{\mathbf{V} - \mathbf{V}_{c}}{\mathbf{V}_{lbp} - \mathbf{V}_{c}} \right) + 2.5 \mathbf{f}_{3} \left( \frac{\mathbf{D}}{\mathbf{D}_{50}} \right) \left( \frac{\mathbf{V}_{lbp} - \mathbf{V}}{\mathbf{V}_{lbp} - \mathbf{V}_{c}} \right) \right]$$

Live Bed Scour

Live Bed Scour 
$$\frac{V}{V_c} \ge \frac{V_{lp}}{V_c}$$
  
 $\frac{d_{se}}{D} = K_s 2.2 \ tanh\left[\left(\frac{y_0}{D}\right)^{0.4}\right]$ 

where

 $D \equiv$  structure width at zero flow skew angle,

 $V_c \equiv$  sediment critical velocity,

 $K_s \equiv$  structure shape coefficient, and

 $V_{lp} \equiv$  velocity where the live bed peak scour occurs (flow and sediment conditions where the bed planes out).

These equations are intended for design and thus are, by design, conservative, especially at lower velocities in the live bed scour range. Figures 18-20 are plots of normalized scour depth  $(y_s/D)$  versus normalized velocity  $(V/V_c)$ . It has long been known that, under most conditions, equilibrium scour depths decrease in magnitude as flow velocities go from clearwater to live bed scour conditions. The data obtained in this study shows the same behavior. To simplify the predictive equations and to provide a level of conservatism to the prediction, the clearwater peak (scour) is connected to the live bed peak (scour) with a straight line as shown in Figures 18-20. This must be kept in mind when comparing the predicted scour depths with the measured values.

As can be seen in Figures 18-20, Sheppard's equations give an accurate prediction of all of the experimental data obtained in this investigation. The slight over prediction in the range of velocities just beyond transition from clearwater to live bed scour conditions (i.e. for  $V/V_c$  just greater than 1) are for the reasons described above. The live bed peak scour depth in the equations was based on the hypothesis that local scour reaches a maximum in the live bed range at the point where the bed planes out. This was supported by data from small scale tests (2 inch diameter cylinder) conducted at the University of Auckland. The tests conducted in this research extended the live bed data to structure diameters three times that of the earlier work. High velocity, live bed tests with larger, prototype scale, structures are needed. But until such time that facilities where such tests can be conducted are available it is the opinion of the author of this report that the above

equations represent the best available method for local scour depth prediction in both the clearwater and live bed scour ranges.

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