

Procedural Manual: Reclassify Unknown Foundation Bridges

Federal Highway Administration & Florida Department of Transportation

NOVEMBER 2009



NCHRP

Web-Only Document 107:

Risk-Based Management
Guidelines for Scour at Bridges
with Unknown Foundations

Stuart Booth
Karlson Soderstrom
G&K & Associates, Inc.
Springfield, VA

Contractor's Final Report for NCHRP Project 24-25
Submitted October 2008

National Cooperative Highway Research Program
Report No. 380
Transportation Research Board of the National Academies

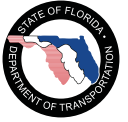


Table of Contents

Introduction..... 1

The Evaluation Procedure..... 2

Step 1: Collect Data..... 5

Step 2: Verify Scour Design 5

Step 3: Determine the Foundation Dimensions from the As-Built Information..... 6

Step 4: Risk Screening Procedure..... 6

 Step 4.1: Calculating Annual and Lifetime Risks Procedure 6

 Step 4.2: Determine which bridges are High Priority..... 10

 Step 4.3: Compare the Annual Probability of Failure to the Minimum Performance Level (MPL)..... 11

 Step 4.4: Determine if the Bridge has a Relatively Low Lifetime Risk of Failure..... 11

 Step 4.5: Determine if the Bridge has a Lifetime Risk of Failure > \$100,000 12

Step 5: Estimate Foundation Dimensions Procedure..... 12

 Step 5.1: Estimate the Design Pile Load 12

 Estimating Pile Load Procedures (PLOAD) 12

 Reverse Engineering Procedures 13

 Step 5.2: Estimate the Pile Embedment 21

 Estimating Pile Embedment of Unknown Foundation Procedure (Geotechnical Method) 21

 Estimating Concrete Pile Embedment Procedure (CPILE) 26

Step 6: Complete the Scour Evaluation Process 27

 Step 6.1: Determine if the Ground Elevations at the Bridge have changed 27

 Step 6.2: Complete the Phase 1 Scour Evaluation..... 27

 Step 6.3: Complete the Phase 2 Scour Evaluation..... 27

 Rapid Calculation of Scour at In-line Pile Bent Bridges over Small Streams Procedures 28

 Step 6.4: Complete the Phase 3 Scour Evaluation..... 30

 Lateral Stability Analysis 30

 Modeling Timber Piles 31

 Step 6.5: Check the Warrant of Automated Monitoring 31

 Step 6.6: Complete the Phase 4 Scour Evaluation..... 32

 Step 6.7: Check the Warrant of Countermeasures..... 32

 Step 6.8: Check the Warrant of Non-Destructive Testing 32

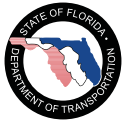
 Non-Destructive Testing Procedures..... 33

Appendix A..... A-1

Appendix B..... B-1

Appendix C..... C-1

Appendix D..... D-1



List of Figures

Figure 1.1: Unknown Foundation Evaluation Process 3
Figure 1.2: Pile Design Load Flow Chart..... 19
Figure 1.3: Estimating Pile Embedment of Unknown Foundations Flow Chart 22
Figure 1.4: Bridge Foundation Types..... 40
Figure 1.5: Bridge Foundation Types..... 41
Figure 1.6: NDT Flow Chart 42

List of Tables

Table 1.1: Typical Pile Data Table 5
Table 1.2: Scour Event Frequency Guidelines 8
Table 1.3: Annual Probability of Failure (P_A) 8
Table 1.4: MPL Description 11
Table 1.5: Median Sediment Diameter, Pile Diameter, and Number of Piles per Bent..... 29
Table 1.6: Estimated Cost of NDT Methods 43



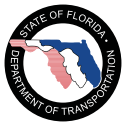
Introduction

The Procedural Manual provides procedures/guidelines and flow charts to evaluate Unknown Foundation Bridges. The Manual will be followed to evaluate Unknown Foundation Bridges in Florida and either:

- Reclassify the bridge as Low Risk, with proper associated coding of Item 113, or;
- Reclassify the bridge as Scour Critical and develop a Plan of Action, or;
- Keep the classification of “U” and develop a Plan of Action that includes a bridge closure plan.

The Procedural Manual has been developed as a manual to accurately and economically evaluate Unknown Foundation Bridges for the safety of Florida’s travelling public and to satisfy FHWA requirements. The process may involve one or more evaluation procedures depending on the site conditions and information available for the bridges.

In support of the procedures, guidelines, flow charts and processes contained in this Procedural Manual, a Final Report was completed to document the various screening methods and methods to evaluate the foundation stability. The Final Report also determined the accuracy and cost of using the various methods for different site conditions. The report used data from known foundation bridges dispersed throughout Florida to calibrate and test the procedures given in this manual.



The Evaluation Procedure

There are three initial steps in the evaluation process – see Figure 1.1: Unknown Foundation Evaluation Process, on the following page. The first step is collection of available data, followed by answering two evaluation criteria:

- Do the Plans contain a Pile Data Table with Scour Criteria?
- Are the as-built foundation dimensions shown in the data collected?

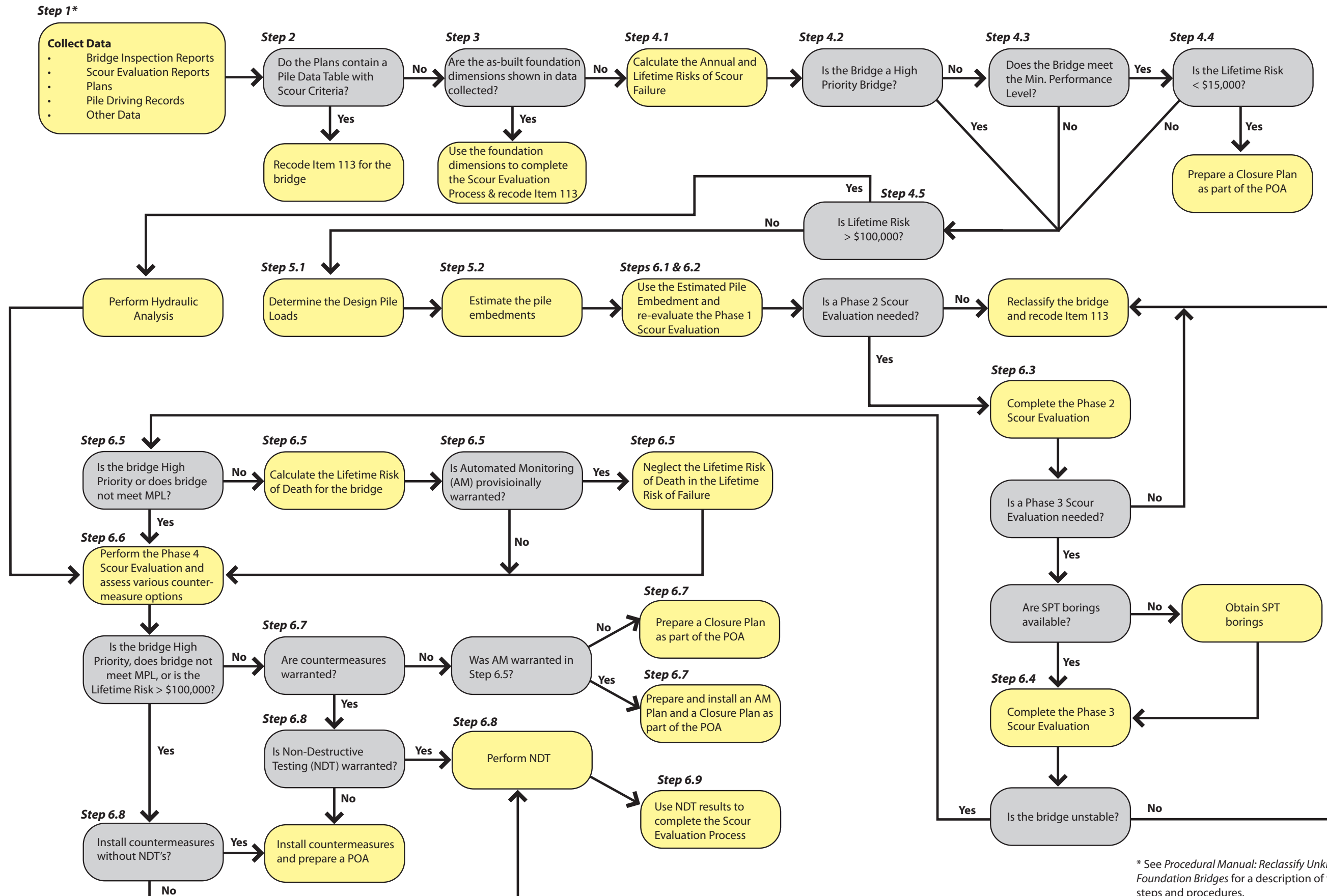
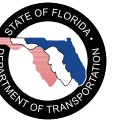
If your answer is no to both criteria, additional evaluation procedures and sub-procedures are needed to determine if the bridge has a low risk of scour failure. These sub-procedures could include:

- Risk Screening
- Calculating Annual & Lifetime Risks
- Estimating Foundation Dimensions, which includes Estimating Pile Loads (PLOAD), Estimating Concrete Pile Embedment (CPILE), and Reverse Engineering with Estimating Pile Embedment of Unknown Foundations
- Rapid Calculating of Scour at In-Line Pile Bent Bridges over Small Streams with Lateral Stability Analysis

These sub-procedures will be required based on the type of bridge, condition of the bridge, available data, soil conditions, and the scour potential at the site. The evaluation procedures and process flow chart will identify where these sub-procedures are required.

The following Figure 1.1 depicts the overall Unknown Foundation Evaluation Process. The process is broken down into various steps described further in this document.

The following are the three initial steps in the evaluation procedure.

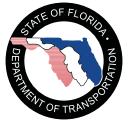


* See Procedural Manual: Reclassify Unknown Foundation Bridges for a description of these steps and procedures.

Figure 1.1: Unknown Foundation Evaluation Process



This Page Intentionally Left Blank



Step 1: Collect Data

The District Bridge Maintenance Office should have the following information available in their files if it was found during the Phase 1 Scour Evaluation. (Note: If a Phase 1 Scour Evaluation was not completed for the bridge, it should be completed during this step.)

- Pile Driving Records / Construction Field Book
- Scour Evaluation Reports
- Bridge Inspection Reports
- Plans (Original Plans and Widening/Reconstruction Plans)

If the District Bridge Maintenance Office does not have the Plans, the local agency may have them. If the local agency is contacted, also ask them for Pile Driving Records or other Construction Records or Field Books. Check the Phase 1 Report for a reference to the Plans. If Plans were located during the Phase 1 Evaluation, the firm that prepared the report may have a copy of the Plans in their files.

If Plans cannot be located, go to Step 3.

Step 2: Verify Scour Design

If a Pile Data Table cannot be found in the Plans, go to Step 3.

If a Pile Data Table is found, check for Scour Design Criteria (see Table 1.1 below). If Scour Design Criteria is not included in the Pile Data Table 1.1, go to Step 3.

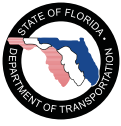
Table 1.1: Typical Pile Data Table

PILE DATA TABLE															
INSTALLATION CRITERIA								DESIGN CRITERIA							PILE CUT-OFF ELEV. (ft)
BENT NO.	PILE SIZE (in)	NOMINAL BEARING CAPACITY (tons)	TENSION CAPACITY (tons)	MIN. TIP ELEV. (ft)	TEST PILE LENGTH (ft)	REQ'D JET ELEV. (ft)	REQ'D PREFORM ELEV. (ft)	FACTORED DESIGN LOAD (tons)	DOWN DRAG (tons)	TOTAL SCOUR RESIST. (tons)	NET SCOUR RESIST. (tons)	100 YR. SCOUR ELEV. (ft)	LONG-TERM SCOUR ELEV. (ft)	Ø	
1	18	131	N/A	*	115	N/A	+8	85	N/A	0	0	0	0	0.65	+29.6
2	18	163	N/A	*	110	N/A	+8	85	N/A	21	21	+8.6	+4.8	0.65	+29.6
3	18	163	N/A	*	80	N/A	+8	85	N/A	21	21	+8.6	+4.8	0.65	+29.6
4	18	163	N/A	*	80	N/A	+8	85	N/A	21	21	+8.6	+4.8	0.65	+29.6
5	18	163	N/A	*	80	N/A	+8	85	N/A	21	21	+8.6	+4.8	0.65	+29.6
6	18	131	N/A	*	80	N/A	+8	85	N/A	0	0	0	0	0.65	+29.6

* THE MINIMUM TIP ELEVATION IS CONTROLLED BY SECTION 455 OF THE SPECIFICATIONS.

If a Pile Data Table with Scour Design Criteria is shown in the Plans, then review the Bridge Inspection Reports and the Scour Evaluation Reports. If conditions at the site have changed significantly since the bridge was constructed, go to Step 3. One indication of significant changes would be that the general bed elevation near the bent is lower than the long-term scour elevation given in the Pile Data Table.

If a Pile Data Table with Scour Design Criteria is shown in the Plans and conditions at the site have not changed significantly since the bridge was constructed, Step 2 completes the evaluation procedure process. Remove the bridge from the list of Unknown Foundations and recode Item 113 as stable.



Step 3: Determine the Foundation Dimensions from the As-Built Information

Check the data collected to see if the As-Built Foundation Dimensions can be determined. New data may have been obtained, or occasionally a piece of information may have been overlooked during the original scour evaluation. If the Foundation Dimensions cannot be determined, go to Step 4.

If the dimensions can be determined, then Step 3 completes the unknown foundation evaluation. Complete the original scour evaluation process as a Known Foundation Bridge. Update the Phase 1 Scour Evaluation with the new information. Complete Phase 2, 3, and 4 Scour Evaluations if needed.

Step 4: Risk Screening Procedure

This procedure is based on the process recommended in NCHRP Web Only Document 107, Risk-Based Guidelines for Scour at Bridges with Unknown Foundations (Stein and Sedmera [2006]).

Step 4.1: Calculating Annual and Lifetime Risks Procedure

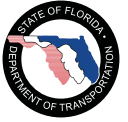
This procedure describes the steps taken to calculate the annual and lifetime risks via the HYRISK methodology as described by NCHRP Web Only Document 107, Risk-Based Management Guidelines for Scour at Bridges with Unknown Foundations (Stein and Sedmera [2006]). The methodology has been modified to reflect representative replacement costs, detour durations, and statewide probabilities of failure for Florida. This procedure refers to the table contained in the Procedural Manual's Appendix A. This table contains the calculated costs of failure (bridge replacement cost, detour cost, loss of life cost, and total cost of failure), the scour vulnerability, overtopping frequency, annual probability of failure, annual unadjusted risk, high priority, minimum performance level, K_1 , remaining life, lifetime probability of failure, unadjusted lifetime risk, and scour mode, sorted by bridge number for the unknown foundation bridges in the National Bridge Inventory. In the table, the unknown foundation bridges were identified by filtering the data in the NBI according to the following:

- Item 42B >4 — Bridge is over water;
- Item 43B \neq 19 — Structure is not a culvert;
- Item 5A = 1 — Route carried on the structure (eliminates multiple bridge number listings); and
- Item 113 = U — Structure has unknown foundations.

Task 1: Calculate Cost of Failure

Consult the table in Appendix A. Identify the bridge replacement cost, detour cost, loss of life cost, and total cost of failure. The total cost of failure equals the sum of the bridge replacement cost, detour cost, and loss of life cost. The replacement costs were estimated via the procedure outlined in the NCHRP Web Only Document 107. If more detailed replacement cost estimates are available, employ those estimates rather than the ones provided.

If the detour cost is listed as NA, then the detour length (NBI Item 19) was coded as 199. This implies that the bridge either is on a dead end road, provides the only access (e.g., to an island), or the detour length is greater than 199 km (= 123.6 mi). For these bridges, develop alternative detour costs; for example, installation of temporary bridges, ferry service, etc. Add the developed detour costs to the replacement cost and loss of life cost to get the new total cost of failure.



Task 2: Determine Whether Bridge Is Tidally Influenced

The HYRISK methodology developed probabilities of failure by relating overtopping frequency and scour vulnerability. The inclusion of overtopping frequency followed the logic that scour is proportional to shear stress and shear stress is proportional to depth of flow. Therefore, the waterway has a maximum scour potential at full flow depth and less potential at lesser depths. For tidal bridges, however, scour potential is not necessarily correlated to the number of high water surface elevation events. Rather, it is a function of not only the bridge's exposure to hurricane generated storm surges (both magnitude of the surge and frequency) but also the way the surge propagates from the ocean through the waterway to the bridge and the storage area behind the bridge. As such, for tidal bridges, the scour event frequency should replace the overtopping frequency in evaluating a bridge's probability of failure.

From the PONTIS database, identify the mode of flow. The bridge should be coded as one of the following:

- @ — Unknown
- ! — Not applicable
- R — Riverine
- M — Tidal/Riverine
- T — Tidal

If the rating is R or !, continue on to Task 3. If the rating is @, M, T, have a qualified coastal engineer assess the scour event frequency. Since this assessment relies on sound engineering judgment, the coastal engineer should have demonstrable experience with tidal circulation and storm surge propagation in the study area. The coastal engineer should consult the following reference materials (at a minimum): aerials of the area, topographic/bathymetric maps, hurricane history at the bridge site, FEMA flood maps, FEMA flood insurance studies (FIS), storm surge hydraulic modeling studies for nearby locations. Based on these materials, rate the scour event frequency employing the guidelines in Table 1.2 below. Associated with each frequency are a return period and a description detailing reasons for rating. The engineer responsible for rating should weigh all factors and not simply hurricane history when assigning a scour event frequency rating. For example, a bridge located at the back of a bay with very little water storage behind it may experience frequent flooding, but since the storage area behind it is low, the scour event frequency may be slight. Illustrating the effects of storm surge propagation, a bridge to a small isolated island off the coast may experience storm surges on a relatively frequent basis (greater than once every three years). However, if the storm surge propagates to the bridge equally on both sides, flow through the bridge may be minimal, thus deserving a lower scour event frequency rating than the hurricane history might imply. Conversely, a bridge across a tidal inlet is located in an area that experiences infrequent surge events (return periods of 11 to 100 years), and when a surge affects the bridge, significant flows result. However, due to the infrequency of surge events, the scour event frequency is rated as slight.

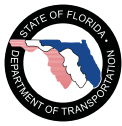


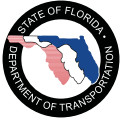
Table 1.2: Scour Event Frequency Guidelines

Scour Event Frequency	Return Period (yr)	Reasons for Rating
Never (N)	Never	The bridge never experiences scour producing flows due to tidal circulation or hurricane induced storm surge.
Remote (R)	> 100	The bridge is located in an area that rarely (> 100 years) experiences storm surges. The surge will attenuate significantly before it reaches the bridge site. The storage area behind the bridge is small (example: bridges on dead end canals, or near the backs of bays).
Slight (S)	11 to 100	The bridge is located in an area that experiences significant hurricane generated surge every 11 to 100 years. The bridge is located relatively far from the coast and significant attenuation of the surge is expected. The storage area behind the bridge is small to moderate (example: bridge located far from an inlet across a tidal creek with narrow floodplains).
Occasional (O)	3 to 10	The bridge is located in an area that experiences hurricane generated surge every 3 to 10 years. The bridge is located relatively near to the coast and significant attenuation of the surge is not expected. The storage area behind the bridge is moderate to large (example: bridges on the Intracoastal Waterway near tidal inlets, or bridges across bays).
Frequent (F)	< 3	The bridge is located in an area that frequently experiences hurricane generated flows. The potential for high flows through the bridge during surge events is high and the storage area behind the bridge is large (example: bridges on the open coast over tidal inlets).

For bridges rated M, @, or left blank, compare the rating selected above with the overtopping frequency contained in Appendix A. Select the more frequent rating. Next, with the scour vulnerability rating from Appendix A, select the new annual probability of failure from Table 1.3 (with N corresponding to a probability of failure of 0):

Table 1.3: Annual Probability of Failure (P_A)

Scour Vulnerability	Overtopping Frequency / Scour Event Frequency			
	Remote (R)	Slight (S)	Occasional (O)	Frequent (F)
0	1	1	1	1
1	0.01	0.01	0.01	0.01
2	0.005	0.006	0.008	0.009
3	0.0011	0.0013	0.0016	0.002
4	0.0004	0.0005	0.0006	0.0007
5	0.00018	0.00024	0.00032	0.00039
6	0.000077	0.00011	0.00017	0.00022
7	0.000077	0.00011	0.00017	0.00022
8	0.0000017	0.0000022	0.0000085	0.0000170
9	0.0000011	0.0000013	0.0000017	0.0000030



Task 3: Calculate the Risk Adjustment Factors

These factors allow adjustments to the risk for the structure foundation and/or design. As defined by the NCHRP document, K_1 is a bridge type factor and K_2 is a foundation type factor.

NCHRP Web Only Document 107 recommends the following for K_1 and K_2 :

K_1	=	0.67	for rigid continuous spans with lengths in excess of 100 ft (NBI Item 43 = 2, 4 or 6 and Item 48 > 100 feet); and
	=	1.0	for all others.
K_2	=	0.2	for bridges on massive rock;
	=	0.8	for all wood or pile foundations; and
	=	1.0	for all others.

According to Stein and Sedmera (2006), the K_1 factor “reflects the benefit of structural continuity which can compensate for loss of intermediate supports... The influence of rigidity, type of structure, etc., has significant effects on the tolerable movement criteria, which may be defined as an increase in maximum stress to a point below yield, therefore precluding collapse.” The reference also notes that even structures founded on massive rock may still incur damage attributed to an inadequate waterway opening or other causes, and as such, the K_2 factor cannot equal zero by definition.

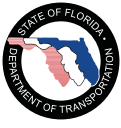
K_1 is given in the table in Appendix A. K_2 must be determined from the information above.

Task 4: Calculate Annual and Lifetime Risks of Failure

Calculate the annual risk of failure ($Risk_A$) via the following equation:

$$Risk_A = K_1 K_2 P_A Cost$$

where K_1 is given in the table in Appendix A and K_2 is the risk adjustment factor calculated in Task 3, P_A is the annual probability of failure found in Appendix A (for bridges not tidally influenced) or calculated in Task 2 (for bridges tidally influenced), and Cost is the total cost of failure from Appendix A or calculated in Task 1.



Calculate the lifetime probability of failure (P_L) via the following equation:

$$P_L = 1 - (1 - P_A)^L$$

where P_A is the annual probability of failure from Appendix A or calculated in Task 2, and L is the provisional remaining life of the bridge. To calculate L , it is recommended to subtract the bridge's current age from 75 years or set equal to 15 years, whichever is greater. Exceptions to this are bridges currently designated for replacement within a known time frame (i.e., within the Five Year Work Program). P_L is given in the table in Appendix A.

Calculate the lifetime risk of failure ($Risk_L$) via the following equation:

$$Risk_L = K_1 K_2 P_L Cost$$

where K_1 and K_2 are the risk adjustment factors from Task 3, P_L is the lifetime probability of failure calculated above, and $Cost$ is the total cost of failure from Appendix A or calculated in Task 1.

Reference

Stein, S. and Sedmera, K. (2006) NCHRP Web Only Document 107, Risk-Based Management Guidelines for Scour at Bridges with Unknown Foundations. Contractor's Final Report for NCHRP Project 24-25. National Cooperative Highway Research Program, Transportation Research Board of the National Academies. http://onlinepubs.trb.org/onlinepubs/nchrp/nchrp_w107.pdf

Step 4.2: Determine which bridges are High Priority

High Priority bridges are defined as:

- Bridges on Principal Arterials
- Bridges on Evacuation routes
- Bridges that provide access to local emergency services such as hospitals
- Bridges that are defined as critical in a local emergency plan (i.e., bridges that enable immediate emergency response to disasters)

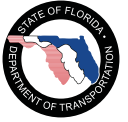
High priority bridges are noted in the table in Appendix A.

High priority bridges automatically require additional investigation in the NCHRP method.

Principal Arterials have a Code of 01, 02, 11, 12, or 14 in the FUNCLASS field of the ROADWAY table in the PONTIS Database. Critical travel routes are identified in the CRIT_TRAVEL field of the ROADWAY table in the PONTIS Database.

If the bridge is a High Priority bridge, exit this procedure and go to Step 4.5.

If the bridge is not a High Priority bridge, go to Step 4.3.



Step 4.3: Compare the Annual Probability of Failure to the Minimum Performance Level (MPL)

The MPL is a probability of failure that a bridge with a certain functional classification must outperform. Table 1.4 is from NCHRP Web Only Document 107, Risk-Based Guidelines for Scour at Bridges with Unknown Foundations (Stein and Sedmera [2006]), and can be used to determine the MPL.

Table 1.4: MPL Description

NBI Item 26	Description	Minimum Performance Level (Threshold Probability of Failure)
Rural		
01, 02	Principal – All	0.0001
06, 07	Minor Arterial or Major Collector	0.0005
08	Minor Collector	0.001
09	Local	0.002
Urban		
11, 12, 14	Principal – All	0.0001
16	Minor Arterial or Major Collector	0.0002
17	Minor Collector	0.0005
19	Local	0.002

The Table in Appendix A gives the MPL and indicates if the bridge meets the MPL.

If the bridge's probability of failure is greater than the MPL, go to Step 4.5.

If the bridge's probability of failure is less than the MPL, go to Step 4.4.

Step 4.4: Determine if the Bridge has a Lifetime Risk of Failure <\$15,000

Compare the lifetime risk of failure to \$15,000. This amount represents a minimum amount that would have to be spent on retrofits/countermeasures/automated monitoring at the bridge.

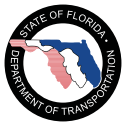
If the lifetime risk of failure is greater than \$15,000, then go to the Step 4.5.

If the lifetime risk of failure is less than \$15,000, prepare a Plan of Action that includes a bridge closure plan. Item 113 will remain coded as "U."

Section 8 of FHWA's Plan of Action (POA) template documents the bridge closure plan. Parts of the closure plan include:

- Criteria for consideration of bridge closure
- Emergency repair plans
- Responsible agency for closure
- Contact person
- Criteria for reopening the bridge
- Agency responsible for reopening the bridge

More information, a copy of the template, and example POA's can be found at: www.fhwa.dot.gov/engineering/hydraulics/bridgehyd/poa.cfm



Step 4.5: Determine if the Bridge has a Lifetime Risk of Failure > \$100,000

If the Lifetime Risk of Failure is greater than \$100,000, then perform a hydraulic analysis to determine the necessary information to select countermeasures. Go to Step 6.6.

If the Lifetime Risk of Failure is less than \$100,000, then continue to Step 5.

Step 5: Estimate Foundation Dimensions Procedure

Step 5.1: Estimate the Design Pile Load

If the Design Pile Loads can be found in the Plans, use the Plan values and go to Step 5.2.

If the bridge can be determined to be one of the historical Design Standards (see Appendix B), use the Design Pile Loads on the Design Standard and go to Step 5.2.

If the bridge includes pile bents (bents with piles in a single row), use the following Estimating Pile Loads (PLOAD) Procedures at all pile bents. This procedure will work with concrete, steel, and timber piles.

For all other bents and piers, use the Reverse Engineering Procedure to estimate the Design Pile Load. Consider using the Reverse Engineering Procedure at pile bents if the bent also includes piles driven for a widening or if the height above ground is significant. Also, if the embedment depths obtained using PLOAD are such that stability is marginal when completing the Scour Evaluation Process as noted in Step 6, consider returning to this step and using the Reverse Engineering Procedure to estimate the Design Pile Load for pile bents.

Estimating Pile Load Procedures (PLOAD)

Pile Loads

Pile loads are generally provided on the bridge plans. If the plans do not exist or the pile loads are not given, the Artificial Neural Network, PLOAD, can be used to estimate the Design Pile Load values. Inputs to and outputs from PLOAD will be from and to a Microsoft Excel (2003) file named "PLOAD_IO". One worksheet is used for input and one for output. *District Offices will provide a CD-ROM of PLOAD worksheets.*

The following fields are required for this program:

- Bridge number
- Pile installation year
- Average span length
- Deck width
- Bridge material
- Bridge design
- Pile size
- Number of piles per bent
- Pile type



Values for these input parameters can be obtained from the PONTIS database and from the sources outlined in the “reverse engineering” section of this document. Each input field will accept values within a predetermined range. These ranges are based on the training data used for PLOAD. In general the PLOAD estimates will be conservative, i.e. the predicted load will be lower or equal to the actual design load. The user’s manual for PLOAD will specify units, formatting of input and output fields in EXCEL spreadsheets, acceptable input ranges and detailed instructions for installing and running the program.

Reverse Engineering Procedures

Reverse engineering is used to calculate the estimated pile design loads on the foundation of a structure given the geometry and likely loads used during the design process. The calculated pile load is then used in conjunction with a pile capacity curve, either per SPT borings or a standard curve as provided, to determine a likely pile embedment.

Task 1: Data Gathering

Before completing the reverse engineering procedure, a full inventory of available data should be created. This should include any available plans, inspection reports, scour reports, etc.

Plans

If bridge plans are available, determine if the design pile load is provided. If the design pile load is provided, this information should be used with the pile capacity curve to determine the estimated minimum pile embedment, so go to Step 5.2. If the pile load is not provided, the bridge geometry on the plans should be used to calculate a pile design load, including dead load, wind load (if deemed appropriate), and live load.

Inspection Reports and Scour Reports

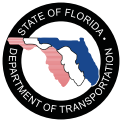
If there are no plans available, recent inspection and scour reports should be studied to ascertain bridge geometry, structure type, and construction materials for the purpose of calculating pile loads.

Bridge Site Visit

If no plans are available and the inspection/scour reports do not have enough data to determine pile loads, a bridge site visit should be made to obtain relevant structure data. Also, if there is any question regarding the reliability of the existing data, a site visit should be made to verify and obtain supporting or additional information.

Structure Dimensions

- Thickness of slab/deck
- Size of beams/girders, if applicable
- Railing type and size
- Wearing surface and thickness
- Pile type and spacing
- Bent or pier cap dimensions
- Span length(s)
- Roadway width
- Sidewalk width and thickness, if applicable
- Curb width and thickness, if applicable
- Utilities and other appurtenances



Bridge Data Cards

The District Offices have bridge data cards for state owned bridges through the mid-1960s. These data cards include span lengths, roadway widths, design live load, and foundation type.

Historical Bridge Standard Drawings

A list of historical bridge standard drawings is included in Appendix B. Many older bridges were standardized with span lengths/widths and the standard drawings are available from the District Offices. Based on the bridge dimensions and year of construction, it may be possible to determine if it was a standard structure. The pile loads may be available on the standard drawings.

Carter Key Manual

The FDOT published a construction estimation guide called the Carter Key Manual. It is useful for determining the weight of post and rail style barriers. It is available online at: <http://www.flacqc.com/transfer/Carter%20Key.pdf>

Task 2: Determining Design Live Load for Pile Loads

Because the intent is to determine the pile load that would have been used for the construction of the bridge, it is necessary to determine what design live load would have been used for the design of the structure. If the design pile load or the design live load is not available from plans or other sources, there are other means of determining the design live load.

Bridge Data Cards

Contact the District Office for a copy of the bridge data card. This card lists the design live load. These cards are available for state owned bridges that were constructed through the mid-1960s.

Barrier End Post

Bridges through at least the mid-1950s that have not had a barrier retrofit have the design live load stamped on the end post of the railing. The stamp is on the left side of the bridge as the bridge is approached.

Bridges Constructed Prior to 1986 without Additional Identifying Features

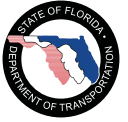
For all other bridges constructed prior to 1986, conservatively use an H15 truck, as defined in the AASHTO Standard Specifications.

Bridges Constructed after 1986 and before 2002

For Bridges constructed after 1986, utilize an HS20-44 live load as defined in the AASHTO Standard Specifications.

Bridges Constructed after 2002

The use of LRFD was mandated by FDOT in 2002. Therefore, for bridges designed after 2002, use the HL-93 live load as defined in the AASHTO LRFD Code.



Task 3: Calculate Pile Loads

Task 3.1: Flat Slab Bridges on Pile Bents

Calculate Superstructure Dead Load Reaction to Bent

Determine the weights of the slab, wearing surface, sidewalks, curbs, utilities and railings for a one-foot strip width. Railings, curbs, utilities and sidewalks shall be assumed evenly distributed across the width of the bridge. Using the distributed live load, determine the reaction on the intermediate bent, taking into account continuity, if applicable.

Calculate Substructure Dead Loads

Determine the self weight of the substructure.

Determine the Live Load Reaction to the Bent

Determine the live load as in Task 2. Calculate the number of lanes on the bridge using the relevant AASHTO Specification. Note that for older structures the number of lanes on the bridge was associated with the roadway width, not a set lane width, as specified in the AASHTO Specifications. Determine the Multiple Presence Factor from the relevant AASHTO Specification. Calculate the reaction of one truck on the intermediate bent and multiply by the number of lanes and the Multiple Presence Factor; this is the total live load reaction at the intermediate bent.

Factor Loads

The pile loads should be determined using the same design methodology (Allowable Stress Design, Load Factor Design or Load and Resistance Factor Design) used when the bridge was designed. It is not always easy to ascertain the original design method, so Engineering Judgment should be used. Regardless of methodology chosen, it is necessary to coordinate with the geotechnical engineer so that the appropriate capacity curves are used.

The standard pile capacity curves are based on Allowable Stress Design (ASD), so if no SPT boring data is available and a boring will not be performed, calculating loads based on ASD is reasonable.

Determine the Pile Load

Sum the superstructure and substructure dead loads and add them to the total live load reaction. Divide by the number of piles to determine a conservative estimate of the design pile load.

Task 3.2: Concrete and Steel Beam Bridges on Pile Bents

Task 3.2.1: Beams Centered Over Piles

Calculate Beam Dead Load Reaction

Using the tributary area of the beam, calculate the deck dead load applied to the beam. Assume wearing surface, railings, sidewalks, utilities, and curbs are distributed equally to all beams. If no information regarding the beam buildup is known, conservatively ignore it for these calculations.

Determine Live Load Reaction

Determine the design truck as in Task 2. Calculate the truck reaction at the intermediate bent and distribute to girders.



Calculate Substructure Dead Load

Determine the total self-weight of the substructure cap and appurtenances.

Factor Loads

The pile loads should be determined using the same design methodology used when the bridge was designed. It is not always easy to ascertain the original design method, so Engineering Judgment should be used. Regardless of methodology chosen, it is necessary to coordinate with the geotechnical engineer so that the appropriate capacity curves are used.

The standard pile capacity curves are based on Allowable Stress Design, so if no SPT boring data is available and a boring will not be performed, calculating loads based on ASD is reasonable.

Determine Pile Load

The pile load is the total weight of the substructure divided by the number of piles plus the beam dead and live load reactions.

Determine Wind Loads

Taller structures may be controlled by load cases in which wind is applied. Calculate the wind load per the AASHTO specification and apply it as appropriate.

Task 3.2.2: Beams Not Centered over Piles

Calculate Dead Load Reaction

Using the tributary area of the beam, calculate the deck dead load applied to the beam. Assume wearing surface, railings, sidewalks, utilities, and curbs are distributed equally to all beams. If no information regarding the beam buildup is known, ignore it for these calculations.

Determine Live Load Reaction

Determine the design truck as in Task 2. Calculate the truck reaction at the intermediate bent and distribute to girders.

Calculate Substructure Dead Load

Determine the self-weight of the substructure cap and appurtenances as a distributed load on a per foot basis.

Factor Loads

The pile loads should be determined using the same design methodology used when the bridge was designed. It is not always easy to ascertain the original design method, so Engineering Judgment should be used. Regardless of methodology chosen, it is necessary to coordinate with the geotechnical engineer so that the appropriate capacity curves are used.

The standard pile capacity curves are based on Allowable Stress Design, so if no SPT boring data is available and a boring will not be performed, calculating loads based on ASD is reasonable.

Determine Pile Load

Perform a continuous beam analysis of the bent cap using calculated dead and live load reactions and the distributed load of the substructure cap.



Determine Wind Loads

Taller structures may be controlled by load cases in which wind is applied. Calculate the wind load per the AASHTO specification and apply it as appropriate.

Task 3.3: Timber Stringer Bridges on Pile Bents

Calculate Superstructure Dead Load

Because the stringers are generally spaced so close together, they can be treated as a distributed load on a per foot basis, and the entire superstructure reaction on the bent can be calculated as follows:

Determine the total weight of the railing, curb and other appurtenances, as well as the weight of the decking over the bridge width. Determine the total weight of the stringers. Calculate the total reaction of all of the stringers, the railing, curb, etc. on the bent. Distribute the reaction of the dead loads using the entire cap width.

Calculate the Live Load Reaction

Determine the design truck as in Task 2. Calculate the truck reaction at the intermediate bent. Generally the spans on a timber stringer bridge will be short enough that only one truck axle will fit on a span at a time. In this case it is acceptable to assume that the wheel load will pass directly through a stringer to the cap. If more than one axle fits on the span, proceed in determining the live load reaction using the same methodology as stated for slab bridges, see Determine the Live load Reaction to the Bent in Task 3.1.

Calculate Substructure Dead Load

Determine the total weight of the bent cap.

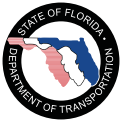
Factor Loads

The pile loads should be determined using the same design methodology used when the bridge was designed. It is not always easy to ascertain the original design method, so Engineering Judgment should be used. Regardless of methodology chosen, it is necessary to coordinate with the geotechnical engineer so that the appropriate capacity curves are used.

The standard pile capacity curves are based on Allowable Stress Design, so if no SPT boring data is available and a boring will not be performed, calculating loads based on ASD is reasonable.

Determine Pile Load

If the live load is calculated per Calculate the Live Load Reaction in this Task, add the super- and substructure dead loads and divide by the number of piles. Add the wheel load as the live load. If the live load is calculated per Determine the Live Load Reaction to the Bent as in Task 3.1, add the super- and substructure dead loads to the live load reaction and divide by the number of piles.



Task 3.4: Bridges with Piers on Pile Footings

Calculate Live and Dead Loads at Base of Column

Determine the loads acting on the pier (including dead, live, wind, centrifugal, braking, etc) and transfer to the base of the column using standard engineering practice.

Factor Loads

The loads should be factored and combined using the same methodology used during design. It is not always easy to ascertain the original design method, so Engineering Judgment should be used. Regardless of methodology chosen, it is necessary to coordinate with the geotechnical engineer so that the appropriate capacity curves are used.

The standard pile capacity curves are based on Allowable Stress Design, so if no SPT boring data is available and a boring will not be performed, calculating loads based on ASD is reasonable.

Determine Maximum Pile Load

Traditional methods of engineering analysis should be used to determine the design pile load.

The Pile Design Load flow chart provides a diagrammatic process to calculate the estimated pile design loads on the foundation of a structure, either being a flat slab bridge, concrete or steel beam bridge, timber stringer bridge or a bridge with piers. The calculated pile load is then used in conjunction with a pile capacity curve, either per SPT borings or a standard curve to determine a likely pile embedment.

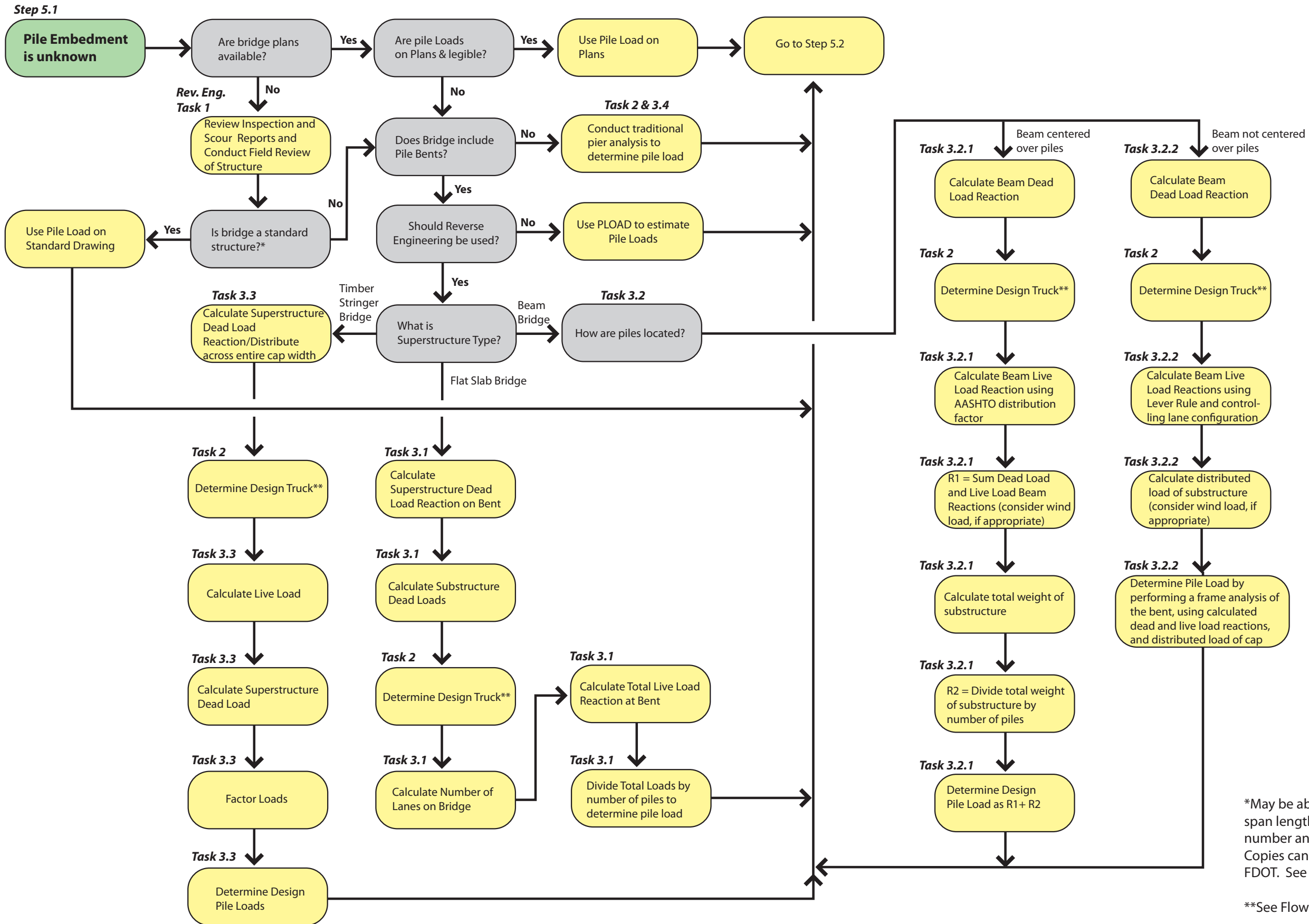
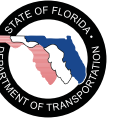


Figure 1.2: Pile Design Load Flow Chart



Reverse Engineering
Task 2

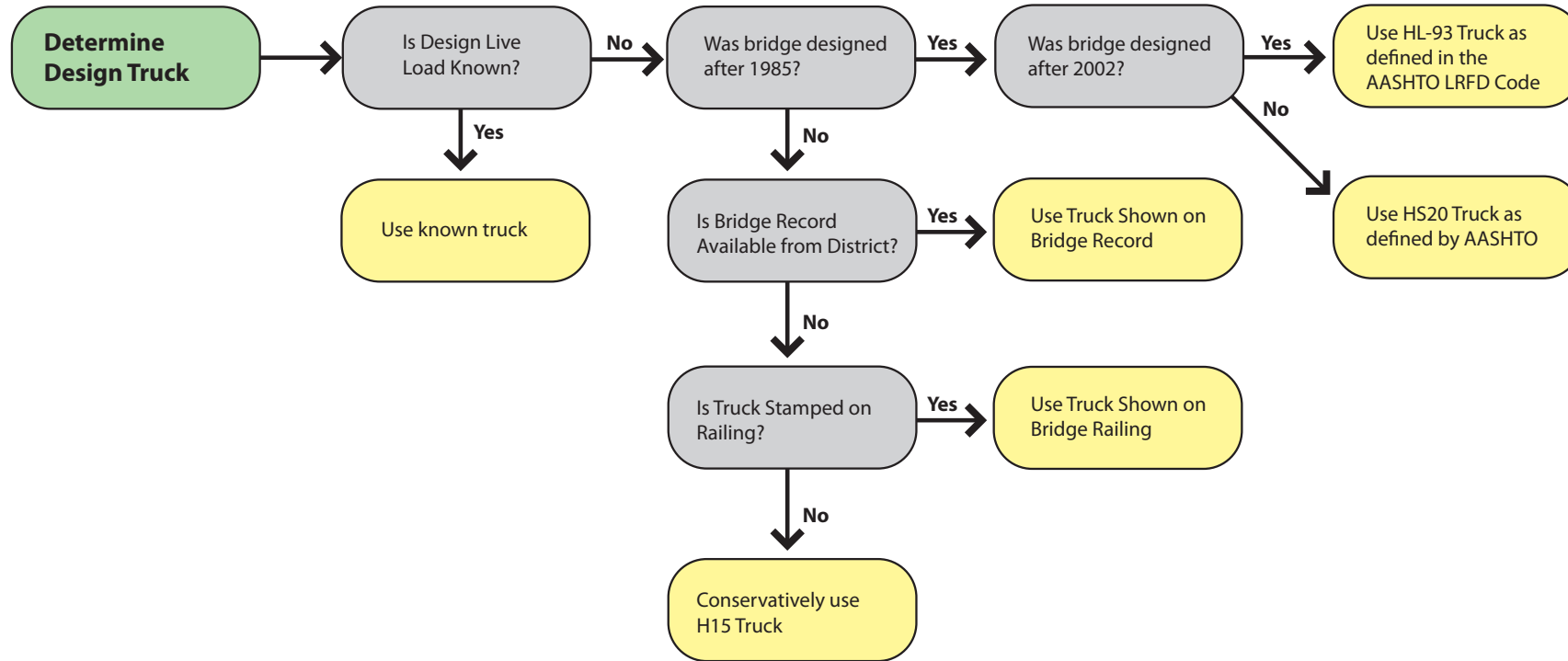


Figure 1.2: Pile Design Load Flow Chart (continued)



Step 5.2: Estimate the Pile Embedment

Use the Procedure for Estimating Pile Embedment of Unknown Foundations (Geotechnical Method) to estimate the pile embedment at each pier or bent, including Concrete Pile Bents (bents with concrete piles in a single row).

Additionally, use the following Estimating Concrete Pile Embedment (CPILE) Procedure at all concrete Pile Bents.

If these instructions are followed, then embedment predictions will be made using both methods (the Geotechnical method and CPILE) for concrete pile bents. Use the smaller of the two embedment values and proceed to the next step. Do not adjust the embedment with a safety factor. If the bent is not a concrete pile bent, then only the Geotechnical method estimate will be made. Adjust the estimate with a safety factor of 0.8 and proceed to the next step. In the unlikely event that an estimate is made with CPILE, but an estimate is not made by the Geotechnical method, then adjust the estimate with a safety factor of 0.7 and proceed to the next step.

Estimating Pile Embedment of Unknown Foundation Procedure (Geotechnical Method)

Introduction

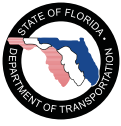
This procedure is intended to estimate the pile embedment under the soil conditions at the time the bridge was originally constructed. It must be noted that these estimated embedment depths are based on the ground elevations and soil profiles at the time of driving the pile. Any soil losses since that time and any predicted scour must be taken off of these embedment depths.

In addition, Allowable Stress Design (ASD) was used in the original design of the bridge foundations, therefore the estimated “Allowable” pile capacity rather than the “Davisson” pile capacity was used to estimate the pile embedment. If the Load Resistance Factor Design (LRFD) methodology will be used to evaluate the bridge stability, appropriate adjustments (either use the Davisson pile capacity curve or divide the Nominal Bearing by 2 and use the “Standardized” curve when SPT data is not available) need to be made to the following procedures.

Task 1: Data Collection

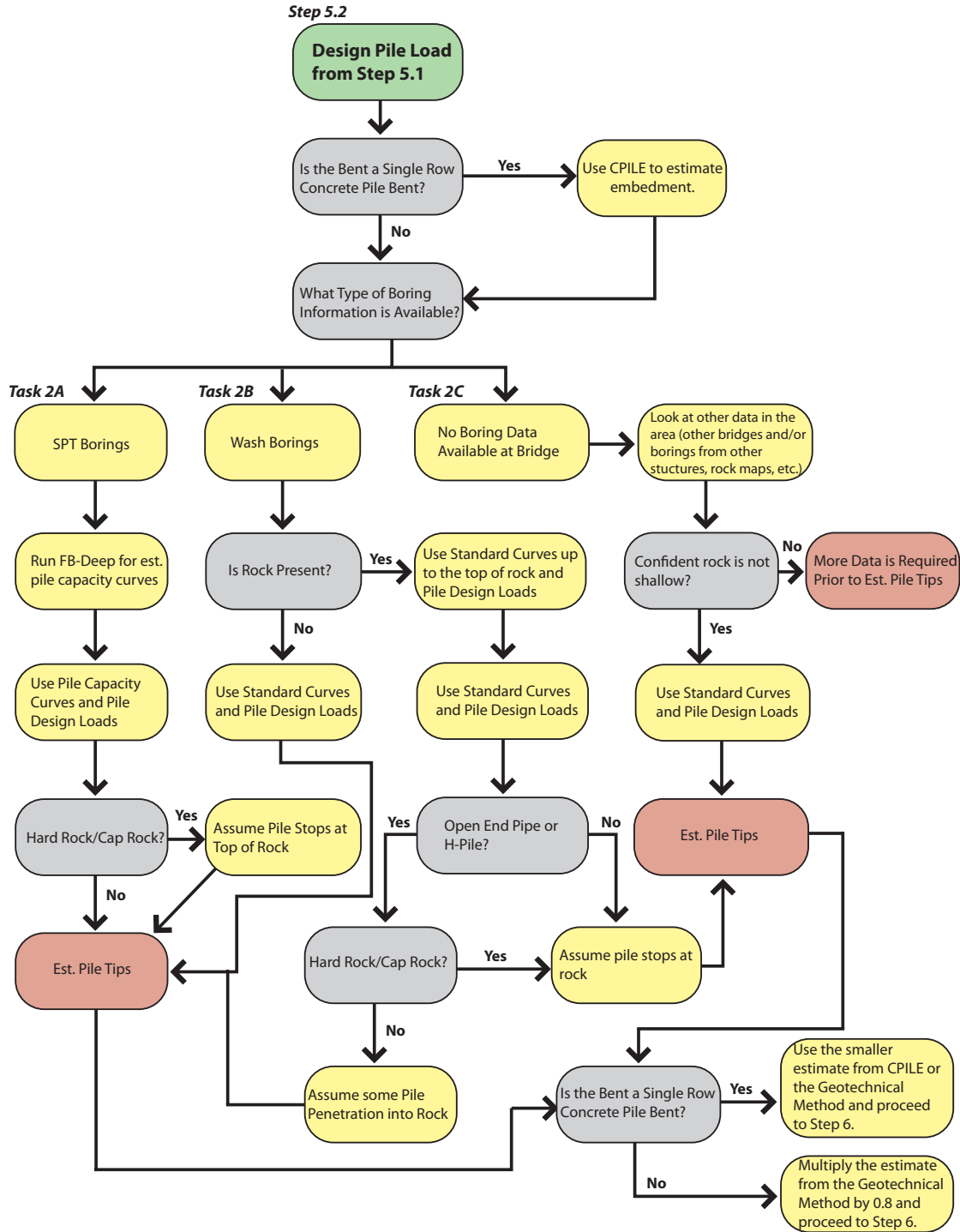
Collect all of the available data for the study bridge with unknown foundations. This may include but not limited to the construction plans and soil borings. The pile driving records of the widened bridge structures of the study bridge may be available. The soil borings may include SPT borings or wash borings. It is also possible that no soil borings are available at the specific site. Based on the availability of the soil data, there are three (3) different approaches to estimate the pile embedment:

- If there are SPT borings available, go to Task 2A
- If there are only wash borings available, go to Task 2B



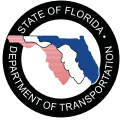
- If there are no soil borings available, go to Task 2C

Figure 1.3 provides a diagrammatic process to estimate the pile embedment using either SPT borings or wash borings. The flow chart also notes the process if there are no soil borings available.



All final results should be concurred with by the District Geotechnical Engineer (DGE)

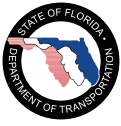
Figure 1.3: Estimating Pile Embedment of Unknown Foundations Flow Chart



Task 2A: Procedure with SPT Boring Data

Develop the estimated allowable pile capacity curves by performing the FB-Deep Analysis using the available SPT boring data for the concrete and steel piles of the corresponding size. However, for the timber pile, the FHWA Program DRIVEN should be used. If there is more than one boring available, all of the allowable pile capacity curves from every soil boring should be plotted in the same graph, so the upper bound of the capacity can be determined. For ASD design the “Allowable” pile capacity curves should be used, for LRFD design the “Davisson” pile capacity curve should be used.

- Obtain the bridge foundation design loads from Step 5.1. The shortest pile embedment for the required design loads should be determined from the allowable pile capacity curves.
- Check the following situations to ensure that the results are reasonable:
 - Is there a hard rock or cap rock layer presented in the soil profile, and is it reasonable to expect that the piles could penetrate this hard layer? If not, assume the pile stops at the top of the rock. It should be noted that FB-Deep limited the maximum N-value used in the calculation and could underestimate pile capacity which might falsely show the pile penetrating deep into the hard layer.
 - Are the estimated minimum embedment depths associated with the correct piers?
 - Is the site condition variable? If so, is there enough information to address this variability?
 - If wash borings are also available, follow the Wash Boring Procedure shown in the Task 2B to estimate the minimum embedment and compare both results.



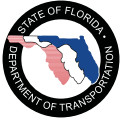
Task 2B: Procedure with Wash Boring Data

- Develop the “Standardized” allowable pile capacity curves by using Program FB-Deep for concrete or steel pile, and Program DRIVEN for timber pile for the corresponding pile size. The standard Bearing Capacity curves for uniform soil profiles have been developed using an SPT N-Value of 15 for concrete piles, 15 for timber piles, and 20 for steel piles. The standard curves are in Appendix C. Review the available wash boring data to check if rock and/or cemented soil layers are present.
- Obtain the bridge foundation design loads from the existing construction plans if they are available. If there is no design loads available from the plans, the structural engineer should be consulted for the structural loads.

The shortest pile embedment for the required design loads should be determined from the “Standardized” allowable pile capacity curves.

However, if rock and cemented soil layers are present, the “Standardized” allowable pile capacity curves might need to be modified according to the type of pile foundation. If the pile foundation is either H-Pile or open-ended pipe pile, the potential and depth of the pile penetrating into the top of rock should be evaluated. For other types of pile foundation, the pile embedment should assume stopping at the top of rock and/or cemented soil layers.

- Check the following questions to ensure that the results are reasonable:
 - Review the estimated pile embedment depths with the boring data to ensure it is reasonable.
 - Are the estimated minimum embedment depths associated with the correct piers?
 - Is the site condition variable? If so, is there enough information to address this variability?



Task 2C: Procedure with No Boring Data

- Search any available soil information in the vicinity of the study bridge site which might include the data from other bridges or structures near the unknown foundation bridge, SCS maps, or Florida Geologic Survey, etc.
- Develop the “Standardized” allowable pile capacity curves by using Program FB-Deep for concrete or steel pile, and Program DRIVEN for timber pile for the corresponding pile size. The standard Bearing Capacity curves for uniform soil profiles have been developed using an SPT N-Value of 15 for concrete piles, 15 for timber piles, and 20 for steel piles. The standard curves are in Appendix C. Review the available boring data to check if rock and/or cemented soil layers might be present.
- Obtain the bridge foundation design loads from the existing construction plans if they are available. If there is no design loads available from the plans, the structural engineer should be consulted for the structural loads.

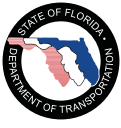
Based on the available information, if it is confident that shallow rock and cemented soil layers are not present, use the “Standardized” allowable pile capacity curves to estimate the shortest pile embedment for the corresponding pile size and required design loads. If rock and cemented soil layers are present, utilize the “Standardized” allowable pile capacity curves for the pile size to the top of this layer.

However, if rock and cemented soil layers are present, the “Standardized” allowable pile capacity curves might need to be modified according to the type of pile foundation. If the pile foundation is either H-Pile or open-ended pipe pile, the potential and depth of the pile penetrating into the top of rock should be evaluated. For other types of pile foundation, the pile embedment should assume stopping at the top of rock and/or cemented soil layers.

- Check the following questions to ensure that the results are reasonable:
 - Review the estimated pile embedment depths with the available data to ensure it is reasonable.
 - Are the estimated minimum embedment depths associated with the correct piers?
 - Is the site condition variable? If so, is there enough information to address this variability?

Task 3: Final Report

The final results should be reviewed and approved by the District Geotechnical Engineer.



Estimating Concrete Pile Embedment Procedure (CPILE)

An Artificial Neural Network (CPILE) has been developed and trained for predicting conservative estimates of concrete pile embedment (conservative in that the prediction is usually less than or equal to the actual embedment) for bridges with more than one span. Inputs to and outputs from CPILE will be from and to a Microsoft Excel (2003) file named "CPILE_IO". Two worksheets are used for input and one for output, all contained within one file. *District Offices will provide a CD-ROM of CPILE worksheets.* The required inputs can be determined based on the PONTIS database, the bridge plans (as explained in the reverse engineering section), and soil borings.

The required input for CPILE is as follows:

- Bridge number
- Pile construction year
- Pile station
- Pile offset
- Pile size
- Design load
- Pile ground elevation
- Is this a state owned bridge?

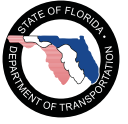
Each layer of the soil boring will be a new row in the boring input worksheet. The required fields in this worksheet are:

- Bridge number
- Boring station
- Boring offset
- Boring ground elevation
- Elevation of the bottom of the layer
- Soil type
- SPT N value

Each input field will accept values within a determined range. These ranges were determined based on the distribution of the training data. The user's manual will specify units, formatting of fields, acceptable input ranges and detailed instructions for installation and running the software.

The output worksheet will include:

- Minimum pile embedment for bridge
- Minimum pile embedment for each pile



Step 6: Complete the Scour Evaluation Process

This procedure will determine the stability of the bridge based on the results of the Estimate Foundation Dimensions Procedure.

Step 6.1: Determine if the Ground Elevations at the Bridge have changed

The pile embedment depths determined in the Estimate Foundation Dimensions Procedure are estimated for the time the pile was driven. Review the Bridge Inspection Reports and the Scour Evaluation Reports to help judge if the ground elevations have changed since the piles were driven. These reports will have information on the ground elevations at the time of construction (if available) and soundings taken during the various inspections and field visits. This information can be used to evaluate how the ground line is changing over time.

Additional long term bed and ground elevation changes expected in the future will be determined and applied in Step 6.3.

Step 6.2: Complete the Phase 1 Scour Evaluation

Using the estimated pile embedments, complete the Phase 1 Scour Evaluation, including a recommendation on the need for a Phase 2 Scour Evaluation.

If a Phase 2 Scour Evaluation is not needed, then reclassify the bridge as stable to complete the process.

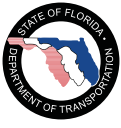
Step 6.3: Complete the Phase 2 Scour Evaluation

The Phase 2 Scour Evaluation involves a quantitative determination of the worst case scour depths for up to the 100 year event. The scour will be computed using the FDOT Bridge Scour Manual. As an alternative to the FDOT Bridge Scour Manual, the following Rapid Calculation of Scour at In-Line Pile Bent Bridges over Small Streams Procedure may be used to estimate the 100 Year Scour Elevation if:

- the bridge has in-line pile bents
- the design flow depth is less than 6 feet
- the bridge is over an inland stream

If a Phase 3 Scour Evaluation is needed, go to Step 6.4.

If a Phase 3 Scour Evaluation is not needed, then reclassify the bridge as stable to complete the process.



Rapid Calculation of Scour at In-line Pile Bent Bridges over Small Streams Procedures

This procedure outlines the steps to rapidly calculate scour at in-line pile bent bridges over small waterways. The scour calculations are only meant to provide a rapid assessment of scour for comparison purposes only. It is not meant to replace a Phase 2 Scour Evaluation. For the purposes of this procedure, a small stream is defined as an inland river (i.e., non-tidal) where the design flows are 6 ft deep or less. Graphs are provided in Appendix D for calculating contraction scour and local scour. This process does not include steps for estimated long term scour (channel migration and aggradation/degradation).

Task 1: Data Collection

Collect the data necessary to perform the scour estimation. These include as a minimum:

- Pile bent geometry (pile size, number of piles) — from existing plans or site visit;
- Current aerial photographs;
- FEMA Flood Maps;
- Bridge Inspection Reports (BIR), if available; and
- USGS Quadrangle Maps.

Task 2: Estimate Scour Inputs

Required inputs for employing the graphs include the following:

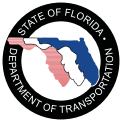
- Upstream width during design conditions;
- Width of the contracted section during design conditions;
- Upstream depth during design conditions;
- Depth at the bridge during design conditions;
- Flow skew angle; and
- Velocity during design conditions.

If this information is available from other sources (e.g., a Flood Insurance Study), then this would supercede the estimation techniques described below.

For contraction scour, estimate the ratio between the upstream width ($W_{upstream}$) and the width at the contracted section (W_{bridge}) from the aerial photography and the FEMA Flood Map. Estimate the upstream depth (y_1) and existing depth (y_0) from the USGS Quadrangle Maps, FEMA Flood Map (if the design flood elevation is unknown), and Bridge Inspection Reports.

For the local scour calculation, estimate the median sediment diameter from geotechnical records or site visit or general knowledge of the area. Graphs of local scour are provided for median sediment diameters of 0.15, 0.2, and 0.3 mm which encompasses a range of fine sands (USC) encountered in Florida. Do not employ these graphs if the sediment diameters are believed to be outside this range of sediments. Estimate the flow angle of attack based on the angle between the floodway approach direction and the bridge alignment. This is done through examination of the flood maps, aeriels, and topographic maps. Estimate the flow velocity through an application of Manning's Equation:

$$V = \frac{1.49}{n} R_h^{2/3} S^{1/2}$$



where V is the average velocity in ft, n is Manning’s n (estimated from site conditions), R_h is the hydraulic radius (estimated from USGS Maps, Bridge Inspection Reports, and design water surface elevations, and S is the slope of the free surface (estimated from the channel bottom slope via the USGS Maps). Manning’s Equation provides estimates of the average velocity. For rivers, local velocities can range from 0.9 to approximately 1.7 times the average velocity for the channel depending on the location across the cross section. As such, a 1.7 multiplier is recommended for conservative estimating purposes.

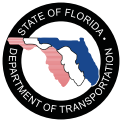
Task 3: Estimate the Local and Contraction Scour

From the first graph in Appendix D, estimate the depth in the contracted section (y_2) from the upstream depth (y_1) and the width ratio ($W_{upstream}/W_{bridge}$). Calculate the contraction scour (y_s) as the difference between y_2 and y_0 . The contraction scour graph was constructed from the assumption that the contraction scour is live bed with all flow routed through the bridge opening. It will provide a more conservative answer than if the bridge approaches are overtopped during the design event. It is left to the engineer performing the estimate to decide whether the assumption of live bed conditions is valid.

From the graphs in Appendix D, estimate the local scour as a function of the angle of attack and velocity. The graphs include the assumption that the flow depth is 6 ft, the piles are square, and the piles are spaced three pile diameters apart. The graphs include a range of median sediment diameters, pile diameters, and number of piles per bent. Table 1.5 below provides quick reference to the figure numbers found in the appendix.

Table 1.5: Median Sediment Diameter, Pile Diameter, and Number of Piles per Bent

		Pile Diameter	# of Piles per Bent			
			4	6	8	10
Median Sediment Diameter	D50 = 0.15 mm	12"	Fig. 2	Fig. 3	Fig. 4	
		14"	Fig. 5	Fig. 6	Fig. 7	
		16"	Fig. 8	Fig. 9	Fig. 10	Fig. 11
		18"	Fig. 12	Fig. 13	Fig. 14	Fig. 15
		20"	Fig. 16	Fig. 17	Fig. 18	Fig. 19
		24"	Fig. 20	Fig. 21	Fig. 22	Fig. 23
	D50 = 0.2 mm	12"	Fig. 24	Fig. 25	Fig. 26	
		14"	Fig. 27	Fig. 28	Fig. 29	
		16"	Fig. 30	Fig. 31	Fig. 32	Fig. 33
		18"	Fig. 34	Fig. 35	Fig. 36	Fig. 37
		20"	Fig. 38	Fig. 39	Fig. 40	Fig. 41
		24"	Fig. 42	Fig. 43	Fig. 44	Fig. 45
	D50 = 0.3 mm	12"	Fig. 46	Fig. 47	Fig. 48	
		14"	Fig. 49	Fig. 50	Fig. 51	
		16"	Fig. 52	Fig. 53	Fig. 54	Fig. 55
		18"	Fig. 56	Fig. 57	Fig. 58	Fig. 59
		20"	Fig. 60	Fig. 61	Fig. 62	Fig. 63
		24"	Fig. 64	Fig. 65	Fig. 66	Fig. 67

**Step 6.4: Complete the Phase 3 Scour Evaluation**

The Phase 3 Scour Evaluation involves a quantitative determination of the bridge stability. Use the Lateral Stability Analysis below.

If the bridge is stable, reclassify the bridge to complete the process.

If the bridge is unstable, go to Step 6.5.

Lateral Stability Analysis

If it is determined that a Phase 3 Scour Evaluation is required, a lateral stability analysis will be conducted. The FB Pier Program is a good tool for conducting the stability analysis. A factor of safety (or resistance factor if working in LRFD) of 1.0 should be applied to the soil parameters.

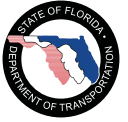
Task 1: Complete an SPT Boring

If SPT Boring data is not available for the bridge being analyzed, one must be performed to get the correct input soil parameters in order to run a lateral stability analysis. If SPT Boring data is obtained at this time, the embedment predictions should be updated with the new data before proceeding to Task 2.

Task 2: Choosing a Pile Embedment

If the bridge does not have concrete pile bents, then estimated embedments must be established using the Geotechnical method. Review the data to ensure the embedment depths provided are reasonable. The minimum embedment predicted for the bridge will be provided. Depending on the bridge characteristics and the soil data available, minimum embedment depths for each bent may also be provided. If the minimum embedment depth for the bridge is applied to the bent with the worst case scour conditions and the bent is shown to be stable, then the bridge can be considered low risk for scour. If the bent is not stable under these assumptions, then the embedment predictions per bent need to be considered in conjunction with the scour predictions for each bent to determine the worst case combination to determine the stability of the bent, and therefore the bridge. If only one embedment value, the minimum embedment for the bridge, has been provided, discuss this with the geotechnical engineer to find out if enough data is available to make a specific embedment prediction at the critical bent.

If the bridge has concrete pile bents, then estimated embedments by both the Geotechnical method and CPILE should have been provided. If the predictions by the two methods are substantially different, double check the input values to CPILE and discuss the situation with the geotechnical engineer to attempt to identify reasons that the predictions are different. After the results are validated, use the smaller of the predictions from the two methods. Do not apply a safety factor to the prediction used. Follow similar reasoning for applying the predicted minimum value per bridge and per bent as discussed in the paragraph above.



Modeling Timber Piles

Many of the bridges in Florida with unknown foundations utilize timber piles. FB Pier does not have a pre-defined timber pile. As such, it is necessary to create a custom pile material to mimic the action of timber. The properties should be as follows:

Section Type

Generally, timber piles are circular. Per the specifications, the minimum tip diameter is 8 inches and the minimum butt diameter is 12 inches. A diameter of 8 inches would be conservative if the actual diameter is not known.

Sometimes, however, the timber piles are square or rectangular, and the size of the pile should be determined during a site visit or through available documentation.

Unit Weight

The unit weight of timber should be conservatively taken as 50 pcf.

Material Properties

The material properties of timber must be input manually. Timber may be modeled as concrete with a linear stress strain curve and a slope equal to the modulus of elasticity of the material being utilized. When using concrete in FB Pier, reinforcing bars must be specified. Two mild reinforcing bars of negligible area, with the standard material properties of steel, may be used to satisfy this requirement.

If a timber bent cap is also used, additional properties are required. From *Wood Handbook – Wood as an Engineering Material* published by the US Department of Agriculture, Forest Service, Forest Products Laboratory in 1999, a reasonable value for Poisson's Ratio is 0.3. Other references that may be of use include the *National Design Specifications for Wood Construction* published by the American Forest & Paper Association and the American Wood Council and the *Timber Pile Design and Construction Manual* published by the Timber Piling Council of the American Wood Preservers Institute.

Step 6.5: Check the Warrant of Automated Monitoring

If the bridge is a High Priority Bridge (determined in Step 4.2) or if the bridge does not meet the Minimum Performance Level (determined in Step 4.3), then bypass this step and go to Step 6.6. These bridges automatically require either Non-Destructive Testing to establish the foundation dimensions or countermeasures to mitigate scour at the bridge.

Calculate the lifetime Risk of Death, using the following formula:

$$R_{\text{death}} = K_1 K_2 P_L \text{Cost}_{\text{death}}$$

K_1, K_2 Determined in Task 3 of Calculating Annual and Lifetime Risks Procedure.

P_L Lifetime Probability of Failure calculated in Task 4 of Calculating Annual and Lifetime Risks of Failure.

$\text{Cost}_{\text{death}}$ The cost of Loss of Life in Appendix A.



Compare the Risk of Death to the estimated cost of Automated Monitoring (AM) for scour. If the Risk of Death is greater than the cost of AM, then AM is provisionally warranted. Later in this process, if countermeasures are warranted then AM may not be needed.

If AM is provisionally warranted, reduce the Lifetime Risk of Failure by the amount of the Lifetime Risk of Death and perform the Phase 4 Scour Evaluation.

AM, as used in this step, does not include visual inspection.

Step 6.6: Complete the Phase 4 Scour Evaluation

The Phase 4 Scour Evaluation assesses countermeasure options to mitigate the potential scour at the bridge. Another option that will be considered for unknown foundations bridges is Non-Destructive Testing to establish the foundation dimensions—see following procedure.

As part of the countermeasure assessments, the cost of each countermeasure option will be estimated.

Step 6.7: Check the Warrant of Countermeasures

If the bridge is a High Priority Bridge, does not meet the Minimum Performance Level, or has a Lifetime Risk greater than \$100,000, then bypass this step and go to Step 6.8. These bridges automatically require either Non-Destructive Testing to establish the foundation dimensions or countermeasures to mitigate scour at the bridge.

Compare the cost of the countermeasure options from Task 4 in the Lifetime Risk of Failure Procedure (Step 4.1). If the cost of countermeasures is less than the Lifetime Risk of Failure (countermeasures are warranted), then go to Step 6.8.

Countermeasures, as used in this step, does not include AM or visual inspection.

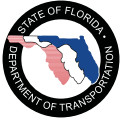
If neither countermeasures nor AM are warranted, prepare a Plan of Action that includes a bridge Closure Plan. Item 113 will remain coded as “U.”

If countermeasures were not warranted, but AM was warranted, reclassify the bridge and prepare a Closure Plan and an AM Plan as part of the Plan of Action.

Step 6.8: Check the Warrant of Non-Destructive Testing

Follow the Non-Destructive Testing Procedures to select the appropriate NDT and estimate the cost.

Compare the cost of countermeasures to the cost of NDTs and decide which should be done. It is difficult to decide the least expensive approach at this point. If the countermeasures are installed, then only the cost of countermeasures will be incurred. If the NDTs are performed and the results show that the bridge is stable for the expected scour, then only the cost of NDTs (and the stability analysis) will be incurred. However, if the results show that the bridge is not stable, then the countermeasure will be needed and the cost of both the NDTs and the countermeasures will be incurred. Assuming that the chance that the bridge is stable verses unstable is about even, then the NDTs should be performed (i.e.,



NDTs are warranted) if their cost is less than half the cost of countermeasures. However, if the cost of NDTs is greater than half the cost of countermeasures, then the countermeasures should be installed without performing the NDTs.

If in the judgment of the evaluating team the bridge is more likely to be shown stable, then the recommendation to perform NDTs could be made even if their cost is greater than half the cost of countermeasures. However, there is still a chance that the bridge will be shown to be unstable, and the cost of both NDTs and countermeasures would be incurred. Therefore, as the cost of the NDTs approaches the cost of countermeasures it is much safer to install the countermeasures and avoid doubling the cost for the bridge. And if the cost of NDTs exceeds the cost of countermeasures, then the countermeasures should be installed without performing the NDTs.

If in the judgment of the evaluating team the bridge is more likely to be shown unstable, then the recommendation could be made to rule out NDTs even if their cost is less than half the cost of countermeasures. However, as the cost becomes a small percentage of the cost of countermeasures, then even a small risk of showing the bridge to be stable is worth taking.

If NDT is warranted, perform the testing and establish the foundation dimensions. Complete the Scour Evaluation Process, including Phase 2, 3, and 4 Evaluations if needed.

If NDT is not warranted, then reclassify the bridge and prepare a Plan of Action including the installation of the countermeasures. Recheck the warrant of AM and include an AM Plan in the POA if needed.

Non-Destructive Testing Procedures

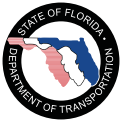
Non-Destructive Testing (NDT) methods and processes can be used to determine the depth of an unknown bridge foundation where such information is not already known. The Final Report includes detailed considerations that must be made when selecting the most appropriate NDT method. The conclusions and recommendations made in the Final Report have been developed through extensive research of existing literature, contact with experts, and with transportation agencies from other states.

Current NDT Methods

The following are NDT methods that are currently being researched or actively used by other states throughout the country:

Surface NDT Methods

- Sonic Echo
- Bending Waves (BW)
- Ultra-Seismic (US)
- Surface Wave Spectral Analysis (SW)
- Ground Penetrating Radar (GPR)
- Dynamic Foundation Response



Subsurface NDT Methods

- Parallel Seismic with Hydrophone or Geophone (PS)
- Borehole Radar (BR)
- Borehole Sonic (BS)
- Cross Hole Sonic (CS)
- Induction Field (IF)
- Borehole Magnetic (BM)

Note: Not all of the NDT methods listed will be recommended for use in Florida; please refer to the NDT recommendation flow chart Figure 1.6 for the proper application of each method.

Task 1: Selection of the Appropriate NDT Method

Selection of the most appropriate NDT method for a project will depend on several factors, including foundation type, foundation material and access limitations.

Foundation Type

Bridge foundations in Florida are influenced by the type, size, and location of the bridge structure. The majority of the bridges throughout Florida are found on non-complex foundations (i.e. driven and/or battered piles). These non-complex foundations can be tested with a fair degree of accuracy using several NDT methods. Figures 1.4 and 1.5 illustrate foundation types commonly found in Florida.

Foundation Materials

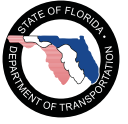
Foundations in Florida will generally consist of concrete, steel, or timber. Composites of concrete and steel are fairly typical and should be expected on many complex foundations. Steel piles may be jacketed in concrete and are a common occurrence throughout Florida. Various material types can be tested using many of the same forms of NDTs, however; the recommended NDT testing method for each material is shown in the Flow Chart, see Figure 1.6.

Access Limitations

NDT testing methods have varying degrees of site access requirements. Surface NDT will generally require access to the substructure of a bridge. This can normally be achieved using wading boots or a small boat. On larger bridges access may require some form of barge or amphibious vehicle. Subsurface NDT methods will require a soil boring or probe and therefore will be more limited at each site. Typically, a soil boring or probe can be installed through the existing bridge superstructure (i.e. bridge deck). In some situations a barge may be required to install the soil boring at the water level. The access requirements should be reviewed prior to selection of the NDT method.

Applicability Guidelines

Based on current research and test data, it is recommended that Surface NDT methods be used only when Subsurface NDT methods cannot be used or the results do not need a high degree of accuracy. The data collected and testing procedure chosen should be closely monitored by an experienced engineer familiar with the following NDT methods:



Surface NDT Methods

- *Sonic Echo*

A wave is produced by striking the foundation in question with a hammer. This wave travels through the foundation and reflects from the bottom back to the receiver. The registered signal is then used to estimate the foundation depth. Refer to ASTM D5882 and NCHRP 21-5 for further detail regarding this method.

The following should be considered:

- o Not recommended for use based on the superior performance of other NDT methods.

- *Bending Waves (BW)*

Two accelerometers are mounted near the top of a pile foundation. An induced flexural wave is created above the receiver locations, and the resulting wave dispersion is recorded through a monitoring device connected to each accelerometer. The recorded data received from the accelerometers is then used to estimate foundation depth. Refer to research by Douglas and Holt in 1993, "Determining lengths of installed timber pilings by dispersive wave propagation methods" for further detail regarding this method.

The following should be considered when selecting this method:

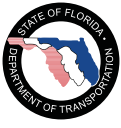
- o Best suited for use on vertically driven piles;
- o Not suitable for imaging below subsurface pile cap;
- o Jacketed steel piles should not be tested with this method;
- o Suitable for timber piles;
- o Steel and concrete are very stiff materials and may complicate the estimation procedure;
- o Stiff soils may complicate the estimation procedure; and
- o Should be used in combination with Subsurface NDT to ensure estimation validity.

- *Ultra-Seismic (US)*

An induced wave is generated near the top of the piling and the resulting wave signals are recorded in the multiple receivers mounted to the piling. The resulting compressional and flexural signal waves are used to predict foundation depth. Refer to NCHRP 21-5 for further detail regarding this method;

The following should be considered when selecting this method:

- o May be used on vertically driven or battered piles;
- o Not suitable for imaging below subsurface pile cap;
- o Jacketed steel piles should not be tested with this test method;
- o All foundation material types should be acceptable for this test;
- o Stiff soils may complicate the estimation procedure; and,
- o Should be used in combination with Subsurface NDT to ensure estimation validity.



- *Surface Wave Spectral Analysis (SW)*

A large impact is made at the existing test surface, resulting in a compressional wave within the soil or foundation medium. This resulting wave dispersion may be monitored through multiple receiver location also mounted on the test surface. Data collected from receivers may be used to estimate the depth of soil layers or foundations. Refer to ASTM D6758-02, ACI 228.2R, and NCHRP 21-5 for further detail regarding this method.

The following should be considered when selecting this method:

- o Suitable for use on large tabular foundations;
- o Not suitable for imaging below subsurface pile cap;
- o Requires a large flat surface to place receivers; and,
- o Should be used in combination with Subsurface NDT to ensure estimation validity.

- *Ground Penetrating Radar (GPR)*

Traditionally, GPR has been used to establish subsurface strata layers by dragging the radar equipment in a grid pattern over the test surface. This test registers the reflected radar signals and allows for the creation of a three (3) dimensional image of the subsurface. Refer to ASTM D6432-99 for further detail regarding this method.

The following should be considered when selecting this method:

- o Suitable for use on large tabular foundations or spread footings;
- o Not suitable for imaging below subsurface pile cap;
- o Radar signals will be obscured by the presence of salty or brackish water; and,
- o Should be used in combination with Subsurface NDT to ensure estimation validity.

- *Dynamic Foundation Response*

Development of correlations between various resonant frequencies and different known foundation types has been explored as a means of determining the existence of a complex subsurface foundation (i.e. subsurface pilecap, pile cluster, etc.). This test method is currently being explored by university researchers. Refer to NCHRP 21-5 for further detail regarding this method.

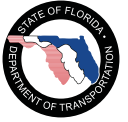
The following should be considered:

- o Not recommended for use based on a need for further research.

Subsurface NDT Methods

- *Parallel Seismic with Hydrophone or Geophone (PS)*

A cased borehole is installed parallel to the unknown foundation. A hydrophone (or geophone) is then lowered into the borehole in descending depth increments. At each depth increment an induced wave is generated from the top of the pile. For every induced wave created, the receiver records the time of first arrival for the signal to pass down through the pile and horizontally through the soil. These received signals are then used to locate the bottom of an unknown foundation. Refer to ACI 228.2R and NCHRP 21-5 for further detail regarding this method.



The following should be considered when selecting this method:

- o May be used on any type of foundation material (i.e. steel, concrete, masonry, and timber) given consideration to any site access limitations;
- o Appropriate foundation types include; vertically driven piles, battered piles, abutments, and complex foundations;
- o Thick bridge decks and pilecaps may limit the transmitted signal required for the test and complicate the interpretation of data;
- o A hydrophone or geophone may be used as a receiver inside of the cased borehole;
- o Steel casing is suitable for this test method; and,
- o Perform a secondary test to check results from the Parallel Seismic method.

- *Borehole Radar (BR)*

A cased boring is installed parallel to the unknown foundation. A radar transmitter/receiver is lowered into the borehole and a radar signal is created at descending depth increments. The reflections of the radar signal received back are analyzed to estimate foundation depth. Refer to NCHRP 21-5 for further detail regarding this method.

The following should be considered when selecting this method:

- o Suitable for foundations with a large cross-sectional area;
- o Suitable foundation materials are concrete and steel;
- o Steel casing should be avoided due to potential signal interference;
- o Brackish water may interfere with the transmission of the radar signal; and,
- o Perform a secondary test to check results from the Borehole Radar method.

- *Borehole Sonic (BS)*

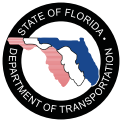
A cased borehole is installed parallel to the unknown foundation. A source transmitter is lowered incrementally into the boring in conjunction with a receiver. The source transmitter induces a sonic wave which reflects off the unknown foundation which then returns to the receiver. The received wave data is then used to estimate foundation depth. Refer to NCHRP 21-5 for further detail regarding this method.

The following should be considered when selecting this method:

- o Suitable for foundations with a large cross-sectional area;
- o Suitable foundation materials are concrete and steel; and,
- o Perform a secondary test to check results from the Borehole Sonic method.

- *Cross Hole Sonic (CS)*

Two (2) cased boreholes are installed on opposite sides of the unknown foundation with the boreholes spaced equidistant from the foundation. Once the boreholes have been installed, either a Parallel Seismic test or a Borehole Sonic test may be performed. During the test, waves are induced between the borings and monitored using receivers mounted at the same depth as the wave source. The resulting wave data collected from within the borings is used to estimate foundation depth. Refer to ASTM D6760 and NCHRP 21-5 for specification of typical application of CS.



The following should be considered when selecting this method:

- o May be used on any type of foundation material (i.e. steel, concrete, masonry, and timber) given consideration to any site access limitations;
- o Appropriate foundation types include; vertically driven piles, battered piles, abutments, complex foundations; and,
- o Perform a secondary test to check results from the Cross Hole Sonic method.

• *Induction Field (IF)*

A cased borehole is installed parallel to the unknown foundation. An electrical current is then passed through the steel pile or steel reinforcement of a concrete pile. The electrical field created by the imposed electrical current is recorded when lowering a sensor into the boring. Data collected from the sensor is then used to determine the depth of the unknown foundation. Refer to NCHRP 21-5 for further detail regarding this method.

The following should be considered when selecting this method:

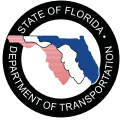
- o Suitable for use on vertically driven and battered piles;
- o Suitable foundation materials include steel and reinforced concrete;
- o If the Induction Field method is to be used on reinforced concrete, access to steel reinforcing will be required; and,
- o Perform a secondary test to check results from the Induction Field method.

• *Borehole Magnetic (BM)*

A cased borehole is installed parallel to the unknown foundation. A flux gate magnetometer is lowered into the cased borehole and the ferrous material in the foundation is tracked at descending depths until the bottom of the foundation is found. Refer to research by Jo, C.H., Cha, Y.H., in 2003, "A Borehole Magnetic Logging Tool for Estimating Unknown Foundation Depths" for further details regarding this method.

The following should be considered when selecting this method:

- o Suitable for use on steel or heavily reinforced concrete foundations;
- o Appropriate foundation types include vertically driven piles, battered piles, abutments, complex foundations;
- o Steel casing should be avoided due to potential signal interference; and,
- o Perform a secondary test to check results from the Borehole Magnetic method.



Task 2: Cost Estimation for NDT Methods

The cost of NDT testing varies from low to fairly high depending on the existing site requirements. The cost breaks down into several major categories: Maintenance of Traffic (MOT), required testing personnel, soil boring installation, testing equipment, mobilization on site, and general lab and engineering labor. Costs incurred through purchase of the testing equipment have been amortized over time. Table 1.6 includes a summary for estimating the costs. Typical general categories are:

- Maintenance of Traffic
- Mobilization
 - Truck drill/probe rig mobilization
 - NDT Equipment
 - Small amphibious drill/probe
 - Support boat
 - Pavement coring equipment
 - Large Barge for coastal application (not included)
- Drilling/probing
 - Footage for borings/probes using truck mounted equipment
 - Footage for temporary casing (if needed)
 - Grout to close boring/probe casing when complete

Task 3: NDT Recommendations

Recommendations for the selection of the appropriate NDT method are shown in the flow charts in Figure 1.6. Recommendations provided in the flow chart have been established based on the successes and failures of past research performed by university researchers and state agencies. The recommendations have been denoted as Options 1 through 4 in the NDT Flow Chart with Option 1 considered as the best available test method given the respective applicability requirements. Before any NDT method is chosen, a review of applicability requirements is needed to ensure correct usage.

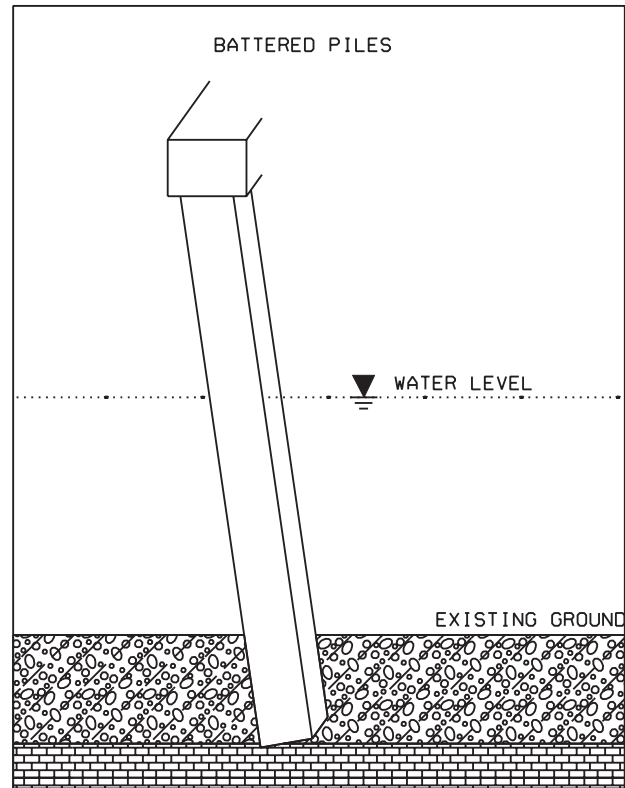
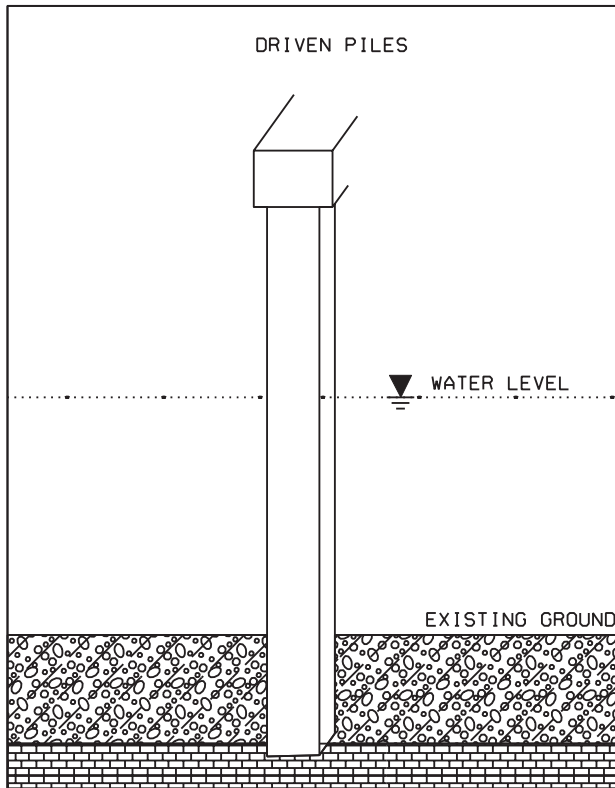
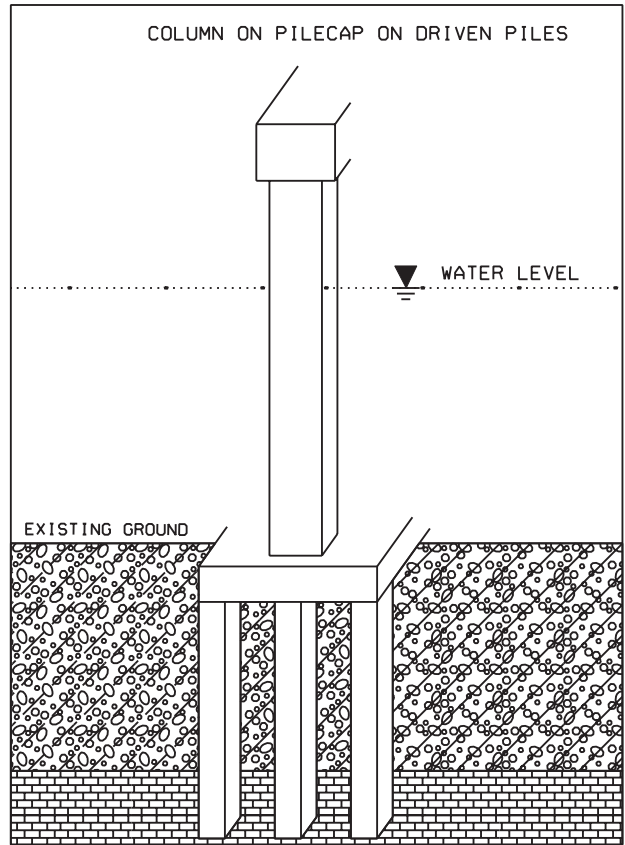
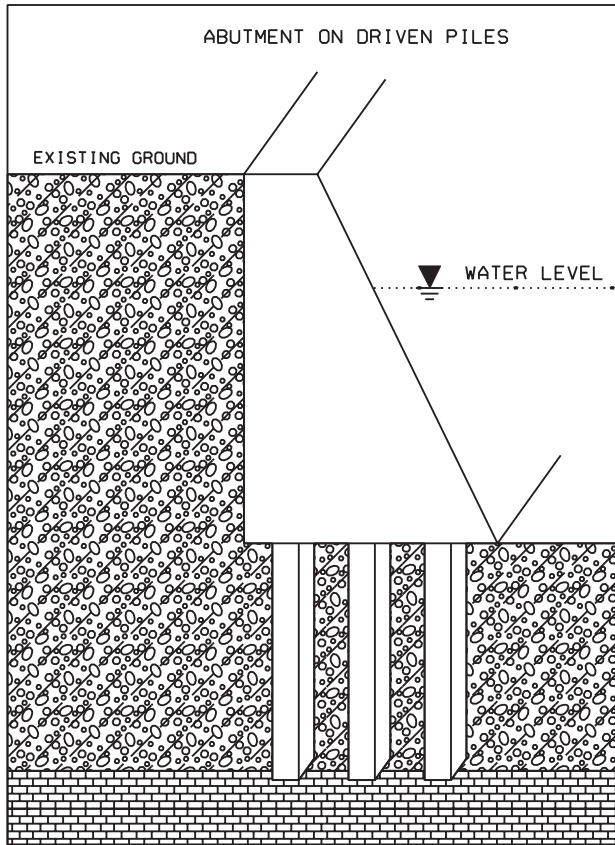


Figure 1.4: Bridge Foundation Types

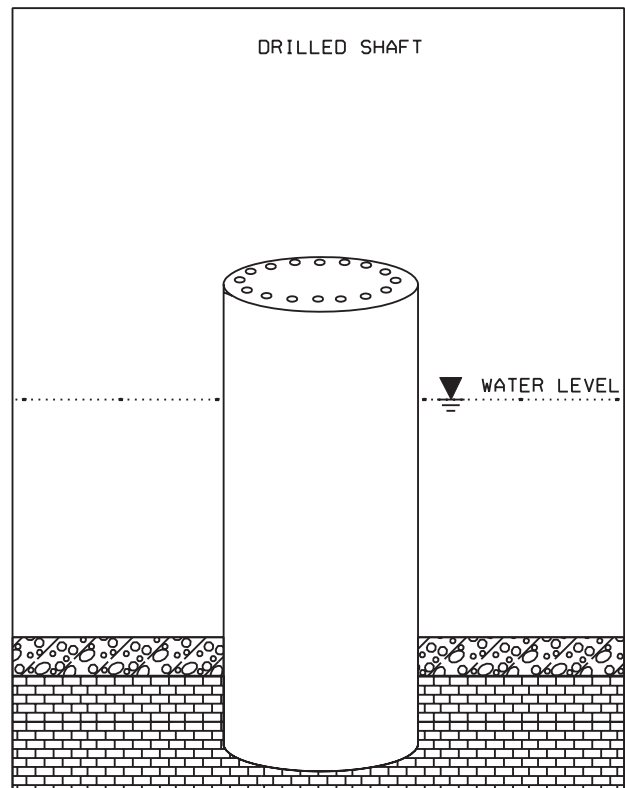
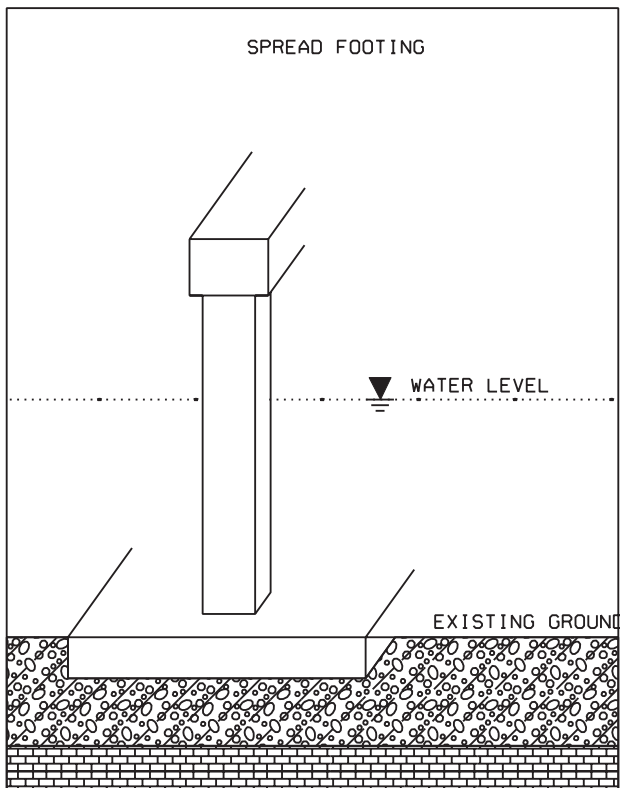
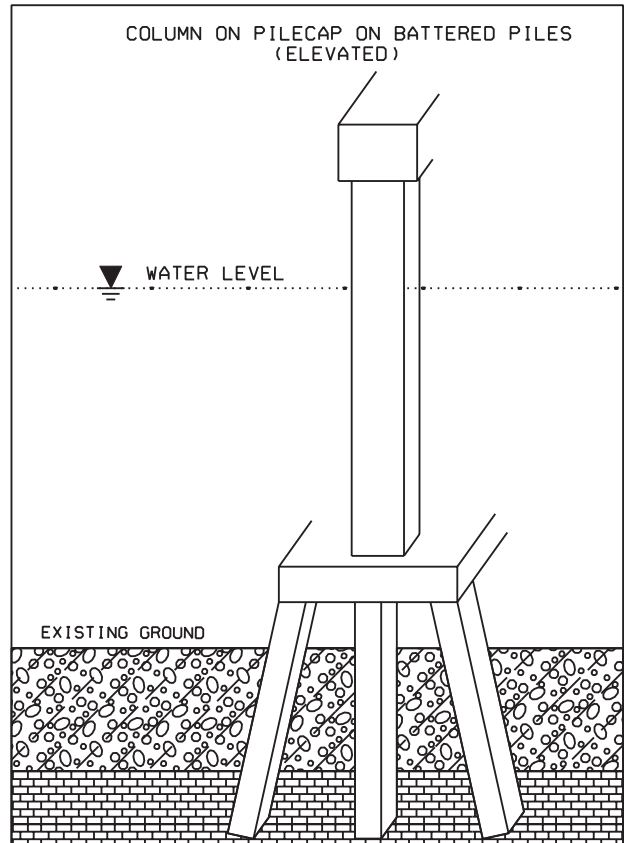
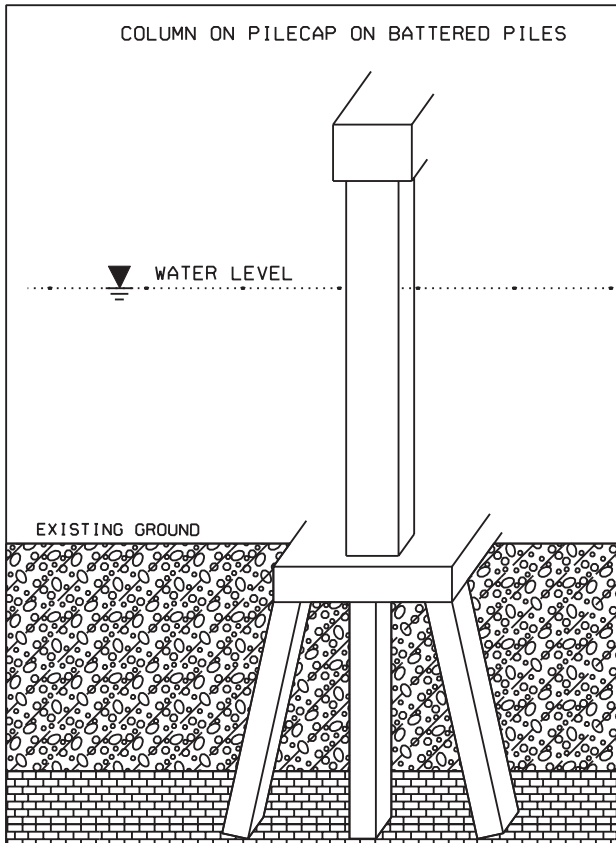
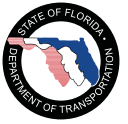


Figure 1.5: Bridge Foundation Types

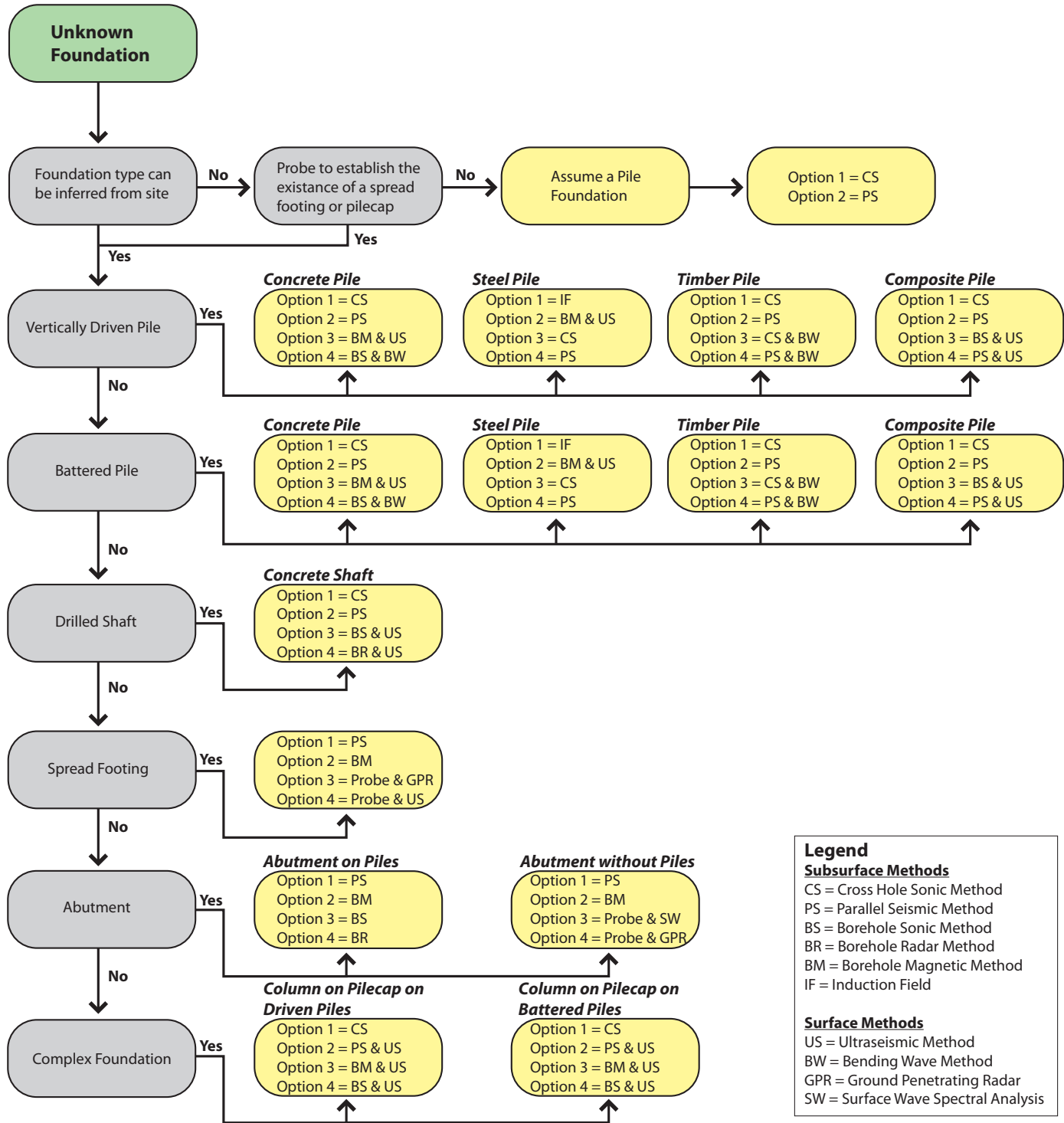
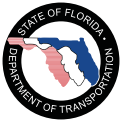


Figure 1.6: NDT Flow Chart

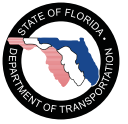
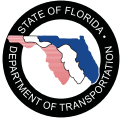


Table 1.6: Estimated Cost of NDT Methods

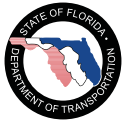
TESTING METHOD	TOTAL COST PER TEST		MOBILIZATION 1		MOT 2		TESTING EQUIPMENT 3		TESTING PERSONNEL 4		SOIL BORINGS AND/OR PROBES 5		LABORATORY AND ENGINEERING 6	
	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH	LOW	HIGH
SURFACE NDT METHODS														
SONIC ECHO	\$4,500	\$11,400	\$500	\$1,500	\$0	\$1,000	\$500	\$900	\$1,000	\$3,000	\$0	\$0	\$2,500	\$5,000
BENDING WAVES	\$4,500	\$11,400	\$500	\$1,500	\$0	\$1,000	\$500	\$900	\$1,000	\$3,000	\$0	\$0	\$2,500	\$5,000
ULTRA-SEISMIC	\$4,600	\$11,600	\$500	\$1,500	\$0	\$1,000	\$600	\$1,100	\$1,000	\$3,000	\$0	\$0	\$2,500	\$5,000
SURFACE WAVE SPECTRAL ANALYSIS	\$4,500	\$11,400	\$500	\$1,500	\$0	\$1,000	\$500	\$900	\$1,000	\$3,000	\$0	\$0	\$2,500	\$5,000
GROUND PENETRATING RADAR	\$6,000	\$14,000	\$500	\$1,500	\$0	\$1,000	\$2,000	\$3,500	\$1,000	\$3,000	\$0	\$0	\$2,500	\$5,000
DYNAMIC FOUNDATION RESPONSE	\$4,500	\$11,500	\$500	\$1,500	\$0	\$1,000	\$500	\$1,000	\$1,000	\$3,000	\$0	\$0	\$2,500	\$5,000
SUBSURFACE NDT METHODS														
PARALLEL SEISMIC TEST	\$10,000	\$22,800	\$500	\$2,000	\$1,000	\$2,500	\$500	\$1,300	\$1,000	\$3,000	\$2,000	\$4,000	\$5,000	\$10,000
BOREHOLE RADAR	\$11,500	\$25,000	\$500	\$2,000	\$1,000	\$2,500	\$2,000	\$3,500	\$1,000	\$3,000	\$2,000	\$4,000	\$5,000	\$10,000
BOREHOLE SONIC TEST	\$10,500	\$23,000	\$500	\$2,000	\$1,000	\$2,500	\$1,000	\$1,500	\$1,000	\$3,000	\$2,000	\$4,000	\$5,000	\$10,000
CROSS HOLE SONIC TEST	\$12,700	\$28,000	\$500	\$2,000	\$1,000	\$2,500	\$1,200	\$2,500	\$1,000	\$3,000	\$4,000	\$8,000	\$5,000	\$10,000
INDUCTION FIELD	\$10,000	\$22,500	\$500	\$2,000	\$1,000	\$2,500	\$500	\$1,000	\$1,000	\$3,000	\$2,000	\$4,000	\$5,000	\$10,000
BOREHOLE MAGNETIC	\$9,800	\$22,500	\$500	\$2,000	\$1,000	\$2,500	\$300	\$1,000	\$1,000	\$3,000	\$2,000	\$4,000	\$5,000	\$10,000
NOTES: 1. MOBILIZATION COSTS INCLUDE EQUIPMENT AND PERSONNEL. 2. MOT COSTS ARE FROM 0 TO 9 HOURS. 3. TESTING EQUIPMENT COSTS ARE BASED ON 5% OF THE AVERAGE COST TO PURCHASE TESTING EQUIPMENT. 4. TESTING PERSONNEL COSTS ARE BASED ON 4 TO 9 HOURS OF A FIELD ENGINEER AND TRAINED TECHNICIANS TIME. 5. SOIL BORING AND/OR PROBES COSTS INCLUDE DRILLING, CASING, GROUTING, ETC. 6. LABATORY AND ENGINEERING ESTIMATES INCLUDE DATA ANALYSIS, COMPUTATIONS AND REPORT PREPARATION WITH RECOMMENDATIONS.														



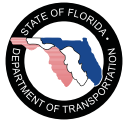
Appendix A

The following items are included in this Appendix:

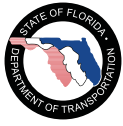
- Unknown Foundation Bridges Probabilities Of Failure And Failure Costs



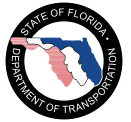
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
010004	\$1,039,658	\$7,529,184	\$2,900,000	\$11,468,842	6	S	0.00011	\$1,262	N	0.002	Y	1	23	0.002526941	\$28,981.09	T
010005	\$778,315	\$1,046,125	\$1,160,000	\$2,984,440	7	S	0.00011	\$328	N	0.002	Y	1	25	0.002746373	\$8,196.39	R
010011	\$263,520	\$614,056	\$1,160,000	\$2,037,576	4	S	0.0005	\$1,019	N	0.0001	N	1	31	0.01538431	\$31,346.70	T
010021	\$1,359,038	\$11,223,338	\$1,160,000	\$13,742,376	7	S	0.00011	\$1,512	N	0.0001	N	1	40	0.004390575	\$60,336.93	T
010032	\$2,031,338	\$687,805	\$2,900,000	\$5,619,144	7	S	0.00011	\$618	Y	0.0001	N	1	37	0.004061952	\$22,824.69	T
010033	\$789,623	\$1,047,353	\$2,900,000	\$4,736,977	6	S	0.00011	\$521	Y	0.0001	N	1	15	0.00164873	\$7,810.00	T
014017	\$408,297	\$2,204,954	\$2,900,000	\$5,513,251	6	S	0.00011	\$606	N	0.0005	Y	1	31	0.003404379	\$18,769.20	T
014022	\$334,191	\$734,985	\$2,900,000	\$3,969,176	6	S	0.00011	\$437	N	0.0002	Y	1	28	0.003075431	\$12,206.93	T
014023	\$744,486	\$477,864	\$1,160,000	\$2,382,350	6	S	0.00011	\$262	N	0.0005	Y	1	29	0.003185092	\$7,588.00	T
014026	\$792,870	\$1,190,675	\$2,900,000	\$4,883,545	6	S	0.00011	\$537	N	0.002	Y	1	30	0.003294742	\$16,090.02	M
014027	\$605,328	\$353,588	\$1,160,000	\$2,118,916	7	S	0.00011	\$233	N	0.0005	Y	1	30	0.003294742	\$6,981.28	R
014029	\$1,522,559	\$1,918,310	\$2,900,000	\$6,340,870	7	R	0.000077	\$488	N	0.0005	Y	1	30	0.002307423	\$14,631.07	T
014031	\$662,569	\$531,195	\$1,160,000	\$2,353,764	7	S	0.00011	\$259	N	0.0002	Y	1	34	0.00373322	\$8,787.12	R
014032	\$551,388	\$524,657	\$1,160,000	\$2,236,045	7	S	0.00011	\$246	N	0.0005	Y	1	34	0.00373322	\$8,347.65	T
014033	\$980,505	\$1,472,910	\$2,900,000	\$5,353,415	6	S	0.00011	\$589	N	0.002	Y	1	34	0.00373322	\$19,985.48	T
014034	\$1,298,152	\$4,887,649	\$2,900,000	\$9,085,801	6	S	0.00011	\$999	N	0.002	Y	1	34	0.00373322	\$33,919.29	T
014035	\$1,514,038	\$4,887,649	\$2,900,000	\$9,301,687	6	S	0.00011	\$1,023	N	0.002	Y	1	35	0.003842809	\$35,744.61	T
014036	\$1,264,065	\$3,529,269	\$2,900,000	\$7,693,334	6	R	0.000077	\$592	N	0.0005	Y	1	34	0.002614677	\$20,115.58	T
014037	\$1,445,863	\$2,303,828	\$2,900,000	\$6,649,692	6	R	0.000077	\$512	N	0.0002	Y	1	34	0.002614677	\$17,386.79	T
014038	\$909,701	\$1,382,710	\$1,160,000	\$3,452,411	6	S	0.00011	\$380	N	0.0002	Y	1	34	0.00373322	\$12,888.61	T
014039	\$713,700	\$595,756	\$1,160,000	\$2,469,456	7	S	0.00011	\$272	N	0.0002	Y	1	34	0.00373322	\$9,219.02	T
014040	\$574,362	\$232,750	\$1,160,000	\$1,967,112	7	S	0.00011	\$216	N	0.0002	Y	1	36	0.003952386	\$7,774.79	T
014041	\$459,490	NA	\$0	\$459,490	7	S	0.00011	\$51	N	0.0002	Y	1	36	0.003952386	\$1,816.08	T
014044	\$649,173	\$68,647	\$580,000	\$1,297,820	7	S	0.00011	\$143	N	0.0005	Y	1	36	0.003952386	\$5,129.49	T
014045	\$698,137	\$68,647	\$580,000	\$1,346,784	7	S	0.00011	\$148	N	0.0005	Y	1	36	0.003952386	\$5,323.01	T
014046	\$509,336	\$33,016	\$580,000	\$1,122,352	7	S	0.00011	\$123	N	0.002	Y	1	36	0.003952386	\$4,435.97	T
014047	\$437,520	\$33,016	\$580,000	\$1,050,536	6	S	0.00011	\$116	N	0.002	Y	1	36	0.003952386	\$4,152.12	T
014048	\$674,445	\$146,226	\$580,000	\$1,400,671	7	S	0.00011	\$154	N	0.002	Y	1	36	0.003952386	\$5,535.99	T
014049	\$754,656	\$33,016	\$580,000	\$1,367,672	6	S	0.00011	\$150	N	0.0005	Y	1	38	0.004171505	\$5,705.25	T
014050	\$754,656	\$49,033	\$580,000	\$1,383,689	6	S	0.00011	\$152	N	0.002	Y	1	38	0.004171505	\$5,772.07	T
014051	\$609,823	\$79,634	\$580,000	\$1,269,457	7	S	0.00011	\$140	N	0.002	Y	1	38	0.004171505	\$5,295.55	T
014052	\$1,372,101	\$1,773,993	\$2,900,000	\$6,046,094	6	S	0.00011	\$665	N	0.002	Y	1	38	0.004171505	\$25,221.31	T
014053	\$699,391	\$168,348	\$580,000	\$1,447,739	7	S	0.00011	\$159	N	0.0001	N	1	41	0.004500092	\$6,514.96	M
014054	\$699,391	\$91,529	\$580,000	\$1,370,920	7	S	0.00011	\$151	N	0.002	Y	1	40	0.004390575	\$6,019.13	T
014059	\$864,961	\$795,133	\$1,160,000	\$2,820,095	6	S	0.00011	\$310	N	0.002	Y	1	40	0.004390575	\$12,381.84	R
014060	\$438,872	\$506,678	\$1,160,000	\$2,105,551	6	S	0.00011	\$232	N	0.002	Y	1	40	0.004390575	\$9,244.58	R
014061	\$438,872	\$392,267	\$1,160,000	\$1,991,139	7	S	0.00011	\$219	N	0.002	Y	1	40	0.004390575	\$8,742.25	R
014063	\$445,263	\$784,534	\$1,160,000	\$2,389,798	5	S	0.00024	\$8	N	0.002	Y	1	48	0.011455266	\$27,375.77	R
014064	\$703,202	\$59,930	\$580,000	\$1,343,132	7	S	0.00011	\$148	N	0.0005	Y	1	41	0.004500092	\$6,044.22	M
014065	\$1,694,010	\$71,044	\$580,000	\$2,345,054	7	S	0.00011	\$258	N	0.002	Y	1	47	0.005156941	\$12,093.31	M
014066	\$942,547	\$318,576	\$1,160,000	\$2,421,123	7	S	0.00011	\$266	N	0.002	Y	1	47	0.005156941	\$12,485.59	T
014067	\$785,456	\$171,953	\$1,160,000	\$2,117,409	7	S	0.00011	\$233	N	0.002	Y	1	47	0.005156941	\$10,919.35	T
014068	\$961,511	\$264,780	\$1,160,000	\$2,386,291	7	S	0.00011	\$262	N	0.0002	Y	1	47	0.005156941	\$12,305.96	T
014069	\$787,602	\$103,172	\$1,160,000	\$2,050,774	7	S	0.00011	\$226	N	0.0002	Y	1	47	0.005156941	\$10,575.72	T
014070	\$694,978	\$108,963	\$580,000	\$1,383,941	6	S	0.00011	\$152	N	0.0005	Y	1	47	0.005156941	\$7,136.90	M
014071	\$694,978	\$65,378	\$580,000	\$1,340,356	7	S	0.00011	\$147	N	0.002	Y	1	47	0.005156941	\$6,912.14	M
014073	\$2,077,506	\$4,498,107	\$2,900,000	\$9,475,613	5	S	0.00024	\$32	N	0.002	Y	1	51	0.012166847	\$115,288.33	T
014074	\$2,645,875	\$2,868,118	\$2,900,000	\$8,413,993	7	S	0.00011	\$926	N	0.002	Y	1	57	0.006250727	\$52,593.58	T
014082	\$806,058	\$796,106	\$1,160,000	\$2,762,164	7	S	0.00011	\$304	N	0.002	Y	1	50	0.005485204	\$15,151.03	R
014083	\$751,978	\$858,085	\$1,160,000	\$2,770,062	7	S	0.00011	\$305	N	0.002	Y	1	50	0.005485204	\$15,194.35	R
014084	\$630,940	\$256,025	\$1,160,000	\$2,046,965	7	S	0.00011	\$225	N	0.002	Y	1	50	0.005485204	\$11,228.02	T
014091	\$751,978	\$402,243	\$1,160,000	\$2,314,221	7	S	0.00011	\$255	N	0.0002	Y	1	50	0.005485204	\$12,693.97	M
014097	\$761,412	\$367,751	\$1,160,000	\$2,289,163	7	S	0.00011	\$252	N	0.0002	Y	1	50	0.005485204	\$12,556.53	R
014098	\$365,727	\$114,635	\$1,160,000	\$1,640,362	7	S	0.00011	\$180	N	0.0005	Y	1	49	0.005375795	\$8,818.25	M
014099	\$365,727	\$229,270	\$1,160,000	\$1,754,997	6	S	0.00011	\$193	N	0.0002	Y	1	49	0.005375795	\$9,434.50	M
014100	\$365,727	\$114,635	\$1,160,000	\$1,640,362	6	S	0.00011	\$180	N	0.0005	Y	1	50	0.005485204	\$8,997.72	M
014101	\$369,277	\$114,635	\$1,160,000	\$1,643,913	6	S	0.00011	\$181	N	0.002	Y	1	51	0.005485204	\$9,017.20	R
014102	\$324,964	\$43,585	\$580,000	\$948,549	6	S	0.00011	\$104	N	0.002	Y	1	50	0.0055946	\$5,306.75	R
014103	\$324,964	\$43,585	\$580,000	\$948,549	7	S	0.00011	\$104	N	0.002	Y	1	51	0.0055946	\$5,306.75	R
014104	\$369,277	\$114,635	\$1,160,000	\$1,643,913	6	S	0.00011	\$181	N	0.002	Y	1	51	0.0055946	\$9,197.04	R
014105	\$369,277	\$114,635	\$1,160,000	\$1,643,913	6	S	0.00011	\$181	N	0.0002	Y	1	51	0.0055946	\$9,197.04	R
014106	\$369,277	\$114,635	\$1,160,000	\$1,643,913	6	S	0.00011	\$181	N	0.0005	Y	1	51	0.0055946	\$9,197.04	M
014107	\$369,277	\$95,529	\$1,160,000	\$1,624,807	6	R	0.000077	\$125	N	0.0005	Y	1	51	0.00391945	\$6,368.35	R
014108	\$324,964	\$32,689	\$580,000	\$937,653	7	S	0.00011	\$103	N	0.002	Y	1	51	0.0055946	\$5,245.79	R
014109	\$324,964	\$0	\$580,000	\$904,964	7	S	0.00011	\$100	N	0.002	Y	1	51	0.0055946	\$5,062.91	R
014110	\$369,277	\$95,529	\$1,160,000	\$1,624,807	6	S	0.00011	\$179	N	0.002	Y	1	51	0.0055946	\$9,090.15	R
014111	\$369,277	\$95,529	\$1,160,000	\$1,624,807	6	S	0.00011	\$179	N	0.002	Y	1	51	0.0055946	\$9,090.15	R
014112	\$324,964	\$22,011	\$580,000	\$926,975	6	S	0.00011	\$102	N	0.002	Y	1	51	0.0055946	\$5,186.05	R
014113	\$324,964	\$88,042	\$580,000	\$993,006	5	S	0.00024	\$3	N	0.002	Y	1	51	0.012166847	\$12,081.75	R
014123	\$367,502	\$95,529	\$1,160,000	\$1,623,031	7	S	0.00011	\$179	N	0.002	Y	1	51	0.0055946	\$9,080.21	R
015004	\$798,005	\$74,886,758	\$1,160,000	\$76,844,762	6	S	0.00011	\$8,453	Y	0.0001	N	1	52	0.005703985	\$438,321.35	T
015005	\$2,706,276	\$3,022,644	\$2,900,000	\$8,628,920	7	S	0.00011	\$949	N	0.0001	N	1	57	0.006250727	\$53,937.03	T
015006	\$															



Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
024025	\$616,940	\$6,409,067	\$2,900,000	\$9,926,007	6	S	0.00011	\$1,092	Y	0.0002	Y	1	27	0.002965757	\$29,438.12	R
024028	\$629,254	\$3,574,580	\$1,160,000	\$5,363,835	7	S	0.00011	\$590	N	0.0002	Y	1	32	0.003514005	\$18,848.54	R
024031	\$287,048	NA	\$1,160,000	\$1,447,048	6	S	0.00011	\$159	Y	0.0002	Y	1	31	0.003404379	\$4,926.30	R
024032	\$287,048	NA	\$1,160,000	\$1,447,048	6	S	0.00011	\$159	Y	0.002	Y	1	30	0.003294742	\$4,767.65	T
024040	\$53,497	NA	\$580,000	\$633,497	7	S	0.00011	\$70	Y	0.002	Y	1	41	0.004500092	\$2,850.79	R
024046	\$521,421	\$1,029,701	\$1,160,000	\$2,711,123	7	R	0.000077	\$209	N	0.0005	Y	1	53	0.004072841	\$11,041.97	R
024047	\$490,331	\$303,452	\$1,160,000	\$1,953,783	6	R	0.000077	\$150	N	0.002	Y	1	53	0.004072841	\$7,957.45	R
024048	\$599,873	\$303,452	\$1,160,000	\$2,063,325	6	R	0.000077	\$159	N	0.0005	Y	1	53	0.004072841	\$8,403.59	R
024049	\$173,745	NA	\$580,000	\$753,745	7	R	0.000077	\$58	Y	0.002	Y	1	57	0.004379551	\$3,301.06	T
024050	\$293,323	\$638,569	\$1,160,000	\$2,091,892	6	R	0.000077	\$161	N	0.002	Y	1	31	0.002384245	\$4,987.58	R
030061	\$323,945	\$10,926,448	\$1,160,000	\$12,410,393	7	S	0.00011	\$1,365	Y	0.002	Y	1	18	0.00197815	\$24,549.62	T
030065	\$432,715	\$10,926,448	\$1,160,000	\$12,519,163	7	S	0.00011	\$1,377	Y	0.002	Y	1	18	0.00197815	\$24,764.78	T
030066	\$326,310	\$10,926,448	\$1,160,000	\$12,412,758	7	S	0.00011	\$1,365	Y	0.0005	Y	1	18	0.00197815	\$24,554.29	T
030067	\$323,945	\$10,926,448	\$1,160,000	\$12,410,393	6	S	0.00011	\$1,365	Y	0.0005	Y	1	18	0.00197815	\$24,549.62	M
030068	\$432,715	\$10,926,448	\$1,160,000	\$12,519,163	7	S	0.00011	\$1,377	Y	0.002	Y	1	18	0.00197815	\$24,764.78	M
030069	\$326,310	\$10,926,448	\$1,160,000	\$12,412,758	7	S	0.00011	\$1,365	Y	0.0001	N	1	18	0.00197815	\$24,554.29	M
030070	\$430,350	\$10,926,448	\$1,160,000	\$12,516,799	7	S	0.00011	\$1,377	Y	0.0005	Y	1	18	0.00197815	\$24,760.10	M
030071	\$430,350	\$10,926,448	\$1,160,000	\$12,516,799	6	S	0.00011	\$1,377	Y	0.0005	Y	1	19	0.002087932	\$26,134.23	T
030072	\$430,350	\$10,926,448	\$1,160,000	\$12,516,799	7	S	0.00011	\$1,377	Y	0.0001	N	1	18	0.00197815	\$24,760.10	T
030073	\$430,350	\$10,926,448	\$1,160,000	\$12,516,799	6	S	0.00011	\$1,377	Y	0.0005	Y	1	18	0.00197815	\$24,760.10	T
030074	\$323,945	\$10,926,448	\$1,160,000	\$12,410,393	7	S	0.00011	\$1,365	Y	0.0002	Y	1	18	0.00197815	\$24,549.62	T
030075	\$326,310	\$10,926,448	\$1,160,000	\$12,412,758	7	S	0.00011	\$1,365	Y	0.0002	Y	1	18	0.00197815	\$24,554.29	M
030078	\$401,976	\$18,857,802	\$1,160,000	\$20,419,777	7	S	0.00011	\$2,246	Y	0.0005	Y	1	16	0.001758549	\$35,909.17	R
030083	\$1,430,677	\$18,857,802	\$1,160,000	\$21,448,479	6	S	0.00011	\$2,359	Y	0.002	Y	1	15	0.00164873	\$35,362.75	R
030086	\$678,863	\$22,399,414	\$1,160,000	\$24,238,277	7	S	0.00011	\$2,666	Y	0.001	Y	1	21	0.002307461	\$55,928.87	R
030087	\$425,621	\$22,399,414	\$1,160,000	\$23,985,035	6	S	0.00011	\$2,638	Y	0.0005	Y	1	15	0.00164873	\$39,544.85	R
030088	\$215,175	\$22,399,414	\$1,160,000	\$23,774,589	6	S	0.00011	\$2,615	Y	0.0002	Y	1	15	0.00164873	\$39,197.88	R
030092	\$279,089	\$22,399,414	\$1,160,000	\$23,838,502	7	S	0.00011	\$2,622	Y	0.0005	Y	1	15	0.00164873	\$39,303.26	R
030100	\$465,233	\$10,635,180	\$1,160,000	\$12,260,413	6	S	0.00011	\$1,349	Y	0.0005	Y	1	15	0.00164873	\$20,214.11	R
030101	\$228,309	\$10,635,180	\$1,160,000	\$12,023,489	7	S	0.00011	\$1,323	Y	0.0005	Y	1	15	0.00164873	\$19,823.49	R
030123	\$1,719,341	\$5,879,878	\$2,900,000	\$10,499,219	6	S	0.00011	\$1,155	N	0.0001	N	1	37	0.004061952	\$42,647.32	R
030125	\$884,955	\$1,786,013	\$2,900,000	\$5,570,968	6	R	0.000077	\$429	N	0.0001	Y	1	41	0.003152143	\$17,560.49	T
030135	\$1,141,732	\$539,367	\$1,160,000	\$2,841,100	6	S	0.00011	\$313	N	0.0005	Y	1	37	0.004061952	\$11,540.41	R
030136	\$195,533	\$12,763,685	\$1,160,000	\$14,119,218	6	S	0.00011	\$1,553	N	0.0005	Y	1	15	0.00164873	\$55,928.87	R
030137	\$278,597	\$8,812,037	\$1,160,000	\$10,250,634	5	S	0.00024	\$35	N	0.0005	Y	1	15	0.003593958	\$36,840.35	R
030138	\$642,763	\$8,812,037	\$1,160,000	\$10,614,800	6	S	0.00011	\$1,168	N	0.0005	Y	1	15	0.00164873	\$17,500.94	R
030139	\$572,739	\$7,880,965	\$1,160,000	\$9,613,704	6	S	0.00011	\$1,058	N	0.0005	Y	1	15	0.00164873	\$15,850.40	R
030140	\$762,279	\$7,880,965	\$1,160,000	\$9,803,243	6	S	0.00011	\$1,078	N	0.0005	Y	1	15	0.00164873	\$16,162.90	R
030141	\$370,464	\$7,880,965	\$1,160,000	\$9,411,429	6	S	0.00011	\$1,035	N	0.002	Y	1	15	0.00164873	\$15,516.91	R
030145	\$2,001,777	\$170,659	\$1,160,000	\$3,332,436	7	S	0.00011	\$367	Y	0.002	Y	1	35	0.003842809	\$12,805.92	T
030146	\$2,001,777	\$170,659	\$1,160,000	\$3,332,436	7	S	0.00011	\$367	Y	0.0005	Y	1	35	0.003842809	\$12,805.92	T
030147	\$555,227	\$562,926	\$580,000	\$1,698,153	6	S	0.00011	\$187	N	0.0005	Y	1	37	0.004061952	\$6,897.82	R
030149	\$2,834,852	\$1,102,477	\$2,900,000	\$6,837,330	7	S	0.00011	\$752	Y	0.0005	Y	1	35	0.003842809	\$26,274.55	T
030157	\$168,001	\$4,278,165	\$1,160,000	\$5,606,166	7	S	0.00011	\$617	N	0.0005	Y	1	21	0.002307461	\$12,936.01	R
030158	\$249,080	\$129,004	\$580,000	\$958,084	7	S	0.00011	\$105	N	0.0005	Y	1	19	0.002087932	\$2,000.41	R
030160	\$1,418,425	\$4,045,355	\$2,900,000	\$8,363,780	7	S	0.00011	\$920	Y	0.0005	Y	1	21	0.002307461	\$19,299.09	R
030161	\$1,470,945	NA	\$1,160,000	\$2,630,945	5	S	0.00024	\$9	Y	0.001	Y	1	21	0.005027922	\$13,228.19	T
030174	\$3,906,038	\$6,574,538	\$2,900,000	\$13,380,576	7	S	0.00011	\$1,472	Y	0.001	Y	1	39	0.004281046	\$57,282.86	R
030207	\$1,997,282	\$3,401,511	\$2,900,000	\$8,298,793	7	S	0.00011	\$913	Y	0.001	Y	1	45	0.00493804	\$40,979.77	T
030208	\$631,642	\$1,885,809	\$2,900,000	\$5,417,451	7	S	0.00011	\$596	Y	0.001	Y	1	29	0.003185092	\$17,255.08	T
030209	\$631,642	\$754,323	\$2,900,000	\$4,285,966	7	S	0.00011	\$471	Y	0.001	Y	1	37	0.004061952	\$17,409.39	T
030210	\$659,170	NA	\$1,160,000	\$1,819,170	7	S	0.00011	\$200	Y	0.002	Y	1	51	0.0055946	\$10,177.53	T
030940	\$436,999	\$10,922,166	\$1,160,000	\$12,519,165	7	S	0.00011	\$1,377	Y	0.002	Y	1	21	0.002307461	\$28,887.48	T
030951	\$428,431	\$10,922,166	\$1,160,000	\$12,510,596	7	S	0.00011	\$1,376	Y	0.001	Y	1	20	0.002197703	\$27,494.57	T
034006	\$368,263	\$25,062	\$580,000	\$973,324	6	S	0.00011	\$107	N	0.002	Y	1	33	0.003623618	\$3,526.95	R
034008	\$556,000	\$22,011	\$580,000	\$1,158,010	6	S	0.00011	\$127	N	0.002	Y	1	33	0.003623618	\$4,196.19	R
034009	\$120,711	\$23,362	\$580,000	\$724,074	6	R	0.000077	\$56	N	0.001	Y	1	33	0.002537872	\$1,837.61	R
034011	\$587,531	\$55,407	\$1,160,000	\$1,802,938	6	S	0.00011	\$198	N	0.001	Y	1	44	0.004828571	\$8,705.61	R
034012	\$264,784	\$0	\$1,160,000	\$1,424,784	6	S	0.00011	\$157	N	0.001	Y	1	31	0.003404379	\$4,850.51	R
034014	\$382,802	\$1,847,101	\$1,160,000	\$3,389,903	7	S	0.00011	\$373	N	0.001	Y	1	26	0.002856071	\$9,681.80	R
034017	\$587,531	\$55,407	\$1,160,000	\$1,802,938	6	S	0.00011	\$198	N	0.0005	Y	1	44	0.004828571	\$8,705.61	R
034019	\$682,211	\$108,903	\$1,160,000	\$1,951,115	7	S	0.00011	\$215	N	0.001	Y	1	31	0.003404379	\$6,642.34	R
034020	\$262,747	NA	\$1,160,000	\$1,422,747	6	S	0.00011	\$157	Y	0.001	Y	1	31	0.003404379	\$4,843.57	R
034021	\$704,663	NA	\$1,160,000	\$1,864,663	6	S	0.00011	\$205	Y	0.001	Y	1	31	0.003404379	\$6,348.02	R
034026	\$614,084	\$679,469	\$1,160,000	\$2,453,553	6	S	0.00011	\$270	Y	0.001	Y	1	26	0.002856071	\$7,007.52	R
034028	\$302,477	\$679,469	\$1,160,000	\$2,141,946	6	S	0.00011	\$236	N	0.001	Y	1	26	0.002856071	\$6,117.55	R
034030	\$570,655	\$300,917	\$1,160,000	\$2,031,573	7	R	0.000077	\$156	N	0.002	Y	1	31	0.002384245	\$4,843.77	R
034032	\$352,226	\$1,715,165	\$1,160,000	\$3,227,391	7	S	0.00011	\$355	N	0.0005	Y	1	26	0.002856071	\$9,217.66	R
034036	\$694,057	\$266,415	\$1,160,000	\$2,120,472	7	S	0.00011	\$233	N	0.002	Y	1	32	0.003514005	\$7,451.35	R
034042	\$511,551	\$98,067	\$580,000	\$1,189,618	7	S	0.00011	\$131	N	0.0005	Y	1	31	0.003404379	\$4,049.91	R
034044	\$575,221	\$516,330	\$1,160,000	\$2,251,551	7	S	0.00011	\$248	N	0.001	Y	1	31	0.00340437		



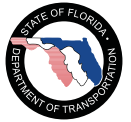
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
034103	\$589,783	\$131,787	\$1,160,000	\$1,881,570	6	S	0.00011	\$207	N	0.001	Y	1	33	0.003623618	\$6,818.09	R
034105	\$490,986	\$269,000	\$1,160,000	\$1,919,986	7	S	0.00011	\$211	N	0.001	Y	1	33	0.003623618	\$6,957.30	R
034106	\$573,582	\$245,167	\$1,160,000	\$1,978,749	7	S	0.00011	\$218	N	0.001	Y	1	33	0.003623618	\$7,170.23	R
034107	\$380,476	\$189,148	\$1,160,000	\$1,729,624	7	S	0.00011	\$190	N	0.001	Y	1	46	0.005047497	\$8,730.27	R
034108	\$502,567	\$209,475	\$1,160,000	\$1,872,042	7	S	0.00011	\$206	N	0.002	Y	1	34	0.00373322	\$6,988.74	R
034112	\$1,877,678	NA	\$580,000	\$2,457,678	6	S	0.00011	\$270	Y	0.002	Y	1	39	0.004281046	\$10,521.43	T
034113	\$711,710	\$735,501	\$1,160,000	\$2,607,211	7	S	0.00011	\$287	N	0.001	Y	1	33	0.003623618	\$9,447.54	T
034116	\$525,257	NA	\$1,160,000	\$1,685,257	5	S	0.00024	\$6	Y	0.001	Y	1	38	0.009079324	\$15,301.50	T
034117	\$951,116	\$314,252	\$1,160,000	\$2,425,368	6	S	0.00011	\$267	N	0.001	Y	1	38	0.004171505	\$10,117.43	T
034118	\$834,456	\$314,252	\$1,160,000	\$2,308,709	7	S	0.00011	\$254	N	0.001	Y	1	38	0.004171505	\$9,630.79	T
034119	\$685,021	NA	\$1,160,000	\$1,845,021	7	S	0.00011	\$203	Y	0.0005	Y	1	38	0.004171505	\$7,696.51	T
034120	\$939,691	\$251,402	\$1,160,000	\$2,351,093	7	S	0.00011	\$259	N	0.0005	Y	1	38	0.004171505	\$9,807.60	T
034122	\$209,642	NA	\$0	\$209,642	6	S	0.00011	\$23	Y	0.001	Y	1	33	0.003623618	\$759.66	T
034124	\$3,174,038	\$3,307,432	\$2,900,000	\$9,381,470	6	S	0.00011	\$1,032	N	0.001	Y	1	51	0.0055946	\$52,485.57	T
034127	\$473,147	NA	\$1,160,000	\$1,633,147	5	S	0.00024	\$6	Y	0.001	Y	1	52	0.012403927	\$20,257.44	T
035250	\$1,499,835	\$1,278,874	\$2,900,000	\$5,678,708	6	R	0.000077	\$437	N	0.001	Y	1	31	0.002384245	\$13,539.43	T
035252	\$253,383	\$169,546	\$1,160,000	\$1,582,928	8	O	0.0000085	\$13	Y	0.002	Y	1	71	0.00606332	\$955.01	M
040004	\$5,576,995	\$3,835,597	\$1,160,000	\$10,572,592	6	R	0.000077	\$814	N	0.0005	Y	1	25	0.001923222	\$20,333.45	R
040025	\$2,021,068	\$3,068,477	\$1,160,000	\$6,249,546	7	S	0.00011	\$687	N	0.0005	Y	1	25	0.002746373	\$17,163.58	R
044006	\$110,204	\$133,427	\$580,000	\$823,631	6	S	0.00011	\$91	N	0.0005	Y	1	36	0.003952386	\$3,255.31	R
044010	\$670,178	\$1,062,165	\$1,160,000	\$2,892,343	6	S	0.00011	\$318	N	0.0005	Y	1	36	0.003952386	\$11,431.66	R
044012	\$818,092	\$1,215,589	\$1,160,000	\$3,193,681	7	S	0.00011	\$351	N	0.002	Y	1	36	0.003952386	\$12,622.66	R
044014	\$755,274	\$220,880	\$580,000	\$1,556,153	6	O	0.00017	\$265	N	0.001	Y	1	49	0.008296104	\$12,910.01	R
044021	\$58,046	\$22,011	\$580,000	\$660,057	6	S	0.00011	\$73	N	0.002	Y	1	26	0.002856071	\$1,885.17	R
044031	\$513,851	\$457,377	\$580,000	\$1,551,229	6	S	0.00011	\$171	N	0.002	Y	1	50	0.005485204	\$8,508.81	R
044032	\$145,838	\$24,045	\$0	\$169,883	6	S	0.00011	\$19	N	0.001	Y	1	51	0.0055946	\$950.43	R
044033	\$212,168	\$65,378	\$580,000	\$857,545	6	S	0.00011	\$94	N	0.0005	Y	1	51	0.0055946	\$4,797.62	R
044034	\$262,986	\$42,219	\$580,000	\$885,206	4	R	0.0004	\$354	N	0.001	Y	1	52	0.020589247	\$18,225.73	R
044035	\$160,422	\$49,687	\$580,000	\$790,109	6	S	0.00011	\$87	N	0.001	Y	1	52	0.005703985	\$4,506.77	R
044036	\$63,804	\$30,646	\$0	\$94,450	4	S	0.0005	\$47	N	0.001	Y	1	15	0.007473807	\$705.90	R
044039	\$151,185	\$33,451	\$580,000	\$764,636	7	R	0.000077	\$59	N	0.002	Y	1	59	0.00453287	\$3,466.00	R
044040	\$137,863	\$20,431	\$0	\$158,293	6	S	0.00011	\$17	N	0.002	Y	1	59	0.00646934	\$1,024.05	R
050011	\$2,150,932	\$17,407,881	\$1,160,000	\$20,718,813	7	S	0.00011	\$2,279	Y	0.002	Y	1	26	0.002856071	\$59,174.40	R
050018	\$1,654,210	\$17,407,881	\$1,160,000	\$20,222,091	7	S	0.00011	\$2,224	Y	0.002	Y	1	26	0.002856071	\$57,755.73	R
050022	\$421,725	\$70,087	\$580,000	\$1,071,812	7	R	0.000077	\$83	N	0.002	Y	1	31	0.002384245	\$2,555.46	R
050031	\$406,096	\$10,672,380	\$1,160,000	\$12,238,476	7	S	0.00011	\$1,346	Y	0.002	Y	1	15	0.00164873	\$20,177.94	R
050032	\$537,528	\$10,672,380	\$1,160,000	\$12,369,908	7	S	0.00011	\$1,361	Y	0.0001	N	1	15	0.00164873	\$20,394.64	R
050033	\$1,540,009	\$10,672,380	\$1,160,000	\$13,372,389	7	S	0.00011	\$1,471	Y	0.0001	N	1	15	0.00164873	\$22,047.46	R
050035	\$544,669	\$10,672,380	\$1,160,000	\$12,377,049	7	S	0.00011	\$1,361	Y	0.0001	N	1	15	0.00164873	\$20,406.41	R
050052	\$1,053,850	\$672,705	\$580,000	\$2,306,555	6	R	0.000077	\$178	N	0.0001	Y	1	43	0.003305562	\$7,624.67	R
050053	\$642,220	\$672,705	\$580,000	\$1,894,924	7	S	0.00011	\$208	N	0.0001	N	1	43	0.00471909	\$8,942.32	R
050062	\$1,245,398	\$25,333,166	\$1,160,000	\$27,738,565	7	S	0.00011	\$3,051	Y	0.0001	N	1	56	0.006141403	\$170,353.70	R
050070	\$639,284	\$1,099,169	\$580,000	\$2,318,453	6	S	0.00011	\$255	N	0.0001	N	1	44	0.004828571	\$11,194.81	R
054002	\$521,234	\$40,861	\$580,000	\$1,142,095	6	S	0.00011	\$126	N	0.0001	N	1	18	0.00197815	\$2,259.23	R
054011	\$146,540	NA	\$0	\$146,540	6	R	0.000077	\$11	N	0.0001	Y	1	28	0.00215376	\$315.61	R
054012	\$147,180	NA	\$0	\$147,180	7	S	0.00011	\$16	Y	0.0001	N	1	28	0.003075431	\$452.64	R
054014	\$147,180	NA	\$0	\$147,180	5	S	0.00024	\$1	Y	0.0001	N	1	28	0.006698272	\$985.85	R
054015	\$649,207	\$37,528	\$580,000	\$1,266,736	6	S	0.00011	\$139	N	0.0001	N	1	24	0.002636663	\$3,339.96	R
054016	\$279,908	NA	\$0	\$279,908	7	S	0.00011	\$31	N	0.0001	N	1	21	0.002307461	\$645.88	R
054017	\$198,398	\$140,562	\$580,000	\$918,961	7	R	0.000077	\$71	N	0.0001	Y	1	52	0.003996148	\$3,672.30	R
060002	\$1,585,833	\$14,428,008	\$2,900,000	\$18,913,841	7	S	0.00011	\$2,081	Y	0.0001	N	1	21	0.002307461	\$43,642.95	R
060022	\$1,411,464	\$10,570,009	\$2,900,000	\$14,881,473	7	S	0.00011	\$1,637	Y	0.0001	N	1	22	0.002417207	\$35,971.60	R
060029	\$894,788	\$1,822,918	\$1,160,000	\$3,877,706	6	S	0.00011	\$427	N	0.0001	N	1	26	0.002856071	\$11,075.00	R
060030	\$1,454,768	\$579,410	\$1,160,000	\$3,194,178	5	R	0.00018	\$10	N	0.0001	N	1	36	0.00645963	\$20,633.21	R
060032	\$453,130	\$445,943	\$1,160,000	\$2,059,073	7	S	0.00011	\$226	N	0.0001	N	1	36	0.003952386	\$8,138.25	R
060036	\$624,347	\$1,107,440	\$580,000	\$2,311,787	6	S	0.00011	\$254	N	0.0001	N	1	19	0.002087932	\$4,826.85	R
060040	\$1,128,200	\$402,999	\$1,160,000	\$2,691,199	7	S	0.00011	\$296	N	0.002	Y	1	27	0.002965757	\$7,981.44	R
064004	\$142,248	\$177,337	\$0	\$319,586	6	R	0.000077	\$25	N	0.002	Y	1	50	0.003842746	\$1,228.09	R
064017	\$227,980	\$951,305	\$580,000	\$1,759,284	6	S	0.00011	\$194	Y	0.0005	Y	1	45	0.00493804	\$8,687.41	R
064033	\$107,303	NA	\$580,000	\$687,303	4	S	0.0005	\$344	N	0.0005	N	1	36	0.017843389	\$12,263.81	R
064034	\$217,043	\$1,241,252	\$580,000	\$2,038,295	6	S	0.00011	\$224	N	0.0005	Y	1	41	0.004500092	\$9,172.52	R
064035	\$174,139	\$142,139	\$580,000	\$896,278	6	S	0.00011	\$99	N	0.0005	Y	1	36	0.003952386	\$3,542.44	R
064040	\$83,284	\$86,626	\$580,000	\$749,910	7	S	0.00011	\$82	N	0.0005	Y	1	58	0.00636004	\$4,769.46	R
064047	\$514,679	\$705,593	\$1,160,000	\$2,380,271	6	S	0.00011	\$262	N	0.0005	Y	1	41	0.004500092	\$10,711.44	R
064054	\$509,317	\$1,251,981	\$1,160,000	\$2,921,299	6	S	0.00011	\$321	N	0.0005	Y	1	43	0.00471909	\$13,785.87	R
064083	\$119,458	\$70,718	\$580,000	\$770,176	6	S	0.00011	\$85	N	0.0001	N	1	51	0.0055946	\$4,308.83	R
064084	\$190,965	\$40,861	\$580,000	\$811,826	7	S	0.00011	\$89	N	0.0001	N	1	51	0.0055946	\$4,541.84	R
064085	\$99,421	\$36,389	\$0	\$135,810	4	S	0.0005	\$68	N	0.002	Y	1	51	0.025183838	\$3,420.22	R
064086	\$272,120	\$156,362	\$580,000	\$1,008,482	7	S	0.00011	\$111	N	0.0002	Y	1	52	0.005703985	\$5,752.37	R
064088	\$79,537	\$31,463	\$0	\$111,000	6	S	0.00011	\$12	N	0.002	Y	1	52	0.005703985	\$633.14	R
064089	\$221,250	\$216,492	\$580,000	\$1,017,742	7	S	0.00011	\$112	N	0.0005	Y	1	53	0.005813357	\$5,916.50	R
064094	\$413,603	\$32,682	\$0	\$446,286	7	S	0.00011	\$49	N	0.0005	Y	1	56	0.006141403	\$2,740.82	R
064097	\$398,651	\$444,255	\$580,000	\$1,422,906	7	S	0.00011	\$157	N	0.0005	Y	1	56	0.006141403	\$8,738.64	R
064098	\$136,283	\$115,537														



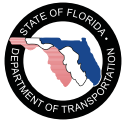
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
064110	\$81,602	\$138,849	\$580,000	\$800,450	6	S	0.00011	\$88	N	0.0001	N	1	57	0.006250727	\$5,003.39	R
064111	\$505,164	\$319,426	\$580,000	\$1,404,590	6	S	0.00011	\$155	N	0.002	Y	1	57	0.006250727	\$8,779.71	R
064112	\$440,817	\$161,837	\$580,000	\$1,182,654	7	S	0.00011	\$130	N	0.002	Y	1	58	0.00636004	\$7,521.73	R
070011	\$872,313	\$5,074,789	\$1,160,000	\$7,107,102	7	S	0.00011	\$782	N	0.002	Y	1	27	0.002965757	\$21,077.94	R
070034	\$661,551	\$3,104,044	\$1,160,000	\$4,925,595	7	S	0.00011	\$542	Y	0.002	Y	1	20	0.002197703	\$10,824.99	R
074018	\$284,684	\$2,793,640	\$1,160,000	\$4,238,324	7	S	0.00011	\$466	Y	0.002	Y	1	52	0.005703985	\$24,175.34	R
074019	\$242,023	NA	\$580,000	\$822,023	7	S	0.00011	\$90	Y	0.002	Y	1	52	0.005703985	\$4,688.81	R
074023	\$133,090	\$123,071	\$580,000	\$836,161	6	R	0.000077	\$64	N	0.002	Y	1	55	0.004226207	\$3,533.79	R
074024	\$523,774	\$269,990	\$1,160,000	\$1,953,764	7	S	0.00011	\$215	N	0.002	Y	1	53	0.005813357	\$11,357.93	R
074030	\$84,562	NA	\$0	\$84,562	6	S	0.00011	\$9	Y	0.002	Y	1	46	0.005047497	\$426.83	R
080028	\$1,266,609	\$1,812,275	\$1,160,000	\$4,238,884	6	S	0.00011	\$466	Y	0.002	Y	1	50	0.005485204	\$23,251.14	T
080031	\$859,670	\$5,638,841	\$1,160,000	\$7,658,512	7	S	0.00011	\$842	Y	0.002	Y	1	51	0.0055946	\$42,846.31	T
084007	\$195,686	NA	\$580,000	\$775,686	7	O	0.00017	\$132	Y	0.002	Y	1	48	0.008127486	\$6,304.38	T
084008	\$146,977	NA	\$1,160,000	\$1,306,977	6	S	0.00011	\$144	N	0.002	Y	1	45	0.004938004	\$6,453.90	T
090004	\$2,391,907	\$1,008,787	\$2,900,000	\$6,300,693	6	S	0.00011	\$693	Y	0.002	Y	1	34	0.00373322	\$23,521.87	R
090010	\$742,613	\$3,667,810	\$1,160,000	\$5,570,423	7	S	0.00011	\$613	N	0.002	Y	1	25	0.002746373	\$15,298.46	R
090015	\$284,309	\$1,451,821	\$1,160,000	\$2,896,131	7	S	0.00011	\$319	N	0.002	Y	1	20	0.002197703	\$6,364.83	R
090028	\$2,200,213	\$1,253,271	\$2,900,000	\$6,353,485	7	S	0.00011	\$699	Y	0.002	Y	1	35	0.003842809	\$24,415.23	R
090047	\$1,941,750	\$1,688,778	\$1,160,000	\$4,790,528	7	R	0.000077	\$369	N	0.002	Y	1	48	0.00368932	\$17,673.79	R
094001	\$270,197	\$70,366	\$580,000	\$920,563	7	S	0.00011	\$101	N	0.002	Y	1	42	0.004609597	\$4,243.42	R
094006	\$219,444	\$154,226	\$1,160,000	\$1,533,670	6	S	0.00011	\$169	N	0.002	Y	1	41	0.004500092	\$6,901.66	R
094007	\$310,062	\$527,215	\$1,160,000	\$1,997,277	7	S	0.00011	\$220	N	0.002	Y	1	40	0.004390575	\$8,769.19	R
094011	\$75,713	\$32,282	\$580,000	\$687,995	7	S	0.00011	\$76	N	0.002	Y	1	41	0.004500092	\$3,096.04	R
094012	\$127,871	\$32,282	\$580,000	\$740,153	7	S	0.00011	\$81	N	0.002	Y	1	42	0.004609597	\$3,411.81	R
094013	\$255,029	\$246,762	\$1,160,000	\$1,661,791	7	S	0.00011	\$183	N	0.0005	Y	1	41	0.004500092	\$7,478.21	R
094014	\$153,949	\$42,477	\$580,000	\$776,426	7	S	0.00011	\$85	N	0.0005	Y	1	41	0.004500092	\$3,493.99	R
094015	\$104,727	\$42,477	\$580,000	\$727,204	7	S	0.00011	\$80	N	0.0005	Y	1	41	0.004500092	\$3,272.49	R
094019	\$219,444	\$102,818	\$1,160,000	\$1,482,261	7	S	0.00011	\$163	N	0.0005	Y	1	40	0.004390575	\$6,507.98	R
094026	\$493,234	\$4,304,071	\$2,900,000	\$7,697,305	7	R	0.000077	\$593	N	0.002	Y	1	26	0.002000074	\$15,395.18	R
094031	\$370,272	NA	\$580,000	\$950,272	6	S	0.00011	\$105	Y	0.002	Y	1	31	0.003404379	\$3,235.09	R
094034	\$97,517	\$1,327	\$0	\$98,844	7	S	0.00011	\$11	N	0.002	Y	1	26	0.002856071	\$282.31	R
094036	\$76,554	\$32,282	\$580,000	\$688,836	7	S	0.00011	\$76	N	0.002	Y	1	42	0.004609597	\$3,175.26	R
094037	\$932,340	\$5,541,303	\$1,160,000	\$7,633,643	6	S	0.00011	\$840	N	0.0005	Y	1	47	0.005156941	\$39,366.25	R
094044	\$270,130	\$1,027,730	\$1,160,000	\$2,457,860	7	S	0.00011	\$270	N	0.002	Y	1	56	0.006141403	\$15,094.71	R
100001	\$3,823,879	\$5,356,926	\$2,900,000	\$12,080,805	7	S	0.00011	\$1,329	Y	0.002	Y	1	15	0.00164873	\$19,917.99	T
100026	\$1,855,315	\$2,636,605	\$1,160,000	\$5,651,920	6	S	0.00011	\$622	N	0.002	Y	1	29	0.003185092	\$18,001.89	R
100030	\$2,360,660	\$888,450	\$2,900,000	\$6,149,110	7	R	0.000077	\$473	N	0.002	Y	1	33	0.002537872	\$15,605.65	T
100039	\$9,674,945	\$563,116	\$2,900,000	\$13,138,061	7	S	0.00011	\$1,445	Y	0.002	Y	1	37	0.004061952	\$53,366.17	T
100100	\$42,523,495	\$4,814,341	\$2,900,000	\$50,237,837	7	S	0.00011	\$5,526	Y	0.002	Y	1	15	0.00164873	\$82,828.63	M
100106	\$1,946,932	\$965,061	\$2,900,000	\$5,811,993	6	S	0.00011	\$639	Y	0.002	Y	1	15	0.00164873	\$9,582.41	T
100248	\$2,052,783	\$7,783,489	\$2,900,000	\$12,736,272	7	S	0.00011	\$1,401	N	0.002	Y	1	39	0.004281046	\$54,524.57	R
100260	\$588,448	\$1,023,185	\$1,160,000	\$2,771,633	3	S	0.0013	\$3,603	N	0.002	Y	1	20	0.025681391	\$71,179.39	R
100262	\$1,501,146	\$894,580	\$2,900,000	\$5,295,725	6	S	0.00011	\$583	Y	0.002	Y	1	26	0.002856071	\$15,124.97	R
100263	\$1,188,181	\$962,830	\$2,900,000	\$5,051,011	6	S	0.00011	\$556	N	0.0005	Y	1	26	0.002856071	\$14,426.05	R
100265	\$346,186	\$3,096,093	\$1,160,000	\$4,602,279	6	S	0.00011	\$506	N	0.0005	Y	1	31	0.003404379	\$15,667.90	R
100271	\$1,446,269	\$1,146,576	\$2,900,000	\$5,492,845	6	S	0.00011	\$604	N	0.002	Y	1	20	0.002197703	\$12,071.64	R
100276	\$7,230,971	\$7,001,883	\$2,900,000	\$17,132,855	6	S	0.00011	\$1,885	N	0.0005	Y	1	27	0.002965757	\$50,811.88	R
100301	\$59,144,329	\$47,924,778	\$2,900,000	\$109,969,107	6	S	0.00011	\$12,097	Y	0.0005	Y	1	40	0.004390575	\$482,827.63	T
100433	\$5,030,758	\$589,218	\$1,160,000	\$6,779,976	7	R	0.000077	\$522	N	0.001	Y	1	46	0.003535887	\$23,973.12	R
100500	\$13,695,262	\$7,887,325	\$2,900,000	\$24,482,587	7	S	0.00011	\$2,693	Y	0.002	Y	0.67	26	0.002856071	\$69,924.01	T
100507	\$846,498	\$2,048,656	\$2,900,000	\$5,795,153	7	S	0.00011	\$637	N	0.002	Y	1	55	0.006032066	\$34,956.75	R
104101	\$151,707	\$13,214,689	\$1,160,000	\$14,526,396	7	S	0.00011	\$1,598	N	0.002	Y	1	27	0.002965757	\$43,081.76	R
104102	\$505,689	NA	\$0	\$505,689	6	S	0.00011	\$56	Y	0.002	Y	1	27	0.002965757	\$1,499.75	R
104103	\$177,810	NA	\$1,160,000	\$1,337,810	6	S	0.00011	\$147	N	0.002	Y	1	36	0.003952386	\$5,287.54	R
104104	\$529,077	\$245,167	\$1,160,000	\$1,934,244	7	S	0.00011	\$213	N	0.002	Y	1	29	0.003185092	\$6,160.75	R
104105	\$147,258	\$416,784	\$1,160,000	\$1,724,042	6	S	0.00011	\$190	N	0.002	Y	1	15	0.00164873	\$2,842.48	R
104107	\$336,611	\$163,445	\$1,160,000	\$1,660,055	7	O	0.00017	\$282	N	0.002	Y	1	31	0.005256584	\$8,726.22	M
104126	\$394,016	\$268,213	\$1,160,000	\$1,822,228	7	S	0.00011	\$200	N	0.002	Y	1	44	0.004828571	\$8,798.76	R
104131	\$2,010,767	\$2,860,561	\$2,900,000	\$7,771,328	7	R	0.000077	\$598	Y	0.0005	Y	1	51	0.00391945	\$30,459.33	R
104132	\$2,138,501	\$2,860,561	\$2,900,000	\$7,899,061	7	R	0.000077	\$608	Y	0.0005	Y	1	51	0.00391945	\$30,959.97	R
104135	\$415,133	\$35,183	\$580,000	\$1,030,316	7	R	0.000077	\$79	N	0.001	Y	1	53	0.004072841	\$4,196.31	R
104136	\$217,540	NA	\$1,160,000	\$1,377,540	5	O	0.00032	\$23	Y	0.0001	N	1	18	0.00574436	\$7,913.08	T
104137	\$261,905	NA	\$1,160,000	\$1,421,905	5	O	0.00032	\$24	Y	0.0001	N	1	31	0.009872531	\$14,037.80	T
104141	\$1,370,041	\$1,661,066	\$2,900,000	\$5,931,107	7	R	0.000077	\$457	N	0.0001	Y	1	59	0.00453287	\$26,884.94	R
104142	\$1,841,237	\$3,659,853	\$2,900,000	\$8,401,090	6	S	0.00011	\$924	N	0.0001	N	1	63	0.006906421	\$58,021.47	R
104143	\$4,920,287	\$1,668,289	\$2,900,000	\$9,488,576	7	S	0.00011	\$1,044	N	0.001	Y	1	67	0.007343311	\$69,677.56	R
104144	\$4,916,479	\$1,668,289	\$2,900,000	\$9,484,768	7	S	0.00011	\$1,043	N	0.001	Y	1	67	0.007343311	\$69,649.60	R
104146	\$217,103	NA	\$1,160,000	\$1,377,103	7	S	0.00011	\$151	Y	0.0005	Y	1	51	0.0055946	\$7,704.34	R
104201	\$144,215	\$659,679	\$1,160,000	\$1,963,894	6	S	0.00011	\$216	N	0.001	Y	1	32	0.003514005	\$6,901.13	R
104204	\$1,029,357	\$14,006,675	\$2,900,000	\$17,936,032	7	S	0.00011	\$1,973	N	0.0005	Y	1	50	0.005485204	\$98,382.79	R
104205	\$215,667	\$2,038,888	\$1,160,000	\$3,414,555	7	S	0.00011	\$376	N	0.002	Y	1	37	0.004061952	\$13,869.76	R
104208	\$281,594	\$1,155,396	\$2,900,000	\$4,336,990	7	S	0.00011	\$477	N	0.002	Y	1	39	0.00428		



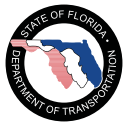
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
104234	\$444,819	\$851,864	\$2,900,000	\$4,196,683	6	S	0.00011	\$462	N	0.0005	Y	1	31	0.003404379	\$14,287.10	R
104235	\$878,400	\$837,883	\$2,900,000	\$4,616,282	6	S	0.00011	\$508	N	0.0005	Y	1	31	0.003404379	\$15,715.58	R
104245	\$1,565,200	\$732,071	\$2,900,000	\$5,197,270	7	S	0.00011	\$572	N	0.001	Y	1	46	0.005047497	\$26,233.20	R
104248	\$468,230	NA	\$1,160,000	\$1,628,230	6	S	0.00011	\$179	Y	0.0005	Y	1	44	0.004828571	\$7,862.02	R
104249	\$336,638	NA	\$1,160,000	\$1,496,638	7	S	0.00011	\$165	Y	0.002	Y	1	47	0.005156941	\$7,718.07	T
104250	\$679,964	\$183,523	\$1,160,000	\$2,023,487	7	S	0.00011	\$223	Y	0.002	Y	1	43	0.00471909	\$9,549.02	R
104252	\$679,964	\$183,523	\$1,160,000	\$2,023,487	6	S	0.00011	\$223	Y	0.002	Y	1	43	0.00471909	\$9,549.02	R
104256	\$2,800,016	\$2,043,993	\$2,900,000	\$7,744,009	7	S	0.00011	\$852	N	0.0005	Y	1	51	0.0055946	\$43,324.63	R
104257	\$188,441	NA	\$580,000	\$768,441	7	S	0.00011	\$85	Y	0.001	Y	1	51	0.0055946	\$4,299.12	R
104260	\$4,310,714	\$8,804,383	\$2,900,000	\$16,015,097	7	S	0.00011	\$1,762	N	0.002	Y	1	55	0.006032066	\$96,604.13	R
104262	\$1,718,217	\$1,067,198	\$2,900,000	\$5,685,415	7	S	0.00011	\$625	N	0.001	Y	1	58	0.00636004	\$36,159.47	M
104267	\$2,330,100	\$6,644,263	\$2,900,000	\$11,874,363	7	S	0.00011	\$1,306	N	0.002	Y	1	57	0.006250727	\$74,223.40	R
104269	\$2,300,227	\$1,792,645	\$2,900,000	\$6,992,872	7	S	0.00011	\$769	N	0.002	Y	1	63	0.006906421	\$48,295.72	M
104281	\$2,360,660	\$888,450	\$2,900,000	\$6,149,110	7	R	0.000077	\$473	N	0.002	Y	1	60	0.004609521	\$28,344.45	T
104288	\$4,211,948	\$10,892,475	\$2,900,000	\$18,004,423	7	R	0.000077	\$1,386	N	0.002	Y	1	58	0.004456213	\$80,231.55	R
104292	\$1,393,734	\$1,641,950	\$2,900,000	\$5,935,684	7	R	0.000077	\$457	N	0.002	Y	1	67	0.005145913	\$30,544.51	R
104293	\$1,382,215	\$1,641,950	\$2,900,000	\$5,924,166	7	R	0.000077	\$456	N	0.002	Y	1	67	0.005145913	\$30,485.24	R
104301	\$473,193	\$1,968,482	\$1,160,000	\$3,601,675	6	S	0.00011	\$396	N	0.002	Y	1	31	0.003404379	\$12,261.47	T
104304	\$259,037	\$167,803	\$580,000	\$1,006,841	7	O	0.00017	\$171	N	0.002	Y	1	32	0.00542569	\$5,462.81	R
104308	\$344,617	\$439,786	\$1,160,000	\$1,944,403	7	S	0.00011	\$214	N	0.001	Y	1	30	0.003294742	\$6,406.31	R
104309	\$149,834	\$13,017,665	\$1,160,000	\$14,327,499	6	R	0.000077	\$1,103	Y	0.002	Y	1	31	0.002384245	\$34,160.27	T
104312	\$531,285	\$952,540	\$2,900,000	\$4,383,825	6	S	0.00011	\$482	N	0.002	Y	1	26	0.002856071	\$12,520.52	T
104313	\$143,591	\$498,665	\$1,160,000	\$1,802,256	7	S	0.00011	\$198	N	0.002	Y	1	30	0.003294742	\$5,937.97	R
104314	\$127,493	\$205,233	\$580,000	\$912,726	6	S	0.00011	\$100	N	0.002	Y	1	32	0.003514005	\$3,207.32	R
104315	\$252,719	\$65,566	\$580,000	\$898,285	6	R	0.000077	\$69	N	0.002	Y	1	31	0.002384245	\$2,141.73	R
104317	\$172,777	\$160,087	\$1,160,000	\$1,492,864	6	S	0.00011	\$164	N	0.001	Y	1	31	0.003404379	\$5,082.28	T
104320	\$156,473	\$50,123	\$580,000	\$786,596	6	F	0.00022	\$173	N	0.001	Y	1	40	0.008762353	\$6,892.43	T
104321	\$1,411,644	\$290,259	\$1,160,000	\$2,861,902	7	R	0.000077	\$220	N	0.002	Y	1	30	0.002307423	\$6,603.62	T
104322	\$491,080	\$717,948	\$1,160,000	\$2,369,027	6	S	0.00011	\$261	N	0.002	Y	1	35	0.003842809	\$9,103.72	T
104323	\$498,080	\$994,796	\$1,160,000	\$2,652,876	6	S	0.00011	\$292	N	0.0005	Y	1	36	0.003952386	\$10,485.19	T
104324	\$209,065	\$1,947,303	\$1,160,000	\$3,316,368	7	S	0.00011	\$365	N	0.0005	Y	1	31	0.003404379	\$11,290.18	T
104329	\$211,078	NA	\$1,160,000	\$1,371,078	7	S	0.00011	\$151	Y	0.0005	Y	1	42	0.004609597	\$6,320.12	T
104330	\$5,661,714	\$12,524,141	\$2,900,000	\$21,085,855	7	O	0.00017	\$3,585	N	0.002	Y	1	37	0.006270791	\$132,224.98	R
104331	\$158,070	\$105,549	\$580,000	\$843,618	7	O	0.00017	\$143	N	0.001	Y	1	43	0.007283964	\$6,144.88	T
104335	\$351,797	\$1,894,927	\$1,160,000	\$3,406,724	7	S	0.00011	\$375	N	0.002	Y	1	32	0.003514005	\$11,971.25	R
104350	\$2,288,592	\$2,245,547	\$1,160,000	\$5,694,139	7	S	0.00011	\$626	N	0.002	Y	1	47	0.005156941	\$29,364.34	R
104357	\$841,761	\$185,072	\$1,160,000	\$2,186,832	7	S	0.00011	\$241	N	0.002	Y	1	53	0.005813357	\$12,712.84	R
104362	\$5,022,423	\$15,650,628	\$2,900,000	\$23,573,051	7	S	0.00011	\$2,593	N	0.0005	Y	1	63	0.006906421	\$162,805.43	R
104363	\$2,437,294	\$16,426,910	\$2,900,000	\$21,764,204	7	R	0.000077	\$1,676	N	0.002	Y	1	63	0.004839439	\$105,326.53	R
104401	\$175,898	\$117,550	\$1,160,000	\$1,453,449	7	S	0.00011	\$160	N	0.002	Y	1	40	0.004390575	\$6,381.48	R
104402	\$156,473	\$70,087	\$580,000	\$806,560	6	S	0.00011	\$89	N	0.001	N	1	40	0.004390575	\$3,541.26	R
104403	\$208,784	\$1,473,820	\$1,160,000	\$2,842,604	6	S	0.00011	\$313	N	0.0005	Y	1	40	0.004390575	\$12,480.67	R
104404	\$177,810	\$420,329	\$1,160,000	\$1,758,139	7	S	0.00011	\$193	N	0.0005	Y	1	40	0.004390575	\$7,719.24	R
104405	\$383,059	\$2,696,768	\$1,160,000	\$4,239,827	6	S	0.00011	\$466	N	0.001	N	1	27	0.002965757	\$12,574.30	R
104406	\$588,003	\$387,012	\$1,160,000	\$2,135,015	7	S	0.00011	\$235	N	0.0005	Y	1	33	0.003623618	\$7,736.48	R
104407	\$255,878	\$159,288	\$580,000	\$995,166	7	S	0.00011	\$109	N	0.002	Y	1	31	0.003404379	\$3,387.92	R
104408	\$129,519	\$47,944	\$580,000	\$757,462	6	O	0.00017	\$129	N	0.002	Y	1	32	0.00542569	\$4,109.75	R
104409	\$348,363	\$1,763,165	\$1,160,000	\$3,271,528	7	S	0.00011	\$360	N	0.0005	Y	1	31	0.003404379	\$11,137.52	R
104410	\$348,925	\$228,689	\$1,160,000	\$1,737,614	7	S	0.00011	\$191	N	0.002	Y	1	31	0.003404379	\$5,915.50	R
104411	\$145,385	\$146,001	\$1,160,000	\$1,451,386	6	S	0.00011	\$160	N	0.002	Y	1	32	0.003514005	\$5,100.18	R
104412	\$129,519	\$58,840	\$580,000	\$768,359	6	S	0.00011	\$85	N	0.002	Y	1	26	0.002856071	\$2,944.49	R
104413	\$130,927	\$99,821	\$580,000	\$810,747	6	S	0.00011	\$89	N	0.002	Y	1	33	0.003623618	\$2,937.84	R
104414	\$174,697	\$490,361	\$1,160,000	\$1,825,058	7	S	0.00011	\$201	N	0.002	Y	1	31	0.003404379	\$6,213.19	R
104415	\$415,578	\$812,725	\$1,160,000	\$2,388,302	6	S	0.00011	\$263	N	0.002	Y	1	37	0.004061952	\$9,701.17	R
104416	\$213,466	\$791,615	\$1,160,000	\$2,165,081	6	O	0.00017	\$368	N	0.001	Y	1	37	0.006270791	\$13,576.77	R
104417	\$303,413	\$284,981	\$1,160,000	\$1,748,394	6	S	0.00011	\$192	N	0.002	Y	1	36	0.003952386	\$6,910.33	R
104418	\$355,387	\$106,930	\$1,160,000	\$1,622,317	7	S	0.00011	\$178	N	0.002	Y	1	37	0.004061952	\$6,589.77	R
104419	\$516,926	\$3,192,846	\$1,160,000	\$4,869,772	7	S	0.00011	\$536	N	0.002	Y	1	31	0.003404379	\$16,578.55	R
104420	\$176,616	\$3,166,459	\$1,160,000	\$4,503,075	6	S	0.00011	\$495	N	0.0005	Y	1	32	0.003514005	\$15,823.83	R
104421	\$529,849	\$1,018,544	\$1,160,000	\$2,708,394	7	S	0.00011	\$298	N	0.0005	Y	1	32	0.003514005	\$9,517.31	R
104422	\$671,348	\$818,002	\$1,160,000	\$2,649,350	6	S	0.00011	\$291	N	0.0001	N	1	32	0.003514005	\$9,309.83	R
104423	\$213,372	\$964,011	\$1,160,000	\$2,337,383	6	S	0.00011	\$257	N	0.0005	Y	1	37	0.004061952	\$9,494.34	R
104424	\$158,156	\$147,489	\$580,000	\$885,645	5	S	0.00024	\$3	N	0.0002	N	1	39	0.009317444	\$8,251.95	R
104425	\$218,008	\$964,011	\$1,160,000	\$2,342,019	6	S	0.00011	\$258	N	0.0001	N	1	37	0.004061952	\$9,513.17	R
104426	\$396,123	\$658,032	\$1,160,000	\$2,214,155	6	S	0.00011	\$244	N	0.0001	N	1	15	0.00164873	\$3,650.54	R
104427	\$284,309	\$254,861	\$580,000	\$1,119,170	6	S	0.00011	\$123	N	0.0001	N	1	36	0.003952386	\$4,423.39	R
104428	\$282,284	\$308,453	\$1,160,000	\$1,750,737	6	S	0.00011	\$193	N	0.0002	Y	1	32	0.003514005	\$6,152.10	R
104429	\$153,211	\$175,914	\$580,000	\$909,126	6	S	0.00011	\$100	N	0.001	Y	1	37	0.004061952	\$3,692.83	R
104430	\$254,488	\$58,406	\$580,000	\$892,893	7	S	0.00011	\$98	N	0.0002	Y	1	33	0.003623618	\$3,235.50	R
104431	\$351,313	\$257,425	\$1,160,000	\$1,768,738	7	S	0.00011	\$195	N	0.0002	Y	1	33	0.003623618	\$6,409.23	R
104432	\$771,052	\$424,956	\$580,000	\$1,776,008	6	R	0.000077	\$137	N	0.0005	Y	1	39	0.002998611	\$5,325.56	R
104433	\$173,987	NA	\$1,160,000	\$1,333,987	7	S	0.00011	\$147	Y	0.002	Y	1	35	0.003842809		



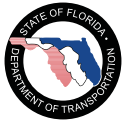
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
104445	\$213,372	\$251,402	\$1,160,000	\$1,624,774	7	S	0.00011	\$179	N	0.002	Y	1	42	0.004609597	\$7,489.55	R
104446	\$213,372	\$1,099,465	\$1,160,000	\$2,472,837	6	S	0.00011	\$272	N	0.002	Y	1	43	0.00471909	\$11,669.54	R
104452	\$742,613	\$1,521,419	\$2,900,000	\$5,164,031	7	S	0.00011	\$568	N	0.002	Y	1	49	0.005375795	\$27,760.77	R
104470	\$414,240	NA	\$580,000	\$994,240	7	S	0.00011	\$109	Y	0.002	Y	1	46	0.005047497	\$5,018.42	R
104501	\$1,825,973	\$962,830	\$2,900,000	\$5,688,803	7	S	0.00011	\$626	Y	0.002	Y	1	53	0.005813357	\$33,071.04	R
104502	\$1,806,994	\$2,629,815	\$2,900,000	\$7,336,809	7	S	0.00011	\$807	Y	0.0005	Y	1	55	0.006032066	\$44,256.12	R
104601	\$1,599,474	\$1,273,803	\$2,900,000	\$5,773,277	8	S	0.0000222	\$13	N	0.0005	Y	1	72	0.000158388	\$914.42	M
104602	\$1,578,060	\$3,108,986	\$2,900,000	\$7,587,046	8	S	0.0000022	\$17	N	0.002	Y	1	70	0.000153988	\$1,168.32	T
104702	\$2,057,403	\$1,611,675	\$2,900,000	\$6,569,078	7	R	0.000077	\$506	N	0.002	Y	1	71	0.005452292	\$35,816.53	R
105100	\$91,491	\$42,477	\$580,000	\$713,967	7	S	0.00011	\$79	N	0.002	Y	1	31	0.003404379	\$2,430.61	R
105300	\$91,491	\$53,096	\$580,000	\$724,587	7	S	0.00011	\$80	N	0.0005	Y	1	31	0.003404379	\$2,466.77	R
105600	\$12,732,113	\$2,149,052	\$2,900,000	\$17,781,165	7	R	0.000077	\$1,369	N	0.0005	Y	1	25	0.001923222	\$34,197.13	T
105602	\$4,228,555	\$5,975,426	\$2,900,000	\$13,103,981	7	S	0.00011	\$1,441	N	0.0002	Y	1	26	0.002856071	\$37,425.90	R
105605	\$11,636,579	\$3,451,633	\$2,900,000	\$17,988,212	6	R	0.000077	\$1,385	Y	0.0002	Y	1	32	0.002461061	\$44,270.10	T
105606	\$5,626,066	\$4,109,087	\$2,900,000	\$12,635,152	6	R	0.000077	\$973	Y	0.002	Y	1	15	0.001154378	\$14,585.74	T
105608	\$1,039,330	\$457,377	\$1,160,000	\$2,656,708	5	S	0.00024	\$9	N	0.002	Y	1	15	0.003593588	\$9,548.10	R
105612	\$1,358,367	\$2,572,124	\$2,900,000	\$6,830,491	7	S	0.00011	\$751	N	0.0005	Y	1	43	0.00471909	\$3,233.70	T
105613	\$325,514	NA	\$580,000	\$905,514	7	S	0.00011	\$100	Y	0.002	Y	1	43	0.00471909	\$4,273.20	T
105618	\$149,131	NA	\$1,160,000	\$1,309,131	7	S	0.00011	\$144	Y	0.002	Y	1	39	0.004281046	\$5,604.45	T
105622	\$391,284	\$1,643,635	\$2,900,000	\$4,934,919	7	O	0.00017	\$839	N	0.0005	Y	1	48	0.008127486	\$40,108.48	T
105623	\$51,240	NA	\$0	\$51,240	7	O	0.00017	\$9	Y	0.002	Y	1	36	0.006101828	\$312.66	T
105627	\$226,670	\$238,932	\$1,160,000	\$1,625,602	7	S	0.00011	\$179	N	0.002	Y	1	58	0.00636004	\$10,338.89	T
105914	\$724,867	NA	\$1,160,000	\$1,884,867	7	S	0.00011	\$207	Y	0.002	Y	1	57	0.006250727	\$11,781.79	T
105915	\$1,048,835	\$1,442,498	\$1,160,000	\$3,651,333	7	R	0.000077	\$281	N	0.002	Y	1	62	0.004762806	\$17,390.59	R
110026	\$32,757,378	\$38,770,292	\$2,900,000	\$74,427,670	6	S	0.00011	\$8,187	Y	0.0002	Y	1	16	0.001758549	\$130,884.69	R
110800	\$264,175	\$23,699	\$0	\$287,875	7	S	0.00011	\$32	N	0.002	Y	1	52	0.005703985	\$1,642.03	R
114023	\$1,393,016	\$6,441,995	\$2,900,000	\$10,735,011	7	S	0.00011	\$1,181	N	0.002	Y	1	34	0.00373322	\$40,076.16	R
114044	\$550,420	\$7,219,903	\$2,900,000	\$10,670,323	6	S	0.00011	\$1,174	N	0.0002	Y	1	20	0.002197703	\$23,450.20	R
114045	\$891,136	\$838,672	\$1,160,000	\$2,889,807	6	O	0.00017	\$491	N	0.002	Y	1	24	0.004072034	\$11,767.39	R
114047	\$1,746,771	\$1,357,192	\$1,160,000	\$4,263,963	7	S	0.00011	\$469	N	0.002	Y	1	25	0.002746373	\$11,710.43	R
114051	\$973,411	\$1,316,579	\$1,160,000	\$3,449,990	7	S	0.00011	\$379	N	0.002	Y	1	33	0.003623618	\$12,501.45	R
114052	\$528,538	NA	\$2,900,000	\$3,428,538	7	O	0.00017	\$583	Y	0.002	Y	1	18	0.00305582	\$10,476.18	R
114053	\$995,481	\$6,012,937	\$1,160,000	\$8,168,417	7	S	0.00011	\$899	N	0.002	Y	1	34	0.00373322	\$30,494.50	R
114054	\$306,663	\$562,457	\$580,000	\$1,449,120	7	R	0.000077	\$112	N	0.002	Y	1	22	0.001692631	\$2,452.83	R
114077	\$1,654,912	\$10,072,673	\$2,900,000	\$14,627,585	7	S	0.00011	\$1,609	N	0.002	Y	1	28	0.003075431	\$44,986.12	R
114079	\$6,407,760	\$10,211,573	\$2,900,000	\$19,519,333	7	S	0.00011	\$2,147	N	0.0002	Y	1	46	0.005047497	\$98,523.77	R
114082	\$942,547	\$1,265,000	\$1,160,000	\$3,367,548	6	R	0.000077	\$259	N	0.002	Y	1	29	0.002230594	\$7,511.63	R
114084	\$161,383	\$123,140	\$580,000	\$864,523	7	S	0.00011	\$95	N	0.0002	Y	1	51	0.0055946	\$4,836.66	R
114086	\$1,321,837	\$1,377,762	\$1,160,000	\$3,859,599	7	S	0.00011	\$425	N	0.0005	Y	1	42	0.004609597	\$17,791.20	R
114087	\$910,895	\$3,230,492	\$1,160,000	\$5,301,387	7	S	0.00011	\$583	N	0.0002	Y	1	45	0.00493804	\$26,178.46	R
114091	\$1,619,467	\$1,397,464	\$1,160,000	\$4,176,931	8	S	0.000022	\$9	N	0.0002	Y	1	65	0.00014299	\$597.26	R
114092	\$2,227,839	\$1,837,426	\$1,160,000	\$5,225,265	7	S	0.00011	\$575	N	0.0002	Y	1	65	0.00712489	\$37,229.44	R
115100	\$98,444	NA	\$580,000	\$678,444	7	S	0.00011	\$75	N	0.0002	Y	1	36	0.003952386	\$2,681.47	R
115600	\$809,102	\$1,177,659	\$1,160,000	\$3,146,761	7	S	0.00011	\$346	N	0.0005	Y	1	25	0.002746373	\$8,642.18	R
120001	\$1,381,279	\$4,520,995	\$2,900,000	\$8,802,274	7	S	0.00011	\$968	Y	0.002	Y	1	15	0.00164873	\$14,512.57	T
120011	\$416,163	\$1,923,052	\$2,900,000	\$5,239,215	7	S	0.00011	\$576	Y	0.002	Y	1	15	0.00164873	\$8,638.05	R
120025	\$1,927,547	\$23,262,763	\$2,900,000	\$28,090,310	7	S	0.00011	\$3,090	Y	0.002	Y	1	38	0.004171505	\$117,178.87	T
120033	\$381,451	\$23,262,763	\$2,900,000	\$26,544,214	7	S	0.00011	\$2,920	Y	0.0005	Y	1	38	0.004171505	\$110,729.32	M
120034	\$1,276,489	\$23,262,763	\$2,900,000	\$27,439,252	7	S	0.00011	\$3,018	Y	0.0005	Y	1	38	0.004171505	\$114,462.97	M
120035	\$1,079,177	\$12,606,677	\$2,900,000	\$16,585,854	7	S	0.00011	\$1,824	Y	0.002	Y	1	38	0.004171505	\$69,187.97	M
120043	\$621,435	NA	\$1,160,000	\$1,781,435	7	S	0.00011	\$196	Y	0.002	Y	1	37	0.004061952	\$7,236.10	T
120050	\$22,121,214	NA	\$2,900,000	\$25,021,214	6	S	0.00011	\$2,752	Y	0.0005	Y	1	34	0.00373322	\$93,409.69	T
120065	\$1,325,278	\$3,080,653	\$2,900,000	\$7,305,931	7	S	0.00011	\$804	N	0.002	Y	1	26	0.002856071	\$20,866.26	R
120160	\$28,538,625	\$26,853,882	\$2,900,000	\$58,292,507	7	S	0.00011	\$6,412	Y	0.0005	Y	1	56	0.006141403	\$357,997.77	T
120164	\$1,732,764	\$6,435,606	\$2,900,000	\$11,068,370	8	R	0.0000017	\$19	Y	0.0005	Y	1	54	9.17959E-05	\$1,016.03	T
124002	\$217,249	\$67,963	\$580,000	\$865,212	7	S	0.00011	\$95	N	0.002	Y	1	16	0.001758549	\$1,521.52	T
124004	\$292,275	\$63,715	\$580,000	\$935,991	7	S	0.00011	\$103	N	0.0005	Y	1	44	0.004828571	\$4,519.50	T
124006	\$256,637	\$398,805	\$1,160,000	\$1,815,442	7	S	0.00011	\$200	N	0.002	Y	1	41	0.004500092	\$8,169.66	R
124008	\$518,448	\$168,348	\$1,160,000	\$1,846,796	7	S	0.00011	\$203	N	0.0005	Y	1	15	0.00164873	\$3,044.87	R
124010	\$1,005,548	NA	\$1,160,000	\$2,165,548	7	S	0.00011	\$238	N	0.002	Y	1	16	0.001758549	\$3,808.22	T
124012	\$858,422	\$1,147,247	\$2,900,000	\$4,905,669	7	S	0.00011	\$540	N	0.0005	Y	1	41	0.004500092	\$22,075.96	R
124015	\$656,693	\$32,909,418	\$1,160,000	\$34,726,111	7	S	0.00011	\$3,820	N	0.0005	Y	1	45	0.00493804	\$171,478.92	R
124019	\$1,726,895	\$4,632,011	\$2,900,000	\$9,258,906	6	S	0.00011	\$1,018	N	0.002	Y	1	39	0.004281046	\$39,637.80	M
124022	\$420,002	NA	\$1,160,000	\$1,580,002	7	S	0.00011	\$174	Y	0.0005	Y	1	51	0.0055946	\$8,839.48	M
124023	\$391,440	\$526,292	\$1,160,000	\$2,077,732	6	S	0.00011	\$229	N	0.0005	Y	1	33	0.003623618	\$7,528.91	M
124025	\$1,025,143	\$1,763,964	\$2,900,000	\$5,689,107	7	S	0.00011	\$626	N	0.002	Y	1	21	0.002307461	\$13,127.39	M
124026	\$740,272	\$1,146,258	\$1,160,000	\$3,046,530	7	S	0.00011	\$335	N	0.0005	Y	1	15	0.00164873	\$5,022.91	T
124027	\$321,908	\$1,125,370	\$1,160,000	\$2,607,279	5	S	0.00024	\$9	N	0.002	Y	1	36	0.008603811	\$22,432.53	T
124031	\$768,647	\$6,257,440	\$2,900,000	\$9,926,087	6	S	0.00011	\$1,092	N	0.002	Y	1	46	0.005047497	\$50,101.89	R
124032	\$320,466	NA	\$580,000	\$900,466	7	S	0.00011	\$99	Y	0.0005	Y	1	52	0.005703985	\$5,136.24	R
124038	\$106,307	NA	\$580,000	\$686,307	6	O	0.00017	\$117	Y	0.002	Y	1	16	0.002716535	\$1,864.38	R
124044	\$33,811,208	\$3,119,372	\$2,900,000	\$39,8												



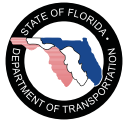
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
124060	\$1,894,022	\$21,915,402	\$2,900,000	\$26,709,424	7	R	0.000077	\$2,057	Y	0.0005	Y	1	29	0.002230594	\$59,577.89	T
124061	\$1,289,974	\$3,517,378	\$2,900,000	\$7,707,352	6	S	0.00011	\$848	Y	0.0005	Y	1	31	0.003404379	\$26,238.75	T
124062	\$1,289,974	\$3,517,378	\$2,900,000	\$7,707,352	6	S	0.00011	\$848	Y	0.0005	Y	1	31	0.003404379	\$26,238.75	T
124063	\$1,289,974	\$4,355,632	\$2,900,000	\$8,545,606	7	S	0.00011	\$940	Y	0.0005	Y	1	33	0.003623618	\$30,966.02	T
124064	\$1,289,974	\$4,355,632	\$2,900,000	\$8,545,606	7	S	0.00011	\$940	Y	0.0005	Y	1	33	0.003623618	\$30,966.02	T
124065	\$42,852,419	\$3,119,618	\$2,900,000	\$48,872,038	7	R	0.000077	\$3,763	Y	0.0005	Y	1	55	0.004226207	\$206,543.37	T
124070	\$6,231,955	\$3,930,562	\$2,900,000	\$13,062,518	6	R	0.000077	\$1,006	N	0.0005	Y	1	56	0.004302882	\$56,206.47	R
124071	\$6,215,599	\$3,930,562	\$2,900,000	\$13,046,161	6	R	0.000077	\$1,005	N	0.0005	Y	1	56	0.004302882	\$56,136.09	R
124073	\$1,428,352	\$2,399,725	\$2,900,000	\$6,728,077	7	S	0.00011	\$740	Y	0.001	Y	1	56	0.006141403	\$41,319.83	R
124074	\$1,907,944	\$2,399,725	\$2,900,000	\$7,207,669	7	S	0.00011	\$793	Y	0.0005	Y	1	57	0.006250727	\$45,053.17	R
124075	\$1,668,148	\$1,397,075	\$2,900,000	\$5,965,222	7	R	0.000077	\$459	Y	0.001	Y	1	57	0.004379551	\$26,124.99	R
124076	\$395,654	\$379,975	\$1,160,000	\$1,935,630	7	S	0.00011	\$213	N	0.002	Y	1	57	0.006250727	\$12,099.10	T
124078	\$157,540	\$95,529	\$1,160,000	\$1,413,069	7	S	0.00011	\$155	N	0.0005	Y	1	57	0.006250727	\$8,832.71	M
124079	\$273,339	NA	\$580,000	\$853,339	7	S	0.00011	\$94	Y	0.001	Y	1	57	0.006250727	\$5,333.99	M
124083	\$99,010	NA	\$580,000	\$679,010	6	O	0.00017	\$115	Y	0.0005	Y	1	58	0.00981238	\$6,662.70	T
124084	\$1,755,676	\$1,660,071	\$2,900,000	\$6,315,747	8	R	0.0000017	\$11	N	0.0005	Y	1	59	0.00100295	\$633.44	R
124092	\$1,200,355	\$10,419,747	\$2,900,000	\$14,520,101	7	S	0.00011	\$1,597	Y	0.002	Y	1	65	0.00712489	\$103,454.12	R
124097	\$1,135,552	\$8,006,802	\$2,900,000	\$12,042,353	7	S	0.00011	\$1,325	Y	0.002	Y	1	65	0.00712489	\$85,800.44	R
124126	\$570,554	\$58,328,394	\$2,900,000	\$61,798,948	7	S	0.00011	\$6,798	Y	0.0005	Y	1	63	0.006906421	\$426,809.58	T
124904	\$317,324	\$205,233	\$580,000	\$1,102,558	7	S	0.00011	\$121	N	0.002	Y	1	30	0.003294742	\$3,632.64	R
124905	\$317,039	\$1,715,493	\$1,160,000	\$3,192,532	7	S	0.00011	\$351	N	0.002	Y	1	38	0.004171505	\$13,317.66	R
124906	\$410,669	\$132,740	\$580,000	\$1,123,409	7	S	0.00011	\$124	N	0.0005	Y	1	38	0.004171505	\$4,686.31	R
124907	\$560,003	\$1,475,229	\$1,160,000	\$3,195,233	7	S	0.00011	\$351	N	0.0005	Y	1	38	0.004171505	\$13,328.93	R
124908	\$213,644	\$137,294	\$580,000	\$930,938	7	S	0.00011	\$102	N	0.002	Y	1	26	0.002856071	\$2,658.82	R
124909	\$245,157	\$220,407	\$1,160,000	\$1,625,565	7	S	0.00011	\$179	N	0.002	Y	1	26	0.002856071	\$4,642.73	R
124910	\$576,953	\$817,223	\$1,160,000	\$2,554,177	7	S	0.00011	\$281	N	0.001	Y	1	30	0.003294742	\$8,415.35	R
124911	\$432,715	\$849,732	\$1,160,000	\$2,442,447	7	S	0.00011	\$269	N	0.0005	Y	1	30	0.003294742	\$8,047.23	R
124912	\$1,342,182	\$2,744,790	\$1,160,000	\$5,246,971	7	S	0.00011	\$577	N	0.002	Y	1	46	0.005047957	\$26,484.07	R
124926	\$429,039	\$52,774	\$580,000	\$1,061,814	7	S	0.00011	\$117	N	0.0005	Y	1	52	0.005703985	\$6,056.57	R
124928	\$972,592	\$47,786	\$0	\$1,020,378	7	S	0.00011	\$112	N	0.002	Y	1	58	0.00636004	\$6,489.64	R
124929	\$821,063	\$238,932	\$580,000	\$1,639,995	7	S	0.00011	\$180	N	0.0005	Y	1	58	0.00636004	\$10,430.43	R
124930	\$1,896,707	\$2,048,656	\$2,900,000	\$6,845,362	7	S	0.00011	\$753	N	0.0002	Y	1	58	0.00636004	\$43,536.77	R
124931	\$809,706	\$343,906	\$1,160,000	\$2,313,612	7	S	0.00011	\$254	N	0.0002	Y	1	58	0.00636004	\$14,714.66	R
124932	\$511,036	\$42,477	\$580,000	\$1,133,513	7	S	0.00011	\$125	N	0.002	Y	1	58	0.00636004	\$7,209.19	R
124933	\$511,036	\$42,477	\$580,000	\$1,133,513	7	S	0.00011	\$125	N	0.0005	Y	1	58	0.00636004	\$7,209.19	R
124934	\$469,488	\$53,096	\$580,000	\$1,102,584	7	S	0.00011	\$121	N	0.002	Y	1	60	0.006578628	\$7,253.49	R
124935	\$690,171	\$653,779	\$1,160,000	\$2,503,950	6	S	0.00011	\$275	N	0.002	Y	1	60	0.006578628	\$16,472.56	R
124936	\$501,474	\$165,549	\$1,160,000	\$1,827,023	8	S	0.000022	\$4	N	0.0002	Y	1	53	0.000116593	\$213.02	R
125002	\$317,039	\$760,018	\$1,160,000	\$2,237,056	7	S	0.00011	\$246	N	0.0002	Y	1	36	0.003952386	\$8,841.71	R
125003	\$554,104	\$1,393,086	\$2,900,000	\$4,847,190	7	S	0.00011	\$533	N	0.002	Y	1	36	0.003952386	\$19,157.97	M
125004	\$464,601	\$923,551	\$1,160,000	\$2,548,152	6	S	0.00011	\$280	N	0.002	Y	1	36	0.003952386	\$10,071.28	R
125005	\$384,323	\$771,751	\$1,160,000	\$2,316,074	6	S	0.00011	\$255	N	0.002	Y	1	36	0.003952386	\$9,154.02	R
125019	\$194,784	\$271,260	\$1,160,000	\$1,626,044	7	S	0.00011	\$179	N	0.0005	Y	1	41	0.004500092	\$7,317.35	R
125203	\$3,893,802	\$1,816,216	\$2,900,000	\$8,610,018	8	R	0.0000017	\$15	N	0.0005	Y	1	74	0.000125792	\$1,083.07	R
125204	\$4,333,875	\$4,273,868	\$2,900,000	\$11,507,743	8	S	0.0000022	\$25	N	0.002	Y	1	74	0.000162787	\$1,873.31	R
125500	\$474,621	\$26,548	\$580,000	\$1,081,169	7	S	0.00011	\$119	Y	0.0005	Y	1	49	0.005375795	\$5,812.14	T
125501	\$474,621	\$21,238	\$580,000	\$1,075,860	7	S	0.00011	\$118	Y	0.002	Y	1	49	0.005375795	\$5,783.60	T
125502	\$907,992	\$477,864	\$1,160,000	\$2,545,856	7	S	0.00011	\$280	N	0.002	Y	1	36	0.003952386	\$10,062.21	T
125512	\$437,514	\$2,498,948	\$2,900,000	\$5,836,463	7	S	0.00011	\$642	N	0.002	Y	1	41	0.004500092	\$26,264.62	R
125514	\$917,731	\$1,763,964	\$2,900,000	\$5,581,695	7	S	0.00011	\$614	N	0.002	Y	1	36	0.003952386	\$22,061.02	R
125518	\$277,614	\$65,378	\$580,000	\$922,991	7	S	0.00011	\$102	N	0.0005	Y	1	36	0.003952386	\$3,648.02	R
125522	\$255,279	\$779,346	\$1,160,000	\$2,194,625	7	S	0.00011	\$241	N	0.002	Y	1	31	0.003404379	\$7,471.34	T
125542	\$336,681	\$1,029,296	\$1,160,000	\$2,525,977	7	S	0.00011	\$278	N	0.0005	Y	1	41	0.004500092	\$11,367.13	R
125546	\$942,454	\$2,006,508	\$2,900,000	\$5,848,962	7	S	0.00011	\$643	N	0.0005	Y	1	36	0.003952386	\$23,117.36	R
125556	\$442,072	\$1,290,653	\$2,900,000	\$4,632,725	7	S	0.00011	\$510	N	0.0005	Y	1	41	0.004500092	\$20,847.69	R
125557	\$184,576	\$343,033	\$1,160,000	\$1,687,609	7	S	0.00011	\$186	N	0.0005	Y	1	40	0.004390575	\$7,409.57	R
125558	\$187,994	\$343,033	\$1,160,000	\$1,691,027	7	S	0.00011	\$186	N	0.0005	Y	1	40	0.004390575	\$7,424.58	R
125560	\$997,954	\$2,175,555	\$2,900,000	\$6,073,509	7	S	0.00011	\$668	N	0.002	Y	1	35	0.003842809	\$23,339.34	R
125562	\$984,938	\$3,527,927	\$2,900,000	\$7,412,865	7	S	0.00011	\$815	N	0.0005	Y	1	35	0.003842809	\$28,486.23	R
125566	\$711,616	\$282,343	\$1,160,000	\$2,153,959	7	S	0.00011	\$237	N	0.001	Y	1	39	0.004281046	\$9,221.20	R
125568	\$708,128	\$263,872	\$1,160,000	\$2,131,999	7	S	0.00011	\$235	N	0.0005	Y	1	36	0.003952386	\$8,426.48	R
125570	\$152,902	\$39,227	\$580,000	\$772,129	7	S	0.00011	\$85	N	0.0005	Y	1	40	0.004390575	\$3,390.09	R
125572	\$279,502	\$39,227	\$580,000	\$898,729	7	S	0.00011	\$99	N	0.002	Y	1	36	0.003952386	\$3,552.12	R
125574	\$205,085	\$126,658	\$1,160,000	\$1,491,743	7	S	0.00011	\$164	N	0.002	Y	1	40	0.004390575	\$6,549.61	R
125577	\$248,380	\$437,047	\$2,900,000	\$3,585,427	7	S	0.00011	\$394	N	0.0005	Y	1	40	0.004390575	\$15,742.09	R
125578	\$243,823	\$437,047	\$2,900,000	\$3,580,870	7	S	0.00011	\$394	N	0.0005	Y	1	40	0.004390575	\$15,722.08	R
125582	\$934,868	\$1,102,477	\$2,900,000	\$4,937,345	7	S	0.00011	\$543	N	0.0005	Y	1	39	0.004281046	\$21,137.00	R
125584	\$703,375	\$1,240,196	\$1,160,000	\$3,103,572	7	S	0.00011	\$341	N	0.0005	Y	1	38	0.004171505	\$12,946.57	R
125586	\$923,974	\$2,601,846	\$2,900,000	\$6,425,820	7	S	0.00011	\$707	Y	0.002	Y	1	39	0.004281046	\$27,509.23	R
125588	\$696,445	\$3,236,825	\$1,160,000	\$5,093,270	7	S	0.00011	\$560	Y	0.002	Y	1	36	0.003952386	\$20,130.57	R
125590	\$146,636	\$78,679	\$580,000	\$805,315	7	S	0.00011	\$89	N	0.0001	N	1	40	0.004390575	\$3,535.80	R
125592	\$166,631	\$143,294	\$1,160,000	\$1,469,9												



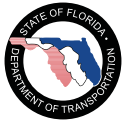
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
125644	\$928,594	\$2,513,648	\$2,900,000	\$6,342,242	7	S	0.00011	\$698	N	0.0001	N	1	35	0.003842809	\$24,372.03	R
125646	\$928,594	\$1,389,121	\$2,900,000	\$5,217,715	7	S	0.00011	\$574	N	0.0001	N	1	36	0.003952386	\$20,622.43	R
125648	\$713,770	\$845,798	\$1,160,000	\$2,719,568	7	S	0.00011	\$299	N	0.002	Y	1	36	0.003952386	\$10,748.78	R
125650	\$265,836	\$71,069	\$580,000	\$916,905	6	R	0.000077	\$71	N	0.002	Y	1	46	0.00353587	\$3,242.06	R
125652	\$286,507	\$118,018	\$580,000	\$984,525	7	S	0.00011	\$108	N	0.002	Y	1	36	0.003952386	\$3,891.22	R
125654	\$151,649	\$46,911	\$580,000	\$778,559	7	S	0.00011	\$86	N	0.002	Y	1	40	0.004390575	\$3,418.32	R
125656	\$276,274	\$65,378	\$580,000	\$921,652	7	S	0.00011	\$101	N	0.002	Y	1	36	0.003952386	\$3,642.72	R
125660	\$1,229,760	\$3,572,026	\$2,900,000	\$7,701,786	7	S	0.00011	\$847	N	0.002	Y	1	36	0.003952386	\$30,440.43	T
125662	\$1,441,400	\$3,902,769	\$2,900,000	\$8,244,169	7	S	0.00011	\$907	N	0.002	Y	1	36	0.003952386	\$32,584.14	R
125664	\$934,868	\$2,465,452	\$2,900,000	\$6,300,320	7	S	0.00011	\$693	N	0.0005	Y	1	36	0.003952386	\$24,901.30	R
125668	\$1,647,546	\$392,141	\$2,900,000	\$4,939,687	7	S	0.00011	\$543	N	0.002	Y	1	34	0.00373322	\$18,440.94	M
125670	\$942,454	\$1,106,274	\$2,900,000	\$4,948,728	7	S	0.00011	\$544	N	0.002	Y	1	36	0.003952386	\$19,559.29	R
125672	\$1,301,992	\$808,483	\$2,900,000	\$5,010,475	7	S	0.00011	\$551	N	0.0005	Y	1	36	0.003952386	\$19,803.33	T
125674	\$944,170	\$2,293,153	\$2,900,000	\$6,137,323	7	S	0.00011	\$675	N	0.0005	Y	1	36	0.003952386	\$24,257.07	R
125675	\$365,735	\$179,789	\$1,160,000	\$1,705,524	7	S	0.00011	\$188	N	0.001	Y	1	40	0.004390575	\$7,488.23	R
125676	\$377,674	\$179,789	\$1,160,000	\$1,717,464	7	S	0.00011	\$189	N	0.0005	Y	1	40	0.004390575	\$7,540.65	R
125677	\$423,514	\$92,536	\$1,160,000	\$1,676,050	7	S	0.00011	\$184	N	0.0005	Y	1	40	0.004390575	\$7,358.82	R
125678	\$427,728	\$83,790	\$1,160,000	\$1,671,518	7	S	0.00011	\$184	N	0.002	Y	1	40	0.004390575	\$7,338.93	R
125680	\$169,031	\$143,294	\$1,160,000	\$1,472,325	7	S	0.00011	\$162	N	0.0002	Y	1	41	0.004500092	\$6,625.60	R
125687	\$444,210	\$362,089	\$1,160,000	\$1,866,299	7	S	0.00011	\$205	N	0.0001	N	1	40	0.004390575	\$8,194.13	R
125708	\$554,104	\$310,612	\$1,160,000	\$2,024,715	7	S	0.00011	\$223	N	0.0001	N	1	41	0.004500092	\$9,111.40	R
125710	\$331,554	\$637,434	\$1,160,000	\$2,128,988	7	S	0.00011	\$234	N	0.0001	N	1	41	0.004500092	\$9,580.64	R
125712	\$693,098	\$1,127,768	\$1,160,000	\$2,980,866	7	S	0.00011	\$328	N	0.0005	Y	1	41	0.004500092	\$13,414.17	R
125714	\$835,440	\$955,729	\$1,160,000	\$2,951,168	6	S	0.00011	\$325	N	0.0002	Y	1	41	0.004500092	\$13,280.53	R
125716	\$539,167	\$764,583	\$1,160,000	\$2,463,750	6	S	0.00011	\$271	N	0.0002	Y	1	49	0.005375795	\$13,244.61	R
125719	\$275,811	\$118,018	\$1,160,000	\$1,553,829	7	S	0.00011	\$171	N	0.002	Y	1	31	0.003404379	\$5,289.82	T
125726	\$270,598	NA	\$1,160,000	\$1,430,598	7	S	0.00011	\$157	N	0.002	Y	1	41	0.004500092	\$6,437.82	R
125729	\$220,855	\$44,239	\$580,000	\$845,094	7	S	0.00011	\$93	N	0.002	Y	1	49	0.005375795	\$4,543.05	T
125730	\$250,971	\$49,198	\$1,160,000	\$1,460,169	7	S	0.00011	\$161	N	0.002	Y	1	49	0.005375795	\$7,849.57	T
125731	\$161,992	\$646	\$0	\$162,638	7	S	0.00011	\$18	N	0.002	Y	1	49	0.005375795	\$874.31	T
125732	\$242,988	\$326,541	\$1,160,000	\$1,729,529	6	S	0.00011	\$190	N	0.002	Y	1	49	0.005375795	\$9,297.59	T
125733	\$316,449	\$23,455	\$580,000	\$919,904	7	S	0.00011	\$101	N	0.0002	Y	1	49	0.005375795	\$4,945.22	T
125734	\$316,449	\$23,455	\$580,000	\$919,904	7	S	0.00011	\$101	N	0.0005	Y	1	49	0.005375795	\$4,945.22	T
125735	\$552,892	\$23,455	\$580,000	\$1,156,348	7	S	0.00011	\$127	N	0.0005	Y	1	49	0.005375795	\$6,216.29	R
125736	\$552,892	\$23,455	\$580,000	\$1,156,348	7	S	0.00011	\$127	N	0.0001	N	1	49	0.005375795	\$6,216.29	R
125737	\$527,912	\$23,455	\$580,000	\$1,131,368	7	S	0.00011	\$124	N	0.0001	N	1	49	0.005375795	\$6,082.00	M
125738	\$527,912	\$23,455	\$580,000	\$1,131,368	7	S	0.00011	\$124	N	0.0001	N	1	49	0.005375795	\$6,082.00	M
125740	\$424,352	\$70,366	\$580,000	\$1,074,718	7	S	0.00011	\$118	N	0.002	Y	1	49	0.005375795	\$5,777.46	R
125743	\$631,596	\$89,895	\$1,160,000	\$1,881,490	7	S	0.00011	\$207	N	0.002	Y	1	50	0.005485204	\$10,320.36	T
125744	\$631,596	\$89,895	\$1,160,000	\$1,881,490	7	S	0.00011	\$207	N	0.002	Y	1	50	0.005485204	\$10,320.36	T
126500	\$621,560	\$883,654	\$2,900,000	\$4,405,213	7	S	0.00011	\$485	Y	0.002	Y	1	35	0.003842809	\$16,928.39	T
130012	\$833,543	\$2,887,195	\$1,160,000	\$4,880,738	7	S	0.00011	\$537	N	0.0005	Y	1	16	0.001758549	\$8,583.02	R
130014	\$227,958	\$2,198,050	\$1,160,000	\$3,586,008	7	S	0.00011	\$394	N	0.0005	Y	1	21	0.002307461	\$8,274.57	R
130037	\$1,516,082	\$8,901,197	\$1,160,000	\$11,577,279	6	S	0.00011	\$1,274	N	0.0005	Y	1	16	0.001758549	\$20,359.21	R
130132	\$100,214,665	\$7,319,707	\$2,900,000	\$110,434,371	7	S	0.00011	\$12,148	Y	0.0005	Y	1	52	0.005703985	\$629,915.97	T
130136	\$10,245,874	\$18,507,842	\$2,900,000	\$31,653,716	7	S	0.00011	\$3,482	Y	0.002	Y	1	54	0.005922718	\$187,476.03	T
134002	\$322,629	\$133,802	\$580,000	\$1,036,431	7	S	0.00011	\$114	N	0.002	Y	1	16	0.001758549	\$1,822.61	T
134005	\$169,195	\$375,923	\$1,160,000	\$1,705,118	7	S	0.00011	\$188	N	0.002	Y	1	26	0.002856071	\$4,869.94	T
134007	\$156,473	\$164,598	\$580,000	\$901,071	7	S	0.00011	\$99	N	0.0005	Y	1	36	0.003952386	\$3,561.38	T
134010	\$261,272	\$161,337	\$0	\$422,609	5	S	0.00024	\$1	N	0.002	Y	1	32	0.007651499	\$3,233.59	R
134011	\$185,814	\$69,025	\$580,000	\$834,839	7	S	0.00011	\$92	N	0.002	Y	1	26	0.002856071	\$2,384.36	R
134015	\$461,581	\$661,046	\$1,160,000	\$2,282,627	6	S	0.00011	\$251	Y	0.0005	Y	1	28	0.003075431	\$7,020.06	T
134017	\$151,980	\$238,823	\$1,160,000	\$1,550,803	6	S	0.00011	\$171	N	0.002	Y	1	34	0.00373322	\$5,789.49	M
134019	\$170,319	\$441,301	\$1,160,000	\$1,771,619	7	S	0.00011	\$195	N	0.002	Y	1	26	0.002856071	\$5,059.87	T
134023	\$909,537	\$1,604,339	\$1,160,000	\$3,673,876	4	R	0.0004	\$1,470	N	0.002	Y	1	29	0.011535273	\$42,379.16	T
134024	\$350,704	\$1,604,339	\$1,160,000	\$3,115,044	6	S	0.00011	\$343	N	0.002	Y	1	29	0.003185092	\$9,921.70	R
134025	\$243,226	\$771,132	\$1,160,000	\$2,174,358	7	S	0.00011	\$239	N	0.002	Y	1	36	0.003952386	\$8,593.90	R
134026	\$193,871	\$2,814,630	\$1,160,000	\$4,168,501	6	S	0.00011	\$459	N	0.002	Y	1	36	0.003952386	\$16,475.53	R
134030	\$150,653	\$1,700,327	\$1,160,000	\$3,010,980	6	S	0.00011	\$331	N	0.002	Y	1	26	0.002856071	\$8,599.57	R
134031	\$197,094	\$1,190,354	\$580,000	\$1,967,448	7	S	0.00011	\$216	N	0.002	Y	1	26	0.002856071	\$5,619.17	R
134033	\$547,579	\$4,183,073	\$2,900,000	\$7,630,653	7	S	0.00011	\$839	N	0.002	Y	1	29	0.003185092	\$24,304.33	R
134034	\$165,051	\$255,750	\$1,160,000	\$1,580,801	7	S	0.00011	\$174	Y	0.002	Y	1	16	0.001758549	\$2,779.92	T
134035	\$230,778	\$84,954	\$580,000	\$895,732	6	R	0.000077	\$69	N	0.002	Y	1	30	0.002307461	\$2,066.83	R
134037	\$166,175	\$196,134	\$1,160,000	\$1,522,308	6	S	0.00011	\$167	N	0.002	Y	1	24	0.002636663	\$4,013.81	R
134042	\$166,175	\$593,632	\$1,160,000	\$1,919,807	4	S	0.0005	\$960	N	0.0005	N	1	24	0.011931252	\$22,905.70	M
134045	\$258,463	\$3,279,044	\$1,160,000	\$4,697,507	7	S	0.00011	\$517	N	0.0005	Y	1	31	0.003404379	\$15,992.10	R
134046	\$990,775	\$1,394,291	\$1,160,000	\$3,545,066	7	R	0.000077	\$273	N	0.0005	Y	1	41	0.003152143	\$11,174.56	R
134049	\$198,155	\$7,767,480	\$1,160,000	\$9,125,635	6	S	0.00011	\$1,004	N	0.0005	Y	1	17	0.001868355	\$17,049.93	R
134054	\$295,079	\$2,225,317	\$1,160,000	\$3,680,396	6	S	0.00011	\$405	N	0.002	Y	1	21	0.002307461	\$8,492.37	R
134055	\$126,549	\$45,663	\$580,000	\$752,211	6	S	0.00011	\$83	N	0.0005	Y	1	36	0.003952386	\$2,973.03	R
134059	\$124,986	\$119,466	\$580,000	\$824,452	6	S	0.00011	\$91	N	0.0005	Y	1	36	0.003952386	\$3,258.55	R
134062	\$150,533	\$152,917	\$580,000	\$883,449	6	S	0.00011	\$97	N	0.002	Y	1	26	0.002856071	\$2,523.19	R
134063	\$102,667															



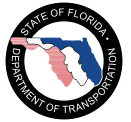
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
134092	\$227,248	\$95,893	\$1,160,000	\$1,483,141	7	S	0.00011	\$163	N	0.002	Y	1	53	0.005813357	\$8,622.03	R
134093	\$716,884	\$180,312	\$1,160,000	\$2,057,196	7	S	0.00011	\$226	N	0.0005	Y	1	54	0.005922718	\$12,184.19	R
134094	\$782,881	\$1,469,970	\$2,900,000	\$5,152,850	7	R	0.000077	\$397	N	0.002	Y	1	55	0.004226207	\$21,777.01	M
134095	\$672,004	\$896,681	\$2,900,000	\$4,468,685	7	S	0.00011	\$492	N	0.002	Y	1	55	0.006032066	\$26,955.40	R
134096	\$893,411	\$68,812	\$580,000	\$1,542,224	7	S	0.00011	\$170	N	0.0005	Y	1	55	0.006032066	\$9,302.80	R
134098	\$1,726,716	\$46,854	\$580,000	\$2,353,570	6	S	0.00011	\$259	N	0.0005	Y	1	55	0.006032066	\$14,196.89	R
134100	\$76,022	NA	\$580,000	\$656,022	6	S	0.00011	\$72	Y	0.0005	Y	1	55	0.006032066	\$3,957.17	R
134101	\$192,699	NA	\$580,000	\$772,699	5	O	0.00032	\$13	Y	0.0005	Y	1	56	0.017763208	\$13,725.61	R
134103	\$174,494	\$167,593	\$1,160,000	\$1,502,086	7	S	0.00011	\$165	N	0.002	Y	1	58	0.00636004	\$9,553.33	R
134106	\$186,037	\$400,113	\$580,000	\$1,166,150	7	S	0.00011	\$128	N	0.002	Y	1	60	0.006578628	\$7,671.67	R
135000	\$144,262	\$52,547	\$1,160,000	\$1,856,809	7	S	0.00011	\$204	N	0.002	Y	1	18	0.00197815	\$3,673.05	T
135001	\$120,218	\$177,874	\$1,160,000	\$1,458,092	7	S	0.00011	\$160	N	0.002	Y	1	18	0.00197815	\$2,884.32	T
140050	\$3,052,798	\$1,295,043	\$2,900,000	\$7,247,841	6	S	0.00011	\$797	N	0.002	Y	1	23	0.002526941	\$18,314.87	T
140064	\$2,999,997	\$580,518	\$1,160,000	\$4,740,515	7	R	0.000077	\$365	N	0.0005	Y	1	51	0.003919465	\$18,580.21	T
144001	\$64,124	NA	\$580,000	\$644,124	7	S	0.00011	\$71	Y	0.0005	Y	1	15	0.00164873	\$1,061.99	R
144017	\$477,107	\$274,284	\$1,160,000	\$1,911,391	6	S	0.00011	\$210	N	0.0005	Y	1	38	0.004171505	\$7,973.38	R
144024	\$3,452,167	\$1,098,067	\$2,900,000	\$7,450,234	7	S	0.00011	\$820	N	0.0005	Y	1	38	0.004171505	\$31,078.69	T
144025	\$1,532,611	\$404,977	\$2,900,000	\$4,837,587	7	S	0.00011	\$532	N	0.002	Y	1	44	0.004828571	\$23,358.63	R
144026	\$1,521,748	\$480,680	\$2,900,000	\$4,902,428	7	S	0.00011	\$539	N	0.002	Y	1	46	0.005047497	\$24,744.99	R
144033	\$247,460	\$269,684	\$1,160,000	\$1,677,143	6	S	0.00011	\$184	N	0.002	Y	1	49	0.005375995	\$9,015.98	T
144034	\$1,492,561	\$1,338,494	\$2,900,000	\$5,731,055	7	S	0.00011	\$630	N	0.0005	Y	1	54	0.005922718	\$33,943.42	T
144035	\$374,163	\$402,844	\$1,160,000	\$1,937,007	7	S	0.00011	\$213	N	0.0005	Y	1	55	0.006032066	\$11,684.15	T
144036	\$1,328,837	\$2,636,368	\$1,160,000	\$5,125,205	7	S	0.00011	\$564	N	0.002	Y	1	54	0.005922718	\$30,355.14	R
144038	\$638,305	NA	\$580,000	\$1,218,305	7	R	0.000077	\$94	N	0.0005	Y	1	35	0.002691475	\$3,279.04	R
144051	\$6,360,438	\$4,961,147	\$2,900,000	\$14,221,585	7	S	0.00011	\$1,564	N	0.0005	Y	1	69	0.007561683	\$107,539.12	R
144055	\$161,695	\$66,740	\$0	\$228,435	7	S	0.00011	\$25	N	0.0005	Y	1	67	0.007343311	\$1,677.47	R
150009	\$955,939	\$4,997,574	\$2,900,000	\$8,853,513	7	S	0.00011	\$974	N	0.0005	Y	1	15	0.00164873	\$14,597.05	T
150013	\$495,387	\$32,339,331	\$2,900,000	\$35,734,719	6	S	0.00011	\$3,931	Y	0.0005	Y	1	15	0.00164873	\$58,916.91	T
150023	\$997,767	\$3,515,446	\$2,900,000	\$7,413,213	6	S	0.00011	\$815	Y	0.0005	Y	1	15	0.00164873	\$12,222.39	T
150062	\$233,491	\$2,456,338	\$2,900,000	\$5,589,829	7	S	0.00011	\$615	N	0.002	Y	1	15	0.00164873	\$9,216.12	R
150067	\$4,445,595	NA	\$2,900,000	\$7,345,595	7	S	0.00011	\$808	Y	0.002	Y	1	29	0.003185092	\$23,396.40	T
150068	\$33,696,551	NA	\$2,900,000	\$36,596,551	6	S	0.00011	\$4,026	Y	0.002	Y	1	29	0.003185092	\$116,563.39	T
150113	\$398,589	\$1,680,604	\$2,900,000	\$4,979,193	7	S	0.00011	\$548	N	0.002	Y	1	15	0.00164873	\$8,209.35	R
154001	\$993,959	NA	\$1,160,000	\$2,153,959	6	S	0.00011	\$237	N	0.002	Y	1	34	0.00373322	\$8,041.20	T
154002	\$1,002,527	NA	\$1,160,000	\$2,162,527	6	O	0.00017	\$368	Y	0.0002	Y	1	34	0.005763816	\$12,464.41	T
154003	\$317,753	\$223,440	\$1,160,000	\$1,701,192	7	S	0.00011	\$187	N	0.0005	Y	1	22	0.002417207	\$4,112.13	R
154004	\$211,835	NA	\$1,160,000	\$1,371,835	7	S	0.00011	\$151	Y	0.0005	Y	1	24	0.002636663	\$3,617.07	R
154005	\$2,475,376	NA	\$2,900,000	\$5,375,376	7	R	0.000077	\$414	Y	0.0005	Y	1	60	0.004609521	\$24,777.91	T
154050	\$703,047	\$472,770	\$1,160,000	\$2,335,817	6	S	0.00011	\$257	N	0.0005	Y	1	43	0.00471909	\$11,022.93	R
154100	\$256,216	\$269,684	\$1,160,000	\$1,685,899	6	S	0.00011	\$185	N	0.0005	Y	1	15	0.00164873	\$2,779.59	T
154101	\$197,804	\$809,051	\$1,160,000	\$2,166,855	6	S	0.00011	\$238	N	0.0005	Y	1	15	0.00164873	\$3,572.56	T
154111	\$3,263,002	\$2,711,997	\$2,900,000	\$8,874,999	6	S	0.00011	\$976	N	0.0005	Y	1	51	0.0055946	\$49,652.07	R
154140	\$182,432	NA	\$580,000	\$762,432	7	S	0.00011	\$84	Y	0.0005	Y	1	43	0.00471909	\$3,597.99	R
154153	\$1,873,670	\$1,168,626	\$2,900,000	\$5,942,295	7	S	0.00011	\$654	N	0.0005	Y	1	51	0.0055946	\$33,244.76	R
154201	\$1,086,793	\$2,238,029	\$2,900,000	\$6,224,822	6	S	0.00011	\$685	N	0.002	Y	1	51	0.0055946	\$34,825.39	R
154208	\$3,022,394	\$8,995,633	\$2,900,000	\$14,918,027	6	S	0.00011	\$1,641	Y	0.0005	Y	1	16	0.001758549	\$26,234.08	T
154209	\$30,172,253	\$20,779,026	\$2,900,000	\$53,851,278	6	S	0.00011	\$5,924	Y	0.002	Y	1	16	0.001758549	\$94,700.10	T
154252	\$159,510	\$1,653,716	\$2,900,000	\$4,713,226	6	S	0.00011	\$518	N	0.002	Y	1	15	0.00164873	\$7,770.84	R
154353	\$1,241,091	\$387,012	\$1,160,000	\$2,788,102	7	S	0.00011	\$307	N	0.0005	Y	1	40	0.004390575	\$12,241.37	T
154362	\$24,696,329	\$2,432,726	\$2,900,000	\$30,029,055	7	R	0.000077	\$2,312	Y	0.0005	Y	1	59	0.00453287	\$136,117.81	R
154363	\$24,696,329	\$2,432,726	\$2,900,000	\$30,029,055	7	R	0.000077	\$2,312	Y	0.002	Y	1	59	0.00453287	\$136,117.81	R
154364	\$11,179,337	\$19,461,808	\$2,900,000	\$33,541,145	6	S	0.00011	\$3,690	N	0.002	Y	1	59	0.00646934	\$216,989.07	R
154370	\$564,686	\$1,212,725	\$2,900,000	\$4,677,410	6	O	0.00017	\$795	N	0.0005	Y	1	42	0.007115173	\$33,280.58	T
154371	\$827,433	\$699,260	\$1,160,000	\$2,686,693	6	S	0.00011	\$296	Y	0.002	Y	1	28	0.003075431	\$8,262.74	T
154406	\$256,216	\$926,816	\$2,900,000	\$4,083,031	7	R	0.000077	\$314	N	0.002	Y	1	31	0.002384245	\$9,734.95	R
154408	\$20,377,031	\$2,469,549	\$2,900,000	\$25,746,580	7	R	0.000077	\$1,982	N	0.002	Y	1	50	0.003842746	\$98,937.57	T
154549	\$993,959	\$734,985	\$2,900,000	\$4,628,944	7	S	0.00011	\$509	N	0.002	Y	1	50	0.005485204	\$25,390.70	R
154554	\$1,928,328	\$3,233,933	\$2,900,000	\$8,062,261	7	S	0.00011	\$887	N	0.002	Y	1	47	0.005156941	\$41,576.61	R
154556	\$1,699,394	\$3,638,175	\$2,900,000	\$8,237,569	7	S	0.00011	\$906	N	0.002	Y	1	47	0.005156941	\$42,480.66	R
154559	\$4,313,804	\$2,263,753	\$2,900,000	\$9,477,557	8	S	0.000022	\$21	N	0.002	Y	1	59	0.00129792	\$1,230.11	R
154700	\$1,280,211	NA	\$1,160,000	\$2,440,211	6	S	0.00011	\$268	Y	0.002	Y	1	23	0.002526941	\$6,166.27	T
154701	\$1,053,939	NA	\$1,160,000	\$2,213,939	7	O	0.00017	\$376	Y	0.002	Y	1	23	0.003902697	\$8,640.33	T
155000	\$115,011	NA	\$580,000	\$695,011	7	S	0.00011	\$76	Y	0.002	Y	1	16	0.001758549	\$1,222.21	T
155001	\$115,011	NA	\$580,000	\$695,011	7	S	0.00011	\$76	Y	0.002	Y	1	16	0.001758549	\$1,222.21	T
155003	\$436,999	\$238,932	\$1,160,000	\$1,835,931	7	R	0.000077	\$141	N	0.0005	Y	1	58	0.004456213	\$8,181.30	R
155200	\$215,971	NA	\$1,160,000	\$1,375,971	6	S	0.00011	\$151	Y	0.0005	Y	1	31	0.003404379	\$4,684.33	T
155501	\$190,429	\$263,872	\$1,160,000	\$1,614,301	6	S	0.00011	\$178	N	0.0005	Y	1	31	0.003404379	\$5,495.69	T
155502	\$190,429	\$263,872	\$1,160,000	\$1,614,301	6	S	0.00011	\$178	Y	0.0005	Y	1	31	0.003404379	\$5,495.69	T
155507	\$438,919	\$1,041,744	\$1,160,000	\$2,640,663	6	S	0.00011	\$290	N	0.0005	Y	1	41	0.004500092	\$11,883.23	R
155701	\$340,347	\$116,811	\$580,000	\$1,037,158	7	S	0.00011	\$114	N	0.0005	Y	1	52	0.005703985	\$5,915.93	R
155703	\$366,666	\$46,725	\$580,000	\$993,391	5	S	0.00024	\$3	N	0.0001	N	1	52	0.012403927	\$12,321.95	R
156311	\$230,744	\$0	\$580,000	\$810,744	7	S	0.00011	\$89	N	0.0001	N	1	55	0.00603		



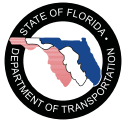
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
157105	\$312,754	\$297,960	\$1,160,000	\$1,770,714	7	S	0.00011	\$195	N	0.002	Y	1	15	0.00164873	\$2,919.43	T
157111	\$199,978	\$40,098	\$580,000	\$820,076	7	O	0.00017	\$139	N	0.001	Y	1	35	0.005932837	\$4,865.38	T
157117	\$2,178,331	\$1,554,346	\$2,900,000	\$6,632,677	6	R	0.000077	\$511	N	0.001	Y	1	15	0.001154378	\$7,656.61	R
157124	\$1,018,713	\$2,947,941	\$2,900,000	\$6,866,653	7	O	0.00017	\$1,167	N	0.0005	Y	1	15	0.002546968	\$17,489.14	R
157125	\$815,251	\$3,154,628	\$2,900,000	\$6,869,879	7	S	0.00011	\$756	N	0.0005	Y	1	15	0.00164873	\$11,326.58	R
157127	\$379,579	\$111,085	\$1,160,000	\$1,650,664	6	R	0.000077	\$127	N	0.001	Y	1	15	0.001154378	\$1,905.49	R
157128	\$1,128,317	NA	\$1,160,000	\$2,288,317	6	S	0.00011	\$252	Y	0.001	Y	1	31	0.003404379	\$7,790.30	T
157130	\$2,759,093	\$1,774,547	\$2,900,000	\$7,433,640	7	R	0.000077	\$572	N	0.0002	Y	1	46	0.00353587	\$26,284.39	R
157152	\$158,636	NA	\$580,000	\$738,636	6	S	0.00011	\$81	Y	0.0005	Y	1	26	0.002856071	\$2,109.60	T
157154	\$5,625,753	\$9,619,334	\$2,900,000	\$18,145,088	6	S	0.00011	\$1,996	N	0.002	Y	1	27	0.002965757	\$53,813.92	T
157159	\$1,113,919	NA	\$1,160,000	\$2,273,919	6	S	0.00011	\$250	Y	0.0005	Y	1	42	0.004609597	\$10,481.85	T
157160	\$454,495	\$923,671	\$2,900,000	\$4,278,166	6	S	0.00011	\$471	N	0.0005	Y	1	23	0.002526941	\$10,810.67	R
157174	\$1,721,339	\$0	\$2,900,000	\$4,621,339	6	S	0.00011	\$508	N	0.001	Y	1	29	0.003185092	\$14,719.39	T
157179	\$414,442	\$151,194	\$1,160,000	\$1,725,636	6	S	0.00011	\$190	N	0.001	Y	1	33	0.003623618	\$6,253.05	T
157181	\$389,380	\$87,715	\$580,000	\$1,057,095	6	S	0.00011	\$116	N	0.001	Y	1	41	0.004500092	\$4,757.02	R
157182	\$526,970	\$202,345	\$1,160,000	\$1,889,314	6	S	0.00011	\$208	N	0.002	Y	1	42	0.004609597	\$8,708.98	R
157185	\$255,466	\$564,676	\$1,160,000	\$1,980,143	7	S	0.00011	\$218	N	0.001	Y	1	23	0.002526941	\$5,003.70	T
157186	\$254,951	\$263,463	\$1,160,000	\$1,678,414	6	S	0.00011	\$185	N	0.002	Y	1	23	0.002526941	\$4,241.25	T
157187	\$155,523	\$647,241	\$1,160,000	\$1,962,764	6	S	0.00011	\$216	N	0.001	Y	1	23	0.002526941	\$4,959.79	T
157189	\$1,431,590	\$3,397,962	\$1,160,000	\$5,989,553	6	S	0.00011	\$659	N	0.001	Y	1	31	0.003404379	\$20,390.71	T
157191	\$3,394,044	\$3,586,350	\$2,900,000	\$9,880,394	7	S	0.00011	\$1,087	N	0.001	Y	1	15	0.00164873	\$16,290.10	T
157196	\$1,180,689	\$793,198	\$1,160,000	\$3,133,887	6	S	0.00011	\$345	N	0.0005	Y	1	21	0.002307461	\$7,231.32	T
157197	\$740,389	\$611,654	\$1,160,000	\$2,512,043	7	S	0.00011	\$276	Y	0.002	Y	1	27	0.002965757	\$7,450.11	T
157198	\$869,222	\$0	\$2,900,000	\$3,769,222	7	S	0.00011	\$415	N	0.001	Y	1	61	0.006687905	\$25,208.20	T
157201	\$502,458	\$203,797	\$1,160,000	\$1,866,255	7	O	0.00017	\$317	Y	0.002	Y	1	33	0.005594768	\$10,441.26	T
157202	\$507,046	NA	\$1,160,000	\$1,667,046	6	O	0.00017	\$283	Y	0.002	Y	1	33	0.005594768	\$9,326.73	T
157205	\$515,451	\$142,491	\$1,160,000	\$1,817,942	7	S	0.00011	\$200	N	0.002	Y	1	41	0.004500092	\$8,180.91	R
157210	\$878,774	NA	\$1,160,000	\$2,038,774	7	S	0.00011	\$224	Y	0.0005	Y	1	69	0.007561838	\$15,416.56	T
157236	\$508,217	\$247,951	\$1,160,000	\$1,916,168	6	O	0.00017	\$326	N	0.0005	Y	1	44	0.007452726	\$14,280.67	T
157237	\$884,143	\$0	\$2,900,000	\$3,784,143	6	S	0.00011	\$416	N	0.0005	Y	1	44	0.004828571	\$18,272.00	T
157238	\$560,963	\$284,893	\$1,160,000	\$2,005,856	6	S	0.00011	\$221	N	0.002	Y	1	44	0.004828571	\$9,685.42	T
157239	\$123,894	\$0	\$1,160,000	\$1,283,894	7	S	0.00011	\$141	N	0.002	Y	1	44	0.004828571	\$6,199.37	T
157402	\$706,466	\$487,589	\$2,900,000	\$4,094,054	7	S	0.00011	\$450	N	0.002	Y	1	49	0.005375795	\$22,008.79	R
157403	\$540,525	\$1,124,086	\$2,900,000	\$4,564,611	7	S	0.00011	\$502	N	0.002	Y	1	49	0.005375795	\$24,538.41	R
157406	\$448,721	\$53,979	\$1,160,000	\$1,662,700	7	S	0.00011	\$183	N	0.002	Y	1	49	0.005375795	\$8,938.33	R
157408	\$1,092,565	NA	\$580,000	\$1,672,565	7	O	0.00017	\$284	Y	0.001	Y	1	50	0.008464694	\$14,157.75	T
157503	\$379,266	NA	\$1,160,000	\$1,539,266	7	S	0.00011	\$169	Y	0.002	Y	1	56	0.006141403	\$9,453.25	T
157701	\$554,104	\$712,981	\$1,160,000	\$2,427,085	7	S	0.00011	\$267	N	0.002	Y	1	43	0.004719009	\$11,453.63	T
157702	\$757,721	\$1,203,905	\$2,900,000	\$4,861,626	5	S	0.00024	\$17	N	0.0002	N	1	52	0.012403927	\$60,303.25	T
157703	\$122,823	NA	\$580,000	\$702,823	8	R	0.0000017	\$1	Y	0.0005	Y	1	61	0.000103695	\$72.88	T
157860	\$419,284	NA	\$2,900,000	\$3,319,284	6	O	0.00017	\$564	Y	0.002	Y	1	24	0.004072034	\$13,516.24	T
157880	\$160,603	NA	\$1,160,000	\$1,320,603	6	O	0.00017	\$225	Y	0.002	Y	1	22	0.003733332	\$4,930.25	T
160037	\$397,996	\$136,563,484	\$2,900,000	\$139,861,480	7	S	0.00011	\$15,385	Y	0.0002	Y	1	15	0.00164873	\$230,593.83	R
160039	\$479,218	\$136,563,484	\$2,900,000	\$139,942,702	7	S	0.00011	\$15,394	Y	0.0005	Y	1	15	0.00164873	\$230,727.75	R
160045	\$1,608,214	\$1,194,579	\$2,900,000	\$5,702,793	4	S	0.0005	\$2,851	Y	0.0002	N	1	17	0.008466085	\$48,280.33	R
160086	\$1,291,847	\$2,368,916	\$1,160,000	\$4,820,763	6	S	0.00011	\$530	N	0.002	Y	1	38	0.004171505	\$20,109.84	R
160087	\$2,597,670	\$1,060,764	\$1,160,000	\$4,818,434	6	S	0.00011	\$530	N	0.0005	Y	1	37	0.004061952	\$19,572.25	R
160093	\$826,036	\$619,099	\$1,160,000	\$2,605,135	7	S	0.00011	\$287	N	0.0002	Y	1	38	0.004171505	\$10,867.33	R
160094	\$1,311,544	\$12,204,414	\$2,900,000	\$16,415,958	6	S	0.00011	\$1,806	N	0.0005	Y	1	20	0.002197703	\$36,077.39	R
160107	\$1,159,572	\$681,063	\$1,160,000	\$3,000,635	7	R	0.000077	\$231	N	0.0005	Y	1	27	0.00207692	\$6,232.08	R
160111	\$925,410	\$3,577,619	\$1,160,000	\$5,663,029	7	S	0.00011	\$623	N	0.0005	Y	1	32	0.003514005	\$19,899.91	R
160212	\$1,542,859	\$118,655	\$580,000	\$2,241,514	7	S	0.00011	\$247	N	0.002	Y	1	49	0.005375795	\$12,049.92	R
160400	\$458,678	NA	\$0	\$458,678	6	S	0.00011	\$50	Y	0.0002	Y	1	30	0.003294742	\$1,511.23	R
164104	\$175,555	\$1,007,219	\$2,900,000	\$4,082,774	7	S	0.00011	\$449	N	0.0001	N	1	26	0.002856071	\$11,660.69	R
164111	\$124,042	\$40,778	\$580,000	\$744,820	6	S	0.00011	\$82	N	0.0002	Y	1	26	0.002856071	\$2,127.26	R
164117	\$358,898	\$1,117,056	\$1,160,000	\$2,635,955	6	S	0.00011	\$290	N	0.0005	Y	1	15	0.00164873	\$4,345.98	R
164121	\$191,857	\$55,420	\$580,000	\$827,277	7	S	0.00011	\$91	N	0.0002	Y	1	26	0.002856071	\$2,362.76	R
164131	\$108,239	\$96,265	\$1,160,000	\$1,364,504	7	O	0.00017	\$232	N	0.0002	Y	1	26	0.00441062	\$6,018.31	R
164136	\$196,540	\$810,428	\$1,160,000	\$2,166,968	7	S	0.00011	\$238	N	0.0002	Y	1	26	0.002856071	\$6,189.01	R
164137	\$272,697	\$6,676,479	\$1,160,000	\$8,109,176	7	S	0.00011	\$892	N	0.002	Y	1	26	0.002856071	\$23,160.38	R
164139	\$272,697	\$6,763,557	\$1,160,000	\$8,196,254	7	S	0.00011	\$902	N	0.002	Y	1	26	0.002856071	\$23,409.08	R
164140	\$217,306	\$3,297,387	\$1,160,000	\$4,674,693	6	O	0.00017	\$795	N	0.002	Y	1	26	0.00441062	\$20,618.30	R
164142	\$200,218	\$621,465	\$580,000	\$1,401,684	6	S	0.00011	\$154	N	0.002	Y	1	26	0.002856071	\$4,003.31	R
164144	\$137,210	\$423,540	\$580,000	\$1,140,750	6	O	0.00017	\$194	N	0.0002	Y	1	26	0.00441062	\$5,031.42	R
164146	\$183,874	\$1,333,083	\$580,000	\$2,096,957	6	S	0.00011	\$231	N	0.002	Y	1	15	0.00164873	\$3,457.32	R
164148	\$407,009	\$4,130,527	\$1,160,000	\$5,697,536	6	S	0.00011	\$627	N	0.002	Y	1	26	0.002856071	\$16,272.57	R
164149	\$402,725	\$4,007,345	\$1,160,000	\$5,570,070	6	S	0.00011	\$613	N	0.002	Y	1	26	0.002856071	\$15,908.52	R
164170	\$547,954	\$1,932,863	\$2,900,000	\$5,380,817	7	S	0.00011	\$592	N	0.0005	Y	1	53	0.005813357	\$31,280.61	R
164171	\$1,157,715	\$1,319,274	\$2,900,000	\$5,376,989	7	S	0.00011	\$591	N	0.002	Y	1	57	0.006250727	\$33,610.09	R
164201	\$128,178	\$898,678	\$1,160,000	\$2,186,856	7	S	0.00011	\$241	N	0.002	Y	1	26	0.002856071	\$6,245.82	R
164202	\$364,166	\$376,851	\$1,160,000	\$1,901,017	7	S	0.00011	\$209	N	0.0002	Y	1	30	0.003294742	\$6,263.36	R
164204	\$468,417	\$438,027	\$1,160,000	\$2,066,444	7	S	0.00011	\$227	N	0.0002	Y	1	26	0.002856071	\$5,901	



Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
164222	\$1,132,711	\$1,866,101	\$2,900,000	\$5,898,812	7	S	0.00011	\$649	N	0.0002	Y	1	50	0.005485204	\$32,356.18	R
164301	\$230,369	\$1,686,991	\$1,160,000	\$3,077,360	7	S	0.00011	\$339	N	0.0005	Y	1	26	0.002856071	\$8,789.16	R
164304	\$215,113	\$1,050,590	\$1,160,000	\$2,425,702	7	S	0.00011	\$267	N	0.002	Y	1	26	0.002856071	\$6,927.98	R
164308	\$190,501	\$3,993,960	\$580,000	\$4,764,461	7	R	0.000077	\$367	Y	0.0005	Y	1	26	0.002000074	\$9,529.28	R
164309	\$200,733	\$336,700	\$580,000	\$1,117,434	7	S	0.00011	\$123	N	0.0005	Y	1	26	0.002856071	\$3,191.47	R
164310	\$196,888	\$324,966	\$580,000	\$1,101,853	7	S	0.00011	\$121	N	0.0005	Y	1	26	0.002856071	\$3,146.97	R
164311	\$287,142	\$315,984	\$580,000	\$1,183,126	6	S	0.00011	\$130	N	0.0002	Y	1	26	0.002856071	\$3,379.09	R
164315	\$131,854	\$80,686	\$580,000	\$792,540	7	S	0.00011	\$87	N	0.002	Y	1	15	0.00164873	\$1,306.68	R
164320	\$154,797	\$3,634,375	\$1,160,000	\$4,949,172	6	S	0.00011	\$544	N	0.002	Y	1	15	0.00164873	\$8,159.85	R
164321	\$99,010	\$201,246	\$580,000	\$880,256	6	S	0.00011	\$97	N	0.002	Y	1	26	0.002856071	\$2,514.07	R
164322	\$188,990	\$662,496	\$580,000	\$1,431,486	6	S	0.00011	\$157	N	0.002	Y	1	21	0.002307461	\$3,303.10	R
164324	\$217,571	\$1,035,888	\$2,900,000	\$4,153,458	6	S	0.00011	\$457	N	0.002	Y	1	27	0.002965757	\$12,318.15	R
164325	\$87,778	NA	\$0	\$87,778	7	S	0.00011	\$10	Y	0.002	Y	1	26	0.002856071	\$250.70	R
164326	\$230,369	\$3,983,618	\$2,900,000	\$7,113,987	7	S	0.00011	\$783	N	0.002	Y	1	15	0.00164873	\$11,729.04	R
164327	\$111,045	\$73,745	\$580,000	\$764,790	6	S	0.00011	\$84	N	0.002	Y	1	26	0.002856071	\$2,184.29	R
164338	\$708,339	\$8,573,645	\$2,900,000	\$12,181,983	6	S	0.00011	\$1,340	N	0.002	Y	1	42	0.004609597	\$56,154.03	R
164344	\$92,744	\$127,372	\$580,000	\$800,116	7	S	0.00011	\$88	N	0.002	Y	1	26	0.002856071	\$2,285.19	R
164345	\$243,168	\$12,646,079	\$1,160,000	\$14,049,247	7	S	0.00011	\$1,545	Y	0.002	Y	1	34	0.00373322	\$52,448.93	R
164346	\$542,035	\$918,992	\$1,160,000	\$2,621,027	7	S	0.00011	\$288	N	0.002	Y	1	55	0.006032066	\$15,810.21	R
164402	\$318,771	\$277,179	\$0	\$595,950	6	S	0.00011	\$66	N	0.002	Y	1	26	0.002856071	\$1,702.08	R
164405	\$175,976	\$148,190	\$580,000	\$904,166	6	O	0.00017	\$154	N	0.0005	Y	1	26	0.00441062	\$3,987.93	R
164406	\$194,896	\$153,046	\$580,000	\$927,942	7	S	0.00011	\$102	N	0.0005	Y	1	26	0.002856071	\$2,650.27	R
164407	\$99,148	\$523,196	\$580,000	\$1,202,344	6	O	0.00017	\$204	N	0.002	Y	1	26	0.00441062	\$5,303.08	R
164408	\$96,555	\$523,196	\$580,000	\$1,199,752	6	S	0.00011	\$132	N	0.002	Y	1	26	0.002856071	\$3,426.58	R
164414	\$103,967	\$932,761	\$1,160,000	\$2,196,727	6	S	0.00011	\$242	N	0.0002	Y	1	26	0.002856071	\$6,274.01	R
164420	\$346,490	\$4,987,597	\$2,900,000	\$8,234,088	6	S	0.00011	\$906	N	0.0005	Y	1	26	0.002856071	\$23,517.14	R
164422	\$127,515	\$1,110,496	\$1,160,000	\$2,398,010	7	S	0.00011	\$264	N	0.002	Y	1	26	0.002856071	\$6,848.89	R
164441	\$173,298	\$175,649	\$580,000	\$928,947	6	S	0.00011	\$102	N	0.002	Y	1	29	0.003185092	\$2,958.78	R
164450	\$935,407	\$1,618,102	\$1,160,000	\$3,713,509	7	S	0.00011	\$408	N	0.0002	Y	1	55	0.006032066	\$22,400.13	R
164504	\$443,882	\$122,584	\$1,160,000	\$1,726,466	6	R	0.000077	\$133	N	0.0005	Y	1	51	0.00391945	\$6,766.80	R
164505	\$442,009	\$122,584	\$1,160,000	\$1,724,593	6	R	0.000077	\$133	N	0.0005	Y	1	51	0.00391945	\$6,759.46	R
165101	\$175,352	\$122,584	\$1,160,000	\$1,457,936	6	S	0.00011	\$160	N	0.002	Y	1	31	0.003404379	\$4,963.37	R
167001	\$163,178	\$844,389	\$1,160,000	\$2,167,567	6	S	0.00011	\$238	N	0.002	Y	1	27	0.002965757	\$6,428.48	R
170014	\$525,354	\$1,451,595	\$2,900,000	\$4,876,949	6	S	0.00011	\$536	Y	0.0005	Y	1	15	0.00164873	\$8,040.77	T
170031	\$1,087,979	\$1,689,347	\$2,900,000	\$5,677,326	6	S	0.00011	\$625	Y	0.002	Y	1	15	0.00164873	\$9,360.38	R
170032	\$4,336,060	\$5,711,954	\$2,900,000	\$12,948,014	7	S	0.00011	\$1,424	N	0.002	Y	1	40	0.004390575	\$56,849.23	T
170033	\$436,578	\$1,689,347	\$2,900,000	\$5,025,924	6	R	0.000077	\$387	Y	0.002	Y	1	15	0.001154378	\$5,801.81	R
170056	\$1,075,056	\$4,014,716	\$2,900,000	\$7,989,772	7	R	0.000077	\$615	N	0.002	Y	1	37	0.002845055	\$22,731.34	R
170058	\$19,191,622	\$5,800,344	\$1,160,000	\$26,151,966	7	S	0.00011	\$2,877	Y	0.0002	Y	1	30	0.003294742	\$86,163.98	T
170064	\$6,851,337	\$3,319,071	\$1,160,000	\$11,330,408	6	S	0.00011	\$1,246	Y	0.002	Y	1	15	0.00164873	\$18,680.78	T
170066	\$1,424,637	\$6,210,962	\$1,160,000	\$8,795,599	5	S	0.00024	\$30	N	0.002	Y	1	20	0.004789072	\$42,122.75	R
170120	\$1,256,730	\$665,239	\$2,900,000	\$4,821,969	7	S	0.00011	\$530	Y	0.002	Y	1	42	0.004609597	\$22,227.33	T
170141	\$1,256,730	\$665,239	\$2,900,000	\$4,821,969	6	S	0.00011	\$530	Y	0.002	Y	1	42	0.004609597	\$22,227.33	T
170400	\$139,954	NA	\$0	\$139,954	6	S	0.00011	\$15	Y	0.002	Y	1	53	0.005813357	\$813.60	M
170401	\$928,266	\$1,864,732	\$1,160,000	\$3,952,998	7	S	0.00011	\$435	N	0.002	Y	1	15	0.00164873	\$6,517.43	R
170920	\$1,974,308	\$13,129,721	\$2,900,000	\$18,004,029	7	S	0.00011	\$1,980	Y	0.002	Y	1	15	0.00164873	\$29,683.78	T
174008	\$274,617	\$402,362	\$1,160,000	\$1,836,979	7	S	0.00011	\$202	N	0.0005	Y	1	34	0.00373322	\$6,857.85	R
174009	\$217,727	\$402,362	\$1,160,000	\$1,780,089	7	S	0.00011	\$196	N	0.0005	Y	1	34	0.00373322	\$6,645.46	R
174014	\$138,206	\$180,550	\$1,160,000	\$1,478,756	6	S	0.00011	\$163	N	0.0005	Y	1	25	0.002746373	\$4,061.22	M
174019	\$157,911	\$607,890	\$1,160,000	\$1,925,800	6	S	0.00011	\$212	N	0.0002	Y	1	28	0.003075431	\$5,922.66	R
174022	\$204,195	\$1,834,999	\$1,160,000	\$3,199,194	7	S	0.00011	\$352	N	0.002	Y	1	23	0.002526941	\$8,084.17	R
174025	\$144,696	NA	\$580,000	\$724,696	6	S	0.00011	\$80	N	0.002	Y	1	21	0.002307461	\$1,672.21	M
174028	\$187,175	\$168,210	\$1,160,000	\$1,515,384	6	S	0.00011	\$167	N	0.002	Y	1	25	0.002746373	\$4,161.81	R
174029	\$216,400	\$110,975	\$1,160,000	\$1,487,375	7	S	0.00011	\$164	N	0.0005	Y	1	34	0.00373322	\$5,552.70	T
174030	\$154,516	\$665,220	\$1,160,000	\$1,979,736	6	S	0.00011	\$218	N	0.002	Y	1	22	0.002417207	\$4,785.43	M
174031	\$241,732	\$54,158	\$580,000	\$875,890	6	S	0.00011	\$96	N	0.0002	Y	1	24	0.002636663	\$2,309.43	R
174035	\$191,600	\$810,614	\$1,160,000	\$2,162,213	6	S	0.00011	\$238	N	0.0002	Y	1	25	0.002746373	\$5,938.24	R
174037	\$147,492	\$104,509	\$1,160,000	\$1,412,002	6	S	0.00011	\$155	N	0.0002	Y	1	41	0.004500092	\$6,354.14	R
174039	\$198,155	\$1,149,912	\$1,160,000	\$2,508,067	7	S	0.00011	\$276	N	0.0005	Y	1	27	0.002965757	\$7,438.32	R
174042	\$100,950	\$88,883	\$580,000	\$769,833	6	S	0.00011	\$85	N	0.0002	Y	1	23	0.002526941	\$1,945.32	M
174043	\$124,276	\$139,650	\$1,160,000	\$1,423,926	7	S	0.00011	\$157	N	0.0005	Y	1	24	0.002636663	\$3,754.41	R
174046	\$287,649	\$176,825	\$1,160,000	\$1,624,474	6	S	0.00011	\$179	N	0.002	Y	1	36	0.003952386	\$6,420.55	T
174049	\$2,383,853	\$2,522,468	\$2,900,000	\$7,806,321	6	S	0.00011	\$859	N	0.002	Y	1	35	0.003842809	\$29,998.20	T
174059	\$533,642	\$5,692,766	\$1,160,000	\$7,386,408	7	S	0.00011	\$813	Y	0.002	Y	1	48	0.005266374	\$38,899.59	T
174065	\$5,502,952	\$14,530,225	\$2,900,000	\$22,933,177	7	S	0.00011	\$2,523	Y	0.002	Y	1	52	0.005703985	\$130,810.49	T
174068	\$2,471,818	\$10,147,494	\$2,900,000	\$15,519,312	7	R	0.000077	\$1,195	N	0.002	Y	1	53	0.004072841	\$63,207.68	R
174069	\$2,936,177	\$5,078,451	\$2,900,000	\$10,914,628	7	S	0.00011	\$1,201	N	0.0005	Y	1	56	0.006141403	\$67,031.13	M
174072	\$933,838	\$9,613,160	\$2,900,000	\$13,446,998	7	S	0.00011	\$1,479	N	0.002	Y	1	54	0.005922718	\$79,642.78	R
174073	\$837,008	\$8,010,967	\$2,900,000	\$11,747,975	7	R	0.000077	\$905	N	0.0001	Y	1	54	0.004149527	\$48,748.54	R
174075	\$905,182	\$2,622,621	\$2,900,000	\$6,427,803	7	S	0.00011	\$707	N	0.0001	N	1	56	0.006141403	\$39,475.73	R
174078	\$412,792	\$714,407	\$1,160,000	\$2,287,199	7	S	0.00011	\$252	N	0.0001	N	1	57	0.006250727	\$14,296.66	R
174079	\$4,038,016	\$6,515,143	\$2,900,000	\$13,453,159	7	S	0.00011	\$1,480	N	0.002	Y	1	58			



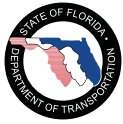
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
175010	\$698,904	\$2,064,531	\$1,160,000	\$3,923,435	7	S	0.00011	\$432	N	0.0005	Y	1	36	0.003952386	\$15,506.93	R
175012	\$706,419	\$3,701,856	\$1,160,000	\$5,568,274	7	S	0.00011	\$613	N	0.002	Y	1	37	0.004061952	\$22,618.06	R
175013	\$1,472,584	\$11,251,370	\$2,900,000	\$15,623,954	6	S	0.00011	\$1,719	N	0.002	Y	1	38	0.004171505	\$65,175.40	R
175014	\$4,078,191	\$7,931,644	\$2,900,000	\$14,909,835	6	S	0.00011	\$1,640	N	0.002	Y	1	39	0.004281046	\$63,829.69	R
175018	\$1,313,105	\$3,571,876	\$1,160,000	\$6,044,981	6	S	0.00011	\$665	N	0.002	Y	1	49	0.005375795	\$32,496.58	R
175019	\$1,313,105	\$3,571,876	\$1,160,000	\$6,044,981	7	S	0.00011	\$665	N	0.001	Y	1	49	0.005375795	\$32,496.58	R
175024	\$780,867	\$11,548	\$0	\$792,416	7	S	0.00011	\$87	N	0.001	Y	1	51	0.0055946	\$4,433.25	R
175025	\$858,954	\$44,282	\$580,000	\$1,483,236	7	S	0.00011	\$163	N	0.001	Y	1	51	0.0055946	\$8,298.11	R
175026	\$1,179,472	\$5,093,396	\$1,160,000	\$7,432,868	6	S	0.00011	\$818	N	0.001	Y	1	52	0.005703985	\$42,396.97	R
175027	\$757,128	\$582,039	\$1,160,000	\$2,499,167	6	S	0.00011	\$275	Y	0.001	Y	1	51	0.0055946	\$13,981.84	R
175028	\$1,514,256	\$2,742,483	\$1,160,000	\$5,416,739	6	S	0.00011	\$596	Y	0.002	Y	1	51	0.0055946	\$30,304.49	R
175029	\$976,084	\$1,118,339	\$1,160,000	\$3,254,423	6	S	0.00011	\$358	Y	0.002	Y	1	51	0.0055946	\$18,207.20	R
175030	\$561,408	NA	\$0	\$561,408	7	S	0.00011	\$62	Y	0.002	Y	1	54	0.005922718	\$3,325.06	R
175033	\$1,117,728	\$72,395	\$0	\$1,190,122	6	S	0.00011	\$131	N	0.002	Y	1	54	0.005922718	\$7,048.76	R
175034	\$710,052	\$142,307	\$580,000	\$1,432,360	6	S	0.00011	\$158	N	0.002	Y	1	54	0.005922718	\$8,483.46	R
175036	\$2,132,632	\$3,579,836	\$2,900,000	\$8,612,468	7	R	0.00077	\$663	Y	0.002	Y	1	59	0.00453287	\$39,039.20	R
175037	\$1,071,217	\$615,124	\$1,160,000	\$2,846,341	7	S	0.00011	\$313	N	0.0005	Y	1	59	0.00646934	\$18,413.95	R
175505	\$129,982	NA	\$580,000	\$709,982	7	S	0.00011	\$78	Y	0.0005	Y	1	29	0.003185092	\$2,261.36	T
175550	\$525,413	NA	\$1,160,000	\$1,685,413	7	S	0.00011	\$185	Y	0.002	Y	1	26	0.002856071	\$4,813.66	T
175575	\$630,495	NA	\$1,160,000	\$1,790,495	7	S	0.00011	\$197	Y	0.002	Y	1	26	0.002856071	\$5,113.78	T
175600	\$1,692,933	\$612,182	\$1,160,000	\$3,465,115	6	S	0.00011	\$381	N	0.002	Y	1	41	0.004500092	\$15,593.34	T
175615	\$622,746	NA	\$1,160,000	\$1,782,746	7	S	0.00011	\$196	Y	0.002	Y	1	26	0.002856071	\$5,091.65	T
175620	\$622,746	NA	\$1,160,000	\$1,782,746	6	S	0.00011	\$196	Y	0.002	Y	1	26	0.002856071	\$5,091.65	T
175624	\$2,376,424	\$3,086,936	\$2,900,000	\$8,363,360	7	S	0.00011	\$920	N	0.0002	Y	1	48	0.005266374	\$44,044.58	T
175630	\$266,844	\$818,002	\$1,160,000	\$2,244,846	7	S	0.00011	\$247	N	0.0005	Y	1	31	0.003404379	\$7,642.31	T
175650	\$491,361	\$2,271,103	\$2,900,000	\$5,662,464	6	S	0.00011	\$623	N	0.0005	Y	1	15	0.00164873	\$9,335.87	M
175660	\$156,267	\$54,158	\$580,000	\$790,425	7	S	0.00011	\$87	N	0.0005	Y	1	15	0.00164873	\$1,303.20	T
175670	\$125,261	\$92,387	\$580,000	\$797,648	6	S	0.00011	\$88	N	0.002	Y	1	21	0.002307461	\$1,840.54	T
175680	\$333,442	\$0	\$2,900,000	\$3,233,442	7	S	0.00011	\$356	N	0.001	Y	1	25	0.002746373	\$8,880.24	R
175690	\$59,128	\$21,451	\$580,000	\$660,579	7	S	0.00011	\$73	N	0.002	Y	1	24	0.002636663	\$1,741.72	M
175700	\$117,175	\$63,715	\$580,000	\$760,890	7	S	0.00011	\$84	N	0.002	Y	1	26	0.002856071	\$2,173.16	R
175710	\$137,777	\$63,715	\$580,000	\$781,492	7	S	0.00011	\$86	N	0.002	Y	1	21	0.002307461	\$1,803.26	R
175760	\$545,722	NA	\$1,160,000	\$1,705,722	7	S	0.00011	\$188	Y	0.001	Y	1	42	0.004609597	\$7,862.69	R
175950	\$457,024	\$4,189,413	\$2,900,000	\$7,546,437	7	S	0.00011	\$830	N	0.002	Y	1	15	0.00164873	\$12,442.04	T
175970	\$262,677	\$1,935,058	\$1,160,000	\$3,357,735	7	S	0.00011	\$369	N	0.001	Y	1	21	0.002307461	\$7,747.84	R
175995	\$190,499	\$515,374	\$1,160,000	\$1,865,873	6	S	0.00011	\$205	N	0.002	Y	1	22	0.002417207	\$4,510.20	R
176000	\$244,728	NA	\$0	\$244,728	7	O	0.00017	\$42	N	0.002	Y	1	36	0.006101828	\$1,493.29	R
176003	\$892,330	\$858,085	\$1,160,000	\$2,910,414	7	S	0.00011	\$320	N	0.002	Y	1	50	0.005485204	\$15,964.21	M
180805	\$214,684	\$32,319	\$0	\$247,003	6	S	0.00011	\$27	N	0.002	Y	1	34	0.00373322	\$922.12	R
184000	\$116,093	\$117,511	\$580,000	\$813,604	5	S	0.00024	\$3	N	0.0005	Y	1	15	0.003593958	\$2,924.06	R
184002	\$175,805	\$104,141	\$580,000	\$859,946	6	S	0.00011	\$95	N	0.002	Y	1	29	0.003185092	\$2,739.01	R
184006	\$2,305,448	\$10,735,036	\$1,160,000	\$14,200,484	6	S	0.00011	\$1,562	N	0.002	Y	1	15	0.00164873	\$23,412.77	R
184008	\$822,056	\$6,541,713	\$2,900,000	\$10,263,769	7	S	0.00011	\$1,129	N	0.002	Y	1	21	0.002307461	\$23,683.24	R
184019	\$1,603,220	\$5,601,818	\$1,160,000	\$8,365,038	7	S	0.00011	\$920	N	0.002	Y	1	17	0.001868355	\$15,628.86	R
184052	\$278,480	\$1,818,020	\$1,160,000	\$3,256,500	6	O	0.00017	\$554	N	0.001	Y	1	21	0.003563938	\$11,605.96	R
184053	\$556,960	\$1,008,781	\$1,160,000	\$2,725,741	6	S	0.00011	\$300	N	0.002	Y	1	23	0.002526941	\$6,887.79	R
184054	\$769,747	\$9,067,156	\$1,160,000	\$10,996,903	6	S	0.00011	\$1,210	N	0.002	Y	1	23	0.002526941	\$27,788.53	R
184055	\$461,453	\$322,275	\$580,000	\$1,363,728	7	S	0.00011	\$150	N	0.002	Y	1	34	0.00373322	\$5,091.10	R
184059	\$371,322	NA	\$0	\$371,322	4	S	0.0005	\$186	Y	0.002	Y	1	31	0.01538431	\$5,712.53	R
184065	\$1,275,529	\$5,601,818	\$1,160,000	\$8,037,347	7	S	0.00011	\$884	N	0.002	Y	1	44	0.004828571	\$38,808.90	R
260006	\$2,208,173	\$32,490,840	\$2,900,000	\$37,599,013	6	S	0.00011	\$4,136	Y	0.0005	Y	1	15	0.00164873	\$61,900.62	R
260017	\$585,522	\$4,513,787	\$1,160,000	\$6,259,309	5	S	0.00024	\$21	N	0.0005	Y	1	21	0.005027922	\$31,471.32	R
260024	\$779,744	\$3,220,446	\$1,160,000	\$5,160,189	5	S	0.00024	\$18	N	0.0005	Y	1	24	0.00574413	\$29,640.80	R
260027	\$581,542	\$1,320,589	\$1,160,000	\$3,062,130	6	S	0.00011	\$337	N	0.0005	Y	1	15	0.00164873	\$5,048.63	R
260033	\$1,980,301	\$9,878,373	\$2,900,000	\$14,758,674	6	S	0.00011	\$1,623	N	0.0005	Y	1	25	0.002746373	\$40,532.82	R
260038	\$2,799,080	\$5,121,640	\$2,900,000	\$10,820,719	6	S	0.00011	\$1,190	Y	0.002	Y	1	23	0.002526941	\$27,343.32	R
260086	\$1,831,872	\$1,023,446	\$1,160,000	\$4,015,318	6	S	0.00011	\$442	N	0.002	Y	1	16	0.001758549	\$7,061.13	R
262501	\$686,051	\$1,460,529	\$1,160,000	\$3,306,580	7	S	0.00011	\$364	N	0.002	Y	1	51	0.0055946	\$18,498.99	R
264126	\$121,140	\$141,083	\$580,000	\$842,224	6	O	0.00017	\$143	N	0.0005	Y	1	15	0.002546968	\$2,145.12	R
270020	\$1,441,076	\$1,595,934	\$1,160,000	\$4,197,010	5	S	0.00024	\$14	N	0.0001	N	1	15	0.003593958	\$15,083.88	R
270024	\$590,251	\$295,341	\$1,160,000	\$2,045,592	4	S	0.0005	\$1,023	N	0.0001	N	1	16	0.00797007	\$16,303.51	R
270027	\$428,524	\$692,985	\$580,000	\$1,701,510	4	S	0.0005	\$851	N	0.0005	N	1	16	0.00797007	\$13,561.15	R
270071	\$43,311	\$1,422	\$0	\$44,733	5	S	0.00024	\$0	N	0.0001	N	1	18	0.004311198	\$192.85	R
270072	\$79,115	\$1,422	\$0	\$80,537	5	S	0.00024	\$0	N	0.0005	Y	1	18	0.004311198	\$347.21	R
270073	\$70,453	\$1,191	\$0	\$71,644	4	S	0.0005	\$36	N	0.0005	N	1	18	0.008961852	\$642.06	R
270074	\$78,538	\$1,422	\$0	\$79,960	5	S	0.00024	\$0	N	0.0005	Y	1	18	0.004311198	\$344.72	R
273001	\$72,435	\$55,072	\$0	\$127,507	5	O	0.00032	\$2	N	0.002	Y	1	39	0.01240442	\$1,581.65	R
273002	\$106,913	\$282,024	\$0	\$388,936	6	S	0.00011	\$43	N	0.0005	Y	1	39	0.004281046	\$1,665.05	R
274091	\$127,682	\$1,025,954	\$580,000	\$813,636	6	O	0.00017	\$138	N	0.0005	Y	1	15	0.002546968	\$2,072.30	R
274092	\$81,310	\$105,954	\$580,000	\$767,264	6	S	0.00011	\$84	N	0.002	Y	1	26	0.002856071	\$2,191.36	R
274094	\$45,075	\$20,161	\$0	\$65,236	7	S	0.00011	\$7	N	0.002	Y	1	15	0.00164873	\$107.56	R
274098	\$43,889	\$8,144	\$0	\$52,033	6	S	0.00011	\$6	N	0.0001	N	1	15	0.00164873	\$85.79	R
274100	\$193,746	\$81,722	\$580,000	\$855,468	6	S	0.00011	\$94	N	0.002	Y	1	15	0.00164873	\$1,410.44	R
274101	\$87,778	\$30,052	\$0													



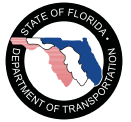
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
274137	\$87,778	\$23,658	\$0	\$111,435	5	S	0.00024	\$0	N	0.002	Y	1	39	0.009317444	\$1,038.29	R
274140	\$45,075	\$309,455	\$0	\$354,530	6	S	0.00011	\$39	Y	0.002	Y	1	49	0.005375795	\$1,905.88	R
274145	\$145,526	\$27,267	\$0	\$172,793	6	S	0.00011	\$19	N	0.002	Y	1	46	0.005047497	\$872.17	R
280003	\$1,936,849	\$28,854,417	\$2,900,000	\$33,691,266	7	S	0.00011	\$3,706	Y	0.002	Y	1	15	0.00164873	\$55,547.80	R
280042	\$275,788	\$0	\$0	\$275,788	6	S	0.00011	\$30	N	0.002	Y	1	15	0.00164873	\$454.70	R
280043	\$413,681	\$758,538	\$1,160,000	\$2,332,220	6	S	0.00011	\$257	N	0.0005	Y	1	15	0.00164873	\$3,845.20	R
280044	\$410,716	\$0	\$0	\$410,716	7	S	0.00011	\$45	N	0.002	Y	1	15	0.00164873	\$677.16	R
280045	\$616,074	\$758,538	\$1,160,000	\$2,534,612	7	S	0.00011	\$279	N	0.002	Y	1	15	0.00164873	\$4,178.89	R
280051	\$377,019	\$1,413,488	\$1,160,000	\$2,950,507	6	S	0.00011	\$325	Y	0.002	Y	1	15	0.00164873	\$4,864.59	R
280052	\$377,019	\$1,413,488	\$1,160,000	\$2,950,507	6	S	0.00011	\$325	Y	0.0005	Y	1	15	0.00164873	\$4,864.59	R
280941	\$2,425,120	\$1,587,567	\$2,900,000	\$6,912,687	6	S	0.00011	\$760	N	0.002	Y	1	15	0.00164873	\$11,397.16	R
284021	\$122,817	\$13,633	\$0	\$136,450	5	S	0.00024	\$0	N	0.0002	N	1	31	0.007413278	\$1,011.54	R
284023	\$118,737	\$211,801	\$580,000	\$910,538	6	S	0.00011	\$100	N	0.0002	Y	1	46	0.005047497	\$4,595.94	R
284024	\$298,799	\$211,801	\$580,000	\$1,090,600	5	S	0.00024	\$4	N	0.0005	Y	1	46	0.010980593	\$11,975.44	R
284025	\$118,737	\$70,600	\$580,000	\$769,337	7	S	0.00011	\$85	N	0.001	Y	1	46	0.005047497	\$3,883.23	R
284026	\$98,360	\$13,633	\$0	\$111,993	5	S	0.00024	\$0	N	0.001	Y	1	44	0.010505693	\$1,176.56	R
284028	\$385,587	\$529,859	\$1,160,000	\$2,075,446	5	S	0.00024	\$7	N	0.002	Y	1	53	0.01264095	\$26,235.61	R
290027	\$2,293,016	\$13,989,856	\$1,160,000	\$17,442,873	6	S	0.00011	\$1,919	N	0.002	Y	0.67	17	0.001868355	\$32,589.48	R
290041	\$433,984	\$317,350	\$580,000	\$1,331,333	5	S	0.00024	\$5	N	0.0002	N	1	17	0.004072176	\$5,421.42	R
290042	\$883,316	\$767,627	\$1,160,000	\$2,810,943	4	S	0.0005	\$1,405	N	0.0005	N	1	17	0.008466085	\$23,397.68	R
290044	\$785,250	\$134,751	\$580,000	\$1,500,001	3	S	0.0013	\$1,950	N	0.002	Y	1	21	0.026948005	\$40,422.03	R
290085	\$1,061,322	\$484,308	\$1,160,000	\$2,705,629	5	S	0.00024	\$9	N	0.0005	Y	1	15	0.003593958	\$9,723.92	R
294070	\$127,768	\$26,489	\$580,000	\$734,256	4	S	0.0005	\$367	N	0.0005	N	1	37	0.018334667	\$13,462.19	R
294090	\$159,186	\$33,744	\$580,000	\$772,929	4	F	0.0007	\$541	N	0.0005	N	1	37	0.025576309	\$19,768.67	R
294130	\$116,152	\$12,023	\$0	\$128,175	6	S	0.00011	\$14	N	0.0005	Y	1	37	0.004061952	\$520.64	R
294370	\$105,680	\$0	\$0	\$105,680	6	S	0.00011	\$12	N	0.0005	Y	1	37	0.004061952	\$429.27	R
294445	\$139,954	\$252,347	\$0	\$392,301	3	O	0.0016	\$628	N	0.002	Y	1	53	0.081366384	\$31,920.11	R
294446	\$171,702	\$42,571	\$580,000	\$794,273	5	S	0.00024	\$3	N	0.002	Y	1	53	0.01264095	\$10,040.37	R
294447	\$279,908	\$24,045	\$0	\$303,953	5	S	0.00024	\$1	N	0.0005	Y	1	52	0.012403927	\$3,770.21	R
294448	\$115,612	\$23,690	\$580,000	\$719,302	6	S	0.00011	\$79	N	0.0005	Y	1	53	0.005813357	\$4,181.56	R
295500	\$72,357	\$0	\$0	\$72,357	1	S	0.01	\$724	N	0.0005	N	1	36	0.303586782	\$21,966.63	R
300002	\$289,191	\$3,501,364	\$1,160,000	\$4,950,554	6	S	0.00011	\$545	N	0.0005	Y	1	15	0.00164873	\$8,162.13	R
300003	\$481,984	\$3,501,364	\$1,160,000	\$5,143,348	6	S	0.00011	\$566	N	0.002	Y	1	15	0.00164873	\$8,479.99	R
300004	\$481,984	\$3,501,364	\$1,160,000	\$5,143,348	6	S	0.00011	\$566	N	0.001	Y	1	15	0.00164873	\$8,479.99	R
300005	\$481,984	\$3,104,983	\$1,160,000	\$4,746,967	6	S	0.00011	\$522	N	0.0005	Y	1	15	0.00164873	\$7,826.47	R
300013	\$294,868	\$935,958	\$1,160,000	\$2,390,826	6	S	0.00011	\$263	N	0.0005	Y	1	21	0.002307461	\$5,516.74	M
300015	\$397,683	NA	\$0	\$397,683	4	S	0.0005	\$199	Y	0.0005	N	1	38	0.0188253	\$7,486.50	T
300022	\$309,341	\$104,655	\$580,000	\$993,995	6	S	0.00011	\$109	N	0.001	Y	1	20	0.002197703	\$2,184.51	R
300038	\$536,123	\$652,440	\$1,160,000	\$2,348,564	7	S	0.00011	\$258	Y	0.002	Y	1	19	0.002087932	\$4,903.64	R
300053	\$411,115	\$104,655	\$580,000	\$1,095,770	6	S	0.00011	\$121	N	0.002	Y	1	21	0.002307461	\$2,528.45	R
300056	\$714,051	\$652,440	\$1,160,000	\$2,526,491	7	S	0.00011	\$278	Y	0.002	Y	1	19	0.002087932	\$5,275.14	R
300057	\$714,051	\$652,440	\$1,160,000	\$2,526,491	7	S	0.00011	\$278	Y	0.002	Y	1	19	0.002087932	\$5,275.14	R
300058	\$714,051	\$652,440	\$1,160,000	\$2,526,491	7	S	0.00011	\$278	Y	0.002	Y	1	19	0.002087932	\$5,275.14	R
310005	\$2,808,585	\$3,958,138	\$1,160,000	\$7,926,723	6	S	0.00011	\$872	N	0.002	Y	1	15	0.00164873	\$13,069.03	R
314000	\$55,626	NA	\$0	\$55,626	5	S	0.00024	\$0	Y	0.002	Y	1	26	0.006221316	\$346.07	R
315250	\$129,793	NA	\$580,000	\$709,793	6	S	0.00011	\$78	Y	0.0005	Y	1	40	0.004390575	\$3,116.40	R
320001	\$741,068	\$1,357,211	\$1,160,000	\$3,258,279	7	S	0.00011	\$358	Y	0.002	Y	1	15	0.00164873	\$5,372.02	R
320004	\$589,385	\$4,543,707	\$1,160,000	\$6,293,091	7	S	0.00011	\$692	Y	0.002	Y	1	15	0.00164873	\$10,375.61	R
320010	\$608,488	\$3,357,622	\$1,160,000	\$5,126,111	7	S	0.00011	\$564	N	0.002	Y	1	34	0.00373322	\$19,136.90	R
320012	\$203,446	\$3,357,622	\$1,160,000	\$4,721,068	6	S	0.00011	\$519	N	0.002	Y	1	29	0.003185092	\$15,037.04	R
320015	\$529,131	\$692,985	\$580,000	\$1,802,117	6	S	0.00011	\$198	N	0.002	Y	1	34	0.00373322	\$6,727.70	R
320021	\$309,422	\$124,899	\$0	\$434,321	7	S	0.00011	\$48	N	0.002	Y	1	29	0.003185092	\$1,383.35	R
320052	\$7,211,685	\$1,792,007	\$1,160,000	\$10,163,692	6	S	0.00011	\$1,118	N	0.002	Y	0.67	50	0.005485204	\$55,749.92	R
324222	\$81,207	\$33,779	\$0	\$114,985	7	O	0.00017	\$20	N	0.002	Y	1	29	0.004918285	\$565.53	R
324232	\$102,261	\$35,623	\$0	\$137,884	6	O	0.00017	\$23	N	0.0005	Y	1	54	0.009138766	\$1,260.09	R
324233	\$322,389	\$71,069	\$580,000	\$973,458	5	S	0.00024	\$3	N	0.002	Y	1	55	0.013114826	\$12,766.73	R
324235	\$137,582	\$27,786	\$0	\$165,367	6	O	0.00017	\$28	N	0.002	Y	1	55	0.009307212	\$1,539.11	R
324304	\$89,931	\$13,539	\$0	\$103,471	7	S	0.00011	\$11	N	0.002	Y	1	61	0.006687905	\$692.00	R
324305	\$151,675	\$29,011	\$0	\$180,687	6	S	0.00011	\$20	N	0.002	Y	1	62	0.006797169	\$1,228.16	R
324306	\$133,555	\$60,104	\$0	\$193,659	7	S	0.00011	\$21	N	0.002	Y	1	62	0.006797169	\$1,316.33	R
330012	\$5,044,399	\$41,792,595	\$2,900,000	\$49,736,994	7	S	0.00011	\$5,471	Y	0.0005	Y	1	20	0.002197703	\$109,307.12	R
330013	\$289,191	\$3,501,364	\$1,160,000	\$4,950,554	6	S	0.00011	\$545	N	0.002	Y	1	15	0.00164873	\$8,162.13	R
330014	\$578,381	\$3,501,364	\$1,160,000	\$5,239,745	6	S	0.00011	\$576	N	0.002	Y	1	15	0.00164873	\$8,638.93	R
330021	\$684,884	\$356,965	\$1,160,000	\$2,201,849	6	S	0.00011	\$242	N	0.002	Y	1	15	0.00164873	\$3,630.25	R
334001	\$392,689	\$19,779	\$0	\$412,468	5	O	0.00032	\$7	N	0.002	Y	1	15	0.004789263	\$1,975.42	R
334005	\$46,776	NA	\$0	\$46,776	6	S	0.00011	\$5	Y	0.002	Y	1	38	0.004171505	\$195.13	R
340008	\$611,986	\$814,246	\$580,000	\$2,006,232	6	S	0.00011	\$221	Y	0.001	Y	1	23	0.002526941	\$5,069.63	M
340012	\$1,142,285	NA	\$580,000	\$1,722,285	6	S	0.00011	\$189	Y	0.0005	Y	1	25	0.002746373	\$4,730.04	T
340025	\$1,932,854	\$251,138	\$1,160,000	\$3,343,992	7	S	0.00011	\$368	Y	0.0005	Y	1	37	0.004061952	\$13,583.13	R
340034	\$1,978,155	\$251,138	\$1,160,000	\$3,389,293	7	S	0.00011	\$373	Y	0.0005	Y	1	37	0.004061952	\$13,767.14	R
340039	\$848,058	\$369,019	\$1,160,000	\$2,377,077	6	S	0.00011	\$261	Y	0.001	Y	1	36	0.003952386	\$9,395.13	R
340045	\$438,341	\$684,154	\$1,160,000	\$2,282,496	7	S	0.00011	\$251	Y	0.0005	Y	1	15	0.00164873	\$3,763.22	R
340049	\$416,959	\$778,655	\$1,160,000	\$2,355,614	6	S	0.00011	\$259	N	0.0005	Y	1	26	0.002856071	\$6,727.80	R
340050	\$625,438	\$778,655	\$1,160,000	\$2,564,094	4	S	0.0005	\$1,282	N	0.0005	N	1	26	0.012919074	\$33,125.72	R
340																



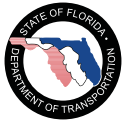
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
344005	\$139,064	NA	\$580,000	\$719,064	6	S	0.00011	\$79	Y	0.0005	Y	1	31	0.003404379	\$2,447.97	R
344007	\$81,940	\$8,144	\$0	\$90,085	5	S	0.00024	\$0	N	0.0005	Y	1	61	0.014535088	\$1,309.39	R
350001	\$2,182,303	\$782,967	\$1,160,000	\$4,125,270	6	S	0.00011	\$454	Y	0.0001	N	1	15	0.00164873	\$6,801.46	R
350007	\$696,200	\$1,404,063	\$1,160,000	\$3,260,262	4	S	0.0005	\$1,630	N	0.0005	N	1	16	0.00797007	\$25,984.52	R
350022	\$408,437	\$749,941	\$580,000	\$1,738,378	6	S	0.00011	\$191	N	0.001	Y	1	29	0.003185092	\$5,536.89	R
350028	\$2,181,902	\$1,023,704	\$580,000	\$3,785,607	6	S	0.00011	\$416	N	0.002	Y	1	37	0.004061952	\$15,376.95	R
350064	\$5,860,892	\$377,160	\$580,000	\$6,818,053	6	S	0.00011	\$750	N	0.0005	Y	1	50	0.005485204	\$37,398.41	R
360028	\$714,051	\$10,433,974	\$1,160,000	\$12,308,025	6	S	0.00011	\$1,354	Y	0.0005	Y	1	21	0.002307461	\$28,400.28	R
360055	\$33,566,840	\$45,041,434	\$2,900,000	\$81,508,274	6	R	0.000077	\$6,276	Y	0.0005	Y	0.67	38	0.002921836	\$238,153.79	R
360800	\$342,744	\$1,062	\$0	\$343,806	6	S	0.00011	\$38	N	0.002	Y	1	35	0.003842809	\$1,321.18	R
364009	\$2,011,423	\$13,342,326	\$2,900,000	\$18,253,749	7	S	0.00011	\$2,008	N	0.002	Y	1	15	0.00164873	\$30,095.51	R
364010	\$1,349,556	\$1,300,359	\$1,160,000	\$3,809,915	6	S	0.00011	\$419	N	0.002	Y	1	27	0.002965757	\$11,299.28	R
364040	\$34,109,643	\$12,567,676	\$1,160,000	\$47,837,319	7	S	0.00011	\$5,262	N	0.002	Y	0.67	35	0.003842809	\$183,829.69	R
364056	\$760,874	\$15,334,106	\$1,160,000	\$17,254,980	7	S	0.00011	\$1,898	Y	0.002	Y	1	45	0.004938004	\$85,205.78	R
364057	\$1,159,572	\$1,263,417	\$1,160,000	\$3,582,989	7	S	0.00011	\$394	Y	0.002	Y	1	46	0.005047497	\$18,085.13	R
364110	\$7,711,039	\$893,997	\$1,160,000	\$9,765,036	6	S	0.00011	\$1,074	N	0.002	Y	1	15	0.00164873	\$16,099.91	R
364130	\$2,184,574	\$11,195,192	\$1,160,000	\$14,539,766	7	R	0.000077	\$1,120	N	0.002	Y	1	56	0.004302882	\$62,562.90	R
364140	\$15,306,348	\$5,916,334	\$2,900,000	\$24,122,682	7	R	0.000077	\$1,857	N	0.002	Y	1	53	0.004072841	\$98,247.84	R
365100	\$285,236	NA	\$580,000	\$865,236	6	S	0.00011	\$95	Y	0.002	Y	1	31	0.003404379	\$2,945.59	R
365102	\$285,683	NA	\$580,000	\$865,683	7	R	0.000077	\$67	Y	0.002	Y	1	57	0.004379551	\$3,791.30	R
380004	\$1,428,102	\$11,946,119	\$1,160,000	\$14,534,220	4	S	0.0005	\$7,267	Y	0.002	Y	1	16	0.00797007	\$115,838.75	R
380009	\$592,662	\$12,178,887	\$1,160,000	\$13,931,549	6	S	0.00011	\$1,532	N	0.002	Y	1	15	0.00164873	\$22,969.36	R
380011	\$439,621	\$3,349,194	\$1,160,000	\$4,948,815	6	S	0.00011	\$544	N	0.002	Y	1	15	0.00164873	\$8,159.26	R
380012	\$291,801	\$3,349,194	\$1,160,000	\$4,800,995	6	S	0.00011	\$528	N	0.002	Y	1	15	0.00164873	\$7,915.54	R
380013	\$585,522	\$2,870,738	\$1,160,000	\$4,616,259	6	S	0.00011	\$508	N	0.002	Y	1	15	0.00164873	\$7,610.97	R
380014	\$592,662	\$2,870,738	\$1,160,000	\$4,623,400	7	S	0.00011	\$509	N	0.002	Y	1	15	0.00164873	\$7,622.74	R
380015	\$2,194,267	\$2,870,738	\$1,160,000	\$6,225,004	6	S	0.00011	\$685	N	0.002	Y	1	15	0.00164873	\$10,263.35	R
380018	\$320,738	\$609,761	\$1,160,000	\$2,090,499	6	S	0.00011	\$230	Y	0.002	Y	1	15	0.00164873	\$3,446.67	R
380025	\$1,543,286	\$451,921	\$1,160,000	\$3,155,208	6	S	0.00011	\$347	Y	0.002	Y	1	25	0.002746373	\$8,665.38	R
380035	\$209,455	\$3,285,843	\$1,160,000	\$4,655,298	5	O	0.00032	\$79	N	0.0001	N	1	15	0.004789263	\$22,295.45	R
380036	\$487,935	\$3,285,843	\$1,160,000	\$4,933,778	6	O	0.00017	\$839	N	0.0005	Y	1	15	0.002546968	\$12,566.17	R
380037	\$292,761	\$3,285,843	\$1,160,000	\$4,738,604	6	S	0.00011	\$521	N	0.0005	Y	1	15	0.00164873	\$7,812.68	R
380038	\$355,597	\$13,626,153	\$1,160,000	\$15,141,750	6	S	0.00011	\$1,666	N	0.0005	Y	1	15	0.00164873	\$24,964.66	R
380040	\$390,348	\$1,982,836	\$1,160,000	\$3,533,184	6	O	0.00017	\$601	N	0.0005	Y	1	15	0.002546968	\$8,998.91	R
380049	\$1,588,237	\$10,501,683	\$1,160,000	\$13,249,920	6	S	0.00011	\$1,457	Y	0.0005	Y	1	18	0.00197815	\$26,210.33	M
380058	\$213,045	\$304,881	\$1,160,000	\$1,677,925	7	S	0.00011	\$185	Y	0.0005	Y	1	15	0.00164873	\$2,765.45	R
380059	\$1,558,270	\$451,921	\$1,160,000	\$3,170,191	6	S	0.00011	\$349	Y	0.0005	Y	1	15	0.00164873	\$5,226.79	R
380060	\$1,946,409	\$546,314	\$1,160,000	\$3,652,723	7	S	0.00011	\$402	Y	0.002	Y	1	19	0.002087932	\$7,626.64	R
380087	\$5,334,903	\$1,103,335	\$580,000	\$7,018,238	6	S	0.00011	\$772	N	0.001	Y	1	48	0.005266374	\$36,960.67	T
380910	\$1,035,702	\$6,393,916	\$1,160,000	\$8,589,617	6	S	0.00011	\$945	N	0.001	Y	1	15	0.00164873	\$14,161.96	R
384006	\$209,549	\$32,965	\$0	\$242,514	5	S	0.00024	\$1	N	0.001	Y	1	50	0.01192971	\$2,893.12	R
384008	\$69,798	\$12,023	\$0	\$81,820	5	S	0.00024	\$0	N	0.002	Y	1	21	0.005027922	\$411.38	R
384029	\$77,851	NA	\$0	\$77,851	4	O	0.0006	\$47	Y	0.002	Y	1	41	0.024307089	\$1,892.33	R
384094	\$175,134	NA	\$0	\$175,134	6	S	0.00011	\$19	Y	0.0005	Y	1	53	0.005813357	\$1,018.12	T
384096	\$67,300	\$15,901	\$0	\$83,201	4	S	0.0005	\$42	N	0.001	Y	1	55	0.027132008	\$2,257.41	T
384097	\$64,382	\$32,965	\$0	\$97,347	6	S	0.00011	\$11	N	0.0005	Y	1	60	0.006578628	\$640.41	R
384101	\$100,669	\$15,901	\$0	\$116,570	7	O	0.00017	\$20	N	0.001	Y	1	60	0.010149015	\$1,183.07	T
385080	\$104,727	\$105,900	\$580,000	\$790,628	4	S	0.0005	\$395	N	0.0005	N	1	16	0.00797007	\$6,301.36	R
390007	\$2,289,598	\$2,877,976	\$1,160,000	\$6,327,574	4	S	0.0005	\$3,164	N	0.002	Y	1	21	0.010447666	\$66,108.38	R
390023	\$490,125	\$378,708	\$580,000	\$1,448,832	6	S	0.00011	\$159	N	0.002	Y	1	26	0.002856071	\$4,137.97	R
394003	\$190,518	\$84,791	\$580,000	\$855,309	6	S	0.00011	\$94	N	0.002	Y	1	53	0.005813357	\$4,972.22	R
394004	\$143,805	\$179,690	\$1,160,000	\$1,483,495	6	S	0.00011	\$163	N	0.002	Y	1	53	0.005813357	\$8,624.09	R
460003	\$1,039,190	\$1,296,593	\$1,160,000	\$3,495,783	4	S	0.0005	\$1,748	N	0.002	Y	1	22	0.010942442	\$38,252.40	T
460007	\$558,481	\$1,172,120	\$1,160,000	\$2,890,601	7	S	0.00011	\$318	N	0.002	Y	1	24	0.002636663	\$7,621.54	R
460015	\$527,508	\$1,154,577	\$2,900,000	\$4,582,085	7	S	0.00011	\$504	N	0.002	Y	1	38	0.004171505	\$19,114.19	R
460020	\$952,216	\$690,853	\$1,160,000	\$2,803,069	6	S	0.00011	\$308	N	0.002	Y	1	21	0.002307461	\$6,467.97	M
460027	\$1,304,138	\$630,493	\$1,160,000	\$3,094,631	6	S	0.00011	\$340	N	0.002	Y	1	24	0.002636663	\$8,159.50	R
460032	\$839,519	\$762,296	\$580,000	\$2,181,815	7	S	0.00011	\$240	N	0.0005	Y	1	32	0.003514005	\$7,666.91	R
460053	\$1,944,453	\$1,653,716	\$2,900,000	\$16,498,169	6	S	0.00011	\$1,815	N	0.0005	Y	1	17	0.001868355	\$30,824.44	T
460055	\$1,647,608	\$17,780,481	\$2,900,000	\$22,328,089	6	S	0.00011	\$2,456	N	0.0005	Y	1	18	0.00197815	\$44,168.30	T
460801	\$65,427	\$0	\$0	\$65,427	7	N	NA	NA	N	0.0005	N	1	62	NA	NA	T
464006	\$10,789,075	\$1,055,486	\$1,160,000	\$13,004,561	7	S	0.00011	\$1,431	N	0.0005	Y	1	23	0.002526941	\$32,861.76	M
464007	\$432,364	\$31,026	\$0	\$463,390	7	S	0.00011	\$51	N	0.001	Y	1	53	0.005813357	\$2,693.85	T
464104	\$201,651	\$136,006	\$1,160,000	\$1,497,657	7	S	0.00011	\$165	N	0.001	Y	1	41	0.004500092	\$6,739.59	T
464109	\$328,276	\$2,382,206	\$1,160,000	\$3,870,482	7	S	0.00011	\$426	N	0.0001	N	1	22	0.002417207	\$9,355.76	T
464129	\$123,379	NA	\$0	\$123,379	7	S	0.00011	\$14	N	0.001	Y	1	70	0.007670851	\$946.42	T
464130	\$49,710	\$27,148	\$0	\$76,858	8	S	0.0000022	\$0	N	0.0001	Y	1	70	0.000153988	\$11.84	R
464201	\$691,264	\$272,530	\$1,160,000	\$2,123,794	6	S	0.00011	\$234	N	0.0001	N	1	32	0.003514005	\$7,463.02	T
464405	\$54,299	\$46,539	\$0	\$100,839	7	S	0.00011	\$11	N	0.0001	N	1	18	0.00197815	\$199.47	R
464408	\$277,836	\$139,650	\$1,160,000	\$1,577,486	6	S	0.00011	\$174	N	0.0005	Y	1	46	0.005047497	\$7,962.36	R
464414	\$95,800	\$334,505	\$580,000	\$1,010,305	6	S	0.00011	\$111	N	0.002	Y	1	38	0.004171505	\$4,214.49	R
464417	\$458,706	\$54,158	\$580,000	\$1,092,864	6	S	0.00011	\$120	N	0.002	Y	1	40	0.004390575	\$4,798.30	R
464418	\$103,682	\$51,711	\$0	\$155,392	6	S	0.00011	\$17	N	0.0001						



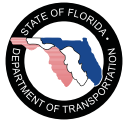
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
464503	\$609,323	\$167,580	\$1,160,000	\$1,936,903	6	S	0.00011	\$213	N	0.002	Y	1	15	0.00164873	\$3,193.43	R
464504	\$329,119	\$349,363	\$1,160,000	\$1,838,482	6	S	0.00011	\$202	N	0.002	Y	1	25	0.002746373	\$5,049.16	M
464505	\$129,602	\$154,226	\$1,160,000	\$1,443,829	7	S	0.00011	\$159	N	0.002	Y	1	46	0.005047497	\$7,287.72	T
464506	\$435,220	\$84,030	\$0	\$519,249	7	S	0.00011	\$57	N	0.002	Y	1	20	0.002197703	\$1,141.15	R
464507	\$78,382	\$32,965	\$0	\$111,347	7	S	0.00011	\$12	N	0.002	Y	1	39	0.004281046	\$476.68	M
465001	\$3,716,811	\$581,743	\$1,160,000	\$5,458,554	6	S	0.00011	\$600	N	0.002	Y	1	15	0.00164873	\$8,999.68	T
465401	\$103,682	\$36,844	\$0	\$140,525	4	S	0.0005	\$70	N	0.002	Y	1	40	0.019806229	\$2,783.27	R
466001	\$283,485	\$31,858	\$580,000	\$895,343	6	S	0.00011	\$98	N	0.0001	N	1	48	0.005266374	\$4,715.21	T
470014	\$1,883,268	\$20,479,060	\$1,160,000	\$23,522,329	4	S	0.0005	\$11,761	Y	0.0005	N	1	15	0.007473807	\$175,801.34	R
470022	\$2,090,882	\$5,129,003	\$1,160,000	\$8,379,885	4	S	0.0005	\$4,190	Y	0.0005	N	1	15	0.007473807	\$62,629.64	R
470023	\$1,870,813	\$4,968,722	\$1,160,000	\$7,999,535	4	S	0.0005	\$4,000	Y	0.0005	N	1	15	0.007473807	\$59,786.98	R
470029	\$58,576,385	\$813,254	\$1,160,000	\$60,549,639	7	S	0.00011	\$6,660	Y	0.002	Y	0.67	15	0.00164873	\$99,830.01	R
470035	\$918,649	\$648,255	\$580,000	\$2,146,904	7	S	0.00011	\$236	N	0.002	Y	1	20	0.002197703	\$4,718.26	R
470045	\$1,622,324	\$4,213,915	\$1,160,000	\$6,996,239	7	R	0.000077	\$539	N	0.0005	Y	1	44	0.00382397	\$23,664.06	R
474057	\$901,686	\$759,792	\$580,000	\$2,241,479	8	S	0.000022	\$5	N	0.001	Y	0.67	63	0.000138591	\$310.65	R
475047	\$129,553	\$93,079	\$580,000	\$802,632	7	S	0.00011	\$88	N	0.0001	N	1	31	0.003404379	\$2,732.46	R
480003	\$851,179	\$2,517,551	\$2,900,000	\$6,269,730	7	S	0.00011	\$690	Y	0.0001	N	1	15	0.00164873	\$10,337.09	R
480009	\$2,373,927	\$851,750	\$1,160,000	\$4,385,676	7	S	0.00011	\$482	Y	0.0001	N	1	26	0.002856071	\$12,525.80	R
480017	\$477,969	\$8,395,690	\$1,160,000	\$10,033,659	4	S	0.0005	\$5,017	Y	0.0005	N	1	15	0.007473807	\$74,989.63	R
480018	\$282,249	\$8,395,690	\$1,160,000	\$9,837,939	6	S	0.00011	\$1,082	Y	0.0005	Y	1	15	0.00164873	\$16,220.11	R
480025	\$214,159	\$424,768	\$580,000	\$1,218,927	7	S	0.00011	\$134	N	0.0005	Y	1	31	0.003404379	\$4,149.69	R
480026	\$186,398	\$750,568	\$580,000	\$1,516,966	6	S	0.00011	\$167	N	0.0001	N	1	34	0.00373322	\$5,663.17	R
480027	\$302,731	\$364,026	\$580,000	\$1,246,757	6	S	0.00011	\$137	N	0.0001	N	1	31	0.003404379	\$4,244.43	R
480030	\$124,265	\$191,146	\$580,000	\$895,411	7	S	0.00011	\$98	N	0.0005	Y	1	34	0.00373322	\$3,342.77	R
480032	\$1,660,406	\$1,770,351	\$2,900,000	\$6,330,757	4	S	0.0005	\$3,165	Y	0.0001	N	1	15	0.007473807	\$47,314.85	T
480033	\$1,660,406	\$1,770,351	\$2,900,000	\$6,330,757	4	S	0.0005	\$3,165	Y	0.002	Y	1	15	0.007473807	\$47,314.85	T
480039	\$1,333,004	\$1,407,315	\$1,160,000	\$3,900,319	6	S	0.00011	\$429	N	0.002	Y	1	15	0.00164873	\$6,430.57	R
480040	\$594,605	\$1,407,315	\$1,160,000	\$3,161,921	7	S	0.00011	\$348	N	0.002	Y	1	15	0.00164873	\$5,213.15	R
480041	\$183,874	\$343,234	\$1,160,000	\$1,687,108	7	S	0.00011	\$186	N	0.0001	N	1	29	0.003185092	\$5,373.59	R
480088	\$468,441	\$322,824	\$580,000	\$1,371,265	7	S	0.00011	\$151	N	0.0005	Y	1	15	0.00164873	\$2,260.85	R
480096	\$6,068,387	\$1,130,251	\$2,900,000	\$10,098,638	6	S	0.00011	\$1,111	N	0.001	Y	1	20	0.002197703	\$22,193.80	M
480099	\$124,265	\$159,288	\$580,000	\$863,553	7	S	0.00011	\$95	N	0.0005	Y	1	34	0.00373322	\$3,223.83	R
480103	\$614,664	\$631,986	\$580,000	\$1,826,650	6	S	0.00011	\$201	N	0.001	Y	1	34	0.00373322	\$6,819.29	R
480105	\$489,129	\$146,014	\$580,000	\$1,215,143	5	S	0.00024	\$4	N	0.0005	Y	1	35	0.008365818	\$10,165.67	R
480106	\$423,030	\$143,132	\$580,000	\$1,146,162	6	S	0.00011	\$126	N	0.0001	N	1	35	0.003842809	\$4,404.48	R
480107	\$802,144	\$175,914	\$580,000	\$1,558,058	6	S	0.00011	\$171	N	0.002	Y	1	24	0.002636663	\$4,108.07	R
480108	\$741,091	\$1,289,646	\$1,160,000	\$3,190,737	7	S	0.00011	\$351	N	0.0005	Y	1	26	0.002856071	\$9,112.97	R
480110	\$6,592,914	\$4,061,847	\$1,160,000	\$11,814,761	7	S	0.00011	\$1,300	N	0.001	Y	1	26	0.002856071	\$33,743.80	R
480114	\$245,886	\$254,861	\$580,000	\$1,080,747	6	S	0.00011	\$119	N	0.0005	Y	1	25	0.002746373	\$2,968.13	R
480115	\$127,218	\$258,896	\$580,000	\$966,114	6	S	0.00011	\$106	N	0.0005	Y	1	24	0.002636663	\$2,547.32	R
480117	\$305,375	\$127,430	\$580,000	\$1,012,805	6	S	0.00011	\$111	N	0.001	Y	1	36	0.003952386	\$4,003.00	R
480120	\$560,773	\$495,782	\$580,000	\$1,636,555	7	S	0.00011	\$180	N	0.0005	Y	1	15	0.00164873	\$2,698.24	R
480131	\$608,602	\$605,149	\$1,160,000	\$2,373,751	7	S	0.00011	\$261	N	0.001	Y	1	15	0.00164873	\$3,913.67	R
484000	\$124,265	\$89,387	\$580,000	\$793,652	7	S	0.00011	\$87	N	0.001	Y	1	31	0.003404379	\$2,701.89	R
484002	\$112,968	\$153,063	\$0	\$266,031	6	S	0.00011	\$29	N	0.002	Y	1	34	0.00373322	\$993.15	R
484003	\$117,775	\$82,737	\$0	\$200,512	6	S	0.00011	\$22	N	0.002	Y	1	30	0.003294742	\$660.64	R
484004	\$432,542	\$170,544	\$580,000	\$1,183,086	6	S	0.00011	\$130	N	0.0001	N	1	33	0.003623618	\$4,287.05	R
484006	\$113,218	\$25,855	\$0	\$139,073	7	S	0.00011	\$15	N	0.0005	Y	1	34	0.00373322	\$519.19	R
484007	\$225,219	\$103,421	\$0	\$328,640	3	S	0.0013	\$427	N	0.0005	N	1	33	0.042019551	\$13,809.31	R
484008	\$109,363	\$103,421	\$0	\$212,784	6	S	0.00011	\$23	N	0.0005	Y	1	32	0.003514005	\$747.72	R
484009	\$167,049	\$32,319	\$0	\$199,368	7	S	0.00011	\$22	N	0.0005	Y	1	31	0.003404379	\$678.72	R
484011	\$224,735	\$51,711	\$0	\$276,445	6	S	0.00011	\$30	N	0.0005	Y	1	31	0.003404379	\$941.12	R
484014	\$169,452	\$134,447	\$0	\$303,900	7	S	0.00011	\$33	N	0.0005	Y	1	31	0.003404379	\$1,034.59	R
484015	\$278,784	\$31,026	\$0	\$309,811	6	S	0.00011	\$34	N	0.0001	N	1	31	0.003404379	\$1,054.71	R
484016	\$309,341	\$82,737	\$580,000	\$972,078	7	S	0.00011	\$107	N	0.0001	N	1	32	0.003514005	\$3,415.89	R
484017	\$224,735	\$51,711	\$0	\$276,445	6	S	0.00011	\$30	N	0.0005	Y	1	31	0.003404379	\$941.12	R
484018	\$116,870	\$148,926	\$0	\$265,797	7	S	0.00011	\$29	N	0.0005	Y	1	34	0.00373322	\$992.28	R
484020	\$164,879	\$165,474	\$0	\$330,353	6	S	0.00011	\$36	N	0.0005	Y	1	34	0.00373322	\$1,233.28	R
484023	\$144,215	\$745,129	\$1,160,000	\$2,049,343	7	S	0.00011	\$225	N	0.0005	Y	1	34	0.00373322	\$7,650.65	R
484024	\$167,650	\$490,334	\$1,160,000	\$1,817,984	6	S	0.00011	\$200	N	0.0005	Y	1	33	0.003623618	\$6,587.68	R
484028	\$221,129	\$106,653	\$0	\$327,782	2	S	0.006	\$1,967	N	0.0001	N	1	35	0.189928312	\$62,255.08	R
484029	\$276,412	\$58,821	\$0	\$335,233	4	S	0.0005	\$168	N	0.0001	N	1	34	0.016860495	\$5,652.19	R
484030	\$204,905	\$381,371	\$580,000	\$1,166,276	5	S	0.00024	\$4	N	0.0001	N	1	35	0.008365818	\$9,756.85	R
484032	\$174,088	\$89,976	\$0	\$264,064	6	S	0.00011	\$29	N	0.0001	N	1	33	0.003623618	\$956.87	R
484034	\$228,871	\$45,247	\$0	\$274,118	6	O	0.00017	\$47	N	0.0005	Y	1	31	0.005256584	\$1,440.92	R
484036	\$125,587	\$65,378	\$580,000	\$770,965	3	S	0.0013	\$1,002	N	0.0005	N	1	34	0.043264925	\$33,355.74	R
484037	\$114,170	\$29,087	\$0	\$143,257	4	S	0.0005	\$72	N	0.002	Y	1	33	0.016368679	\$2,344.93	R
484038	\$117,775	\$72,395	\$0	\$190,170	7	S	0.00011	\$21	N	0.002	Y	1	31	0.003404379	\$647.41	R
484039	\$309,341	\$99,284	\$580,000	\$988,625	6	S	0.00011	\$109	N	0.002	Y	1	31	0.003404379	\$3,365.65	R
484040	\$118,088	\$64,638	\$0	\$182,726	6	S	0.00011	\$20	N	0.002	Y	1	32	0.003514005	\$642.10	R
484041	\$165,847	\$19,391	\$0	\$185,239	6	S	0.00011	\$20	N	0.002	Y	1	32	0.003514005	\$650.93	R
484042	\$111,767	\$127,208	\$0	\$238,974	6	S	0.00011	\$26	N	0.002	Y	1	32	0.003514005	\$839.76	R
484043	\$353,045	\$678,596	\$1,160,000	\$2,191,641	6	S	0.00011	\$241	N	0.002	Y	1	33	0.003623618	\$7,941.67	R
484045	\$490,451	\$944,147	\$580,000	\$2,014,598	4	S	0.0005	\$1,007	N	0.002	Y	1	26	0.012919074		



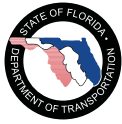
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
484051	\$168,001	\$78,859	\$0	\$246,859	6	S	0.00011	\$27	N	0.0005	Y	1	25	0.002746373	\$677.97	R
484052	\$66,770	\$64,638	\$0	\$131,408	6	S	0.00011	\$14	N	0.0005	Y	1	22	0.002417207	\$317.64	R
484053	\$113,218	\$95,147	\$0	\$208,365	4	S	0.0005	\$104	N	0.0005	N	1	26	0.012919074	\$2,691.88	R
484054	\$286,026	\$41,239	\$0	\$327,265	7	O	0.00017	\$56	N	0.0005	Y	1	25	0.004241341	\$1,388.04	R
484060	\$138,479	\$232,750	\$1,160,000	\$1,531,229	6	S	0.00011	\$168	N	0.0005	Y	1	24	0.002636663	\$4,037.33	R
484064	\$128,557	\$31,647	\$580,000	\$740,204	7	S	0.00011	\$81	N	0.002	Y	1	27	0.002965757	\$2,195.27	R
484067	\$149,693	\$19,391	\$0	\$169,085	6	S	0.00011	\$19	N	0.0005	Y	1	28	0.003075431	\$520.01	R
484068	\$99,749	\$95,573	\$580,000	\$775,321	4	S	0.0005	\$388	N	0.002	Y	1	15	0.007473807	\$5,794.60	T
484069	\$903,310	\$6,614,863	\$2,900,000	\$10,418,173	7	S	0.00011	\$1,146	N	0.002	Y	1	28	0.003075431	\$32,040.37	R
484071	\$318,584	\$395,807	\$1,160,000	\$1,874,391	7	S	0.00011	\$206	N	0.002	Y	1	36	0.003952386	\$7,408.32	R
484072	\$175,305	\$1,445,725	\$1,160,000	\$2,781,030	7	S	0.00011	\$306	N	0.002	Y	1	26	0.002856071	\$7,942.82	R
484073	\$169,452	\$837,319	\$1,160,000	\$2,166,772	3	S	0.0013	\$2,817	N	0.0005	N	1	24	0.030737977	\$66,602.19	R
484075	\$335,300	\$41,368	\$0	\$376,668	3	S	0.0013	\$490	N	0.002	Y	1	24	0.030737977	\$11,578.01	R
484078	\$282,421	\$512,049	\$1,160,000	\$1,954,470	7	S	0.00011	\$215	N	0.002	Y	1	26	0.002856071	\$5,582.11	M
484083	\$195,171	\$88,115	\$580,000	\$863,286	7	S	0.00011	\$95	N	0.002	Y	1	42	0.004609597	\$3,979.40	R
484084	\$145,382	\$84,392	\$580,000	\$809,774	6	O	0.00017	\$138	N	0.002	Y	1	42	0.007115713	\$5,761.68	R
485005	\$2,266,046	\$6,614,863	\$2,900,000	\$11,780,910	7	S	0.00011	\$1,296	N	0.0005	Y	1	22	0.002417207	\$28,476.90	M
490018	\$757,850	\$4,100,301	\$1,160,000	\$6,018,151	7	S	0.00011	\$662	Y	0.002	Y	1	15	0.00164873	\$9,922.31	R
490025	\$2,205,208	\$3,807,422	\$1,160,000	\$7,172,630	7	S	0.00011	\$789	Y	0.0005	Y	1	43	0.00471909	\$33,848.29	R
490030	\$608,371	\$517,387	\$1,160,000	\$2,285,759	7	S	0.00011	\$251	Y	0.002	Y	1	52	0.005703985	\$13,037.93	T
490806	\$196,001	\$40,314	\$0	\$236,315	8	O	0.0000085	\$2	N	0.002	Y	1	63	0.000535359	\$126.51	R
490807	\$87,590	\$36,649	\$0	\$124,239	7	O	0.00017	\$21	N	0.002	Y	1	63	0.010653753	\$1,323.61	R
490808	\$85,436	\$10,995	\$0	\$96,431	7	O	0.00017	\$16	N	0.002	Y	1	63	0.010653753	\$1,027.35	R
490811	\$66,052	\$36,649	\$0	\$102,700	8	O	0.0000085	\$1	N	0.002	Y	1	63	0.000535359	\$54.98	R
490825	\$97,111	\$58,638	\$0	\$155,749	7	O	0.00017	\$26	N	0.002	Y	1	67	0.011326337	\$1,764.07	M
490826	\$400,181	\$69,633	\$0	\$469,813	7	O	0.00017	\$80	N	0.002	Y	1	67	0.011326337	\$5,321.26	M
490827	\$266,579	\$69,633	\$0	\$336,212	7	O	0.00017	\$57	N	0.002	Y	1	67	0.011326337	\$3,808.05	R
490828	\$87,590	\$40,314	\$0	\$127,904	7	O	0.00017	\$22	N	0.002	Y	1	67	0.011326337	\$1,448.68	R
490829	\$43,795	\$10,995	\$0	\$54,790	7	O	0.00017	\$9	N	0.002	Y	1	67	0.011326337	\$620.57	M
490830	\$43,795	\$10,995	\$0	\$54,790	7	O	0.00017	\$9	N	0.002	Y	1	67	0.011326337	\$620.57	M
490831	\$43,795	\$18,324	\$0	\$62,120	8	O	0.0000085	\$1	N	0.002	Y	1	67	0.00056934	\$35.37	M
490832	\$76,165	\$10,995	\$0	\$87,160	7	O	0.00017	\$15	N	0.002	Y	1	67	0.011326337	\$987.20	M
490833	\$43,795	\$21,989	\$0	\$65,784	7	O	0.00017	\$11	N	0.002	Y	1	67	0.011326337	\$745.09	M
490834	\$56,812	\$47,643	\$0	\$104,455	7	O	0.00017	\$18	N	0.002	Y	1	67	0.011326337	\$1,183.09	M
490835	\$43,795	\$47,643	\$0	\$91,439	7	O	0.00017	\$16	N	0.001	N	1	67	0.011326337	\$1,035.67	M
490836	\$109,847	\$10,995	\$0	\$120,841	7	O	0.00017	\$21	N	0.0005	Y	1	67	0.011326337	\$1,368.69	M
490837	\$87,590	\$10,995	\$0	\$98,585	7	O	0.00017	\$17	N	0.0005	Y	1	67	0.011326337	\$1,116.61	R
490838	\$43,795	\$36,649	\$0	\$80,444	7	O	0.00017	\$14	N	0.001	N	1	67	0.011326337	\$911.14	R
490839	\$65,334	\$10,995	\$0	\$76,328	7	O	0.00017	\$13	N	0.001	Y	1	67	0.011326337	\$864.52	R
490840	\$56,812	\$36,649	\$0	\$93,461	7	O	0.00017	\$16	N	0.0005	Y	1	67	0.011326337	\$1,058.57	R
490841	\$56,812	\$18,324	\$0	\$75,136	7	O	0.00017	\$13	N	0.001	Y	1	67	0.011326337	\$851.02	R
490842	\$56,812	\$51,308	\$0	\$108,120	7	O	0.00017	\$18	N	0.002	Y	1	67	0.011326337	\$1,224.60	R
490843	\$65,334	\$40,314	\$0	\$105,647	7	O	0.00017	\$18	N	0.0001	N	1	67	0.011326337	\$1,196.59	R
494000	\$593,805	\$2,615,115	\$580,000	\$3,788,920	7	S	0.00011	\$417	N	0.0001	N	1	55	0.006032066	\$22,855.02	M
494096	\$158,808	\$19,391	\$0	\$178,199	5	S	0.00024	\$1	N	0.0005	Y	1	25	0.005982752	\$1,066.12	M
494099	\$58,232	\$89,201	\$0	\$147,433	6	S	0.00011	\$16	N	0.0005	Y	1	65	0.00712489	\$1,050.44	M
500004	\$2,025,688	\$17,456,582	\$2,900,000	\$22,382,271	8	S	0.0000022	\$49	N	0.0005	Y	1	37	8.13968E-05	\$1,821.84	R
500041	\$1,442,383	\$527,757	\$1,160,000	\$3,130,140	6	S	0.00011	\$344	N	0.0005	Y	1	22	0.002417207	\$7,566.20	R
500045	\$2,782,972	\$5,152,735	\$1,160,000	\$9,095,707	5	S	0.00024	\$31	N	0.0005	Y	1	25	0.005982752	\$54,417.36	R
500048	\$888,022	\$2,781,921	\$1,160,000	\$4,829,943	4	S	0.0005	\$2,415	Y	0.0005	N	1	15	0.007473807	\$36,098.06	R
500049	\$464,133	\$974,112	\$1,160,000	\$2,598,245	4	S	0.0005	\$1,299	N	0.0001	N	1	33	0.016368679	\$42,529.84	R
500063	\$3,561,514	\$997,519	\$2,900,000	\$7,459,033	4	O	0.0006	\$4,475	N	0.0001	N	1	15	0.008962298	\$66,850.08	R
500106	\$1,162,869	\$658,032	\$1,160,000	\$2,980,901	7	S	0.00011	\$328	N	0.0005	Y	1	45	0.00493804	\$14,719.81	R
500803	\$72,357	NA	\$0	\$72,357	8	O	0.0000085	\$1	N	0.0005	Y	1	69	0.000586331	\$42.43	R
500804	\$72,357	NA	\$0	\$72,357	8	O	0.0000085	\$1	N	0.0005	Y	1	69	0.000586331	\$42.43	R
500910	\$412,558	\$715,993	\$1,160,000	\$2,288,550	6	S	0.00011	\$252	N	0.001	Y	1	15	0.00164873	\$3,773.20	R
500920	\$6,185,132	\$1,684,725	\$2,900,000	\$10,769,858	8	S	0.0000022	\$24	N	0.0005	Y	1	37	8.13968E-05	\$876.63	R
504024	\$93,693	\$45,764	\$0	\$139,457	7	S	0.00011	\$15	N	0.0005	Y	1	26	0.002856071	\$398.30	R
504130	\$387,268	\$148,669	\$580,000	\$1,115,937	7	S	0.00011	\$123	N	0.0005	Y	1	61	0.006687905	\$7,463.28	R
504131	\$463,719	\$178,403	\$580,000	\$1,222,122	7	S	0.00011	\$134	N	0.001	Y	1	61	0.006687905	\$8,173.44	R
504135	\$583,143	\$108,963	\$580,000	\$1,272,106	6	S	0.00011	\$140	N	0.001	Y	1	62	0.006797169	\$8,646.72	R
504136	\$513,165	\$431,685	\$580,000	\$1,524,849	7	S	0.00011	\$168	N	0.001	Y	1	62	0.006797169	\$10,364.66	R
504137	\$571,288	\$338,575	\$1,160,000	\$2,069,862	7	S	0.00011	\$228	N	0.001	Y	1	63	0.006906421	\$14,295.34	R
510019	\$460,028	\$55,751	\$580,000	\$1,095,779	6	S	0.00011	\$121	N	0.0005	Y	1	32	0.003514005	\$3,850.57	M
510020	\$271,399	\$4,136,841	\$580,000	\$4,988,240	7	S	0.00011	\$549	N	0.001	Y	1	46	0.005047497	\$25,178.12	T
510022	\$1,318,864	\$17,774,402	\$1,160,000	\$20,253,266	7	S	0.00011	\$2,228	Y	0.001	Y	1	15	0.00164873	\$33,392.17	R
510024	\$377,019	\$7,039,252	\$1,160,000	\$8,576,271	7	S	0.00011	\$943	N	0.001	Y	1	15	0.00164873	\$14,139.96	R
510026	\$471,789	\$7,039,252	\$1,160,000	\$8,671,041	7	S	0.00011	\$954	N	0.001	Y	1	15	0.00164873	\$14,296.21	M
510046	\$510,558	\$318,576	\$0	\$829,134	7	S	0.00011	\$91	N	0.001	Y	1	41	0.004500092	\$3,731.18	T
514008	\$163,662	\$16,160	\$0	\$179,822	6	S	0.00011	\$20	N	0.002	Y	1	26	0.002856071	\$513.58	R
514013	\$480,064	\$637,152	\$580,000	\$1,697,216	7	S	0.00011	\$187	N	0.002	Y	1	16	0.001758549	\$2,984.64	M
514017	\$193,457	\$144,789	\$0	\$338,247	5	S	0.00024	\$1	N	0.002	Y	1	55	0.013114826	\$4,436.05	T
514019	\$331,156	\$575,778	\$1,160,000	\$2,066,934	7	S	0.00011	\$227	N	0.002	Y	1	59	0.00646934	\$13,371.70	R
514055	\$206,770	\$19,391	\$0	\$226,162	7	S	0.00011	\$25	N	0.002	Y	1	59	0.00646934	\$1,463.12	R
514056	\$228,403	\$31,026	\$0	\$259,429	7	S	0.00011	\$29	N	0.002	Y	1	59	0.00646934	\$1,678.33	R
514057	\$121,490															



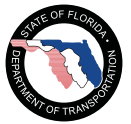
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
514064	\$121,490	NA	\$0	\$121,490	4	S	0.0005	\$61	N	0.002	Y	1	65	0.031985418	\$3,885.91	R
520006	\$653,499	\$548,853	\$580,000	\$1,782,352	6	S	0.00011	\$196	N	0.002	Y	1	22	0.002417207	\$4,308.31	R
520062	\$753,733	\$3,503,508	\$1,160,000	\$5,417,241	6	S	0.00011	\$596	N	0.002	Y	1	35	0.003842809	\$20,817.42	R
524000	\$95,597	\$31,026	\$0	\$126,623	6	S	0.00011	\$14	N	0.002	Y	1	50	0.005485204	\$694.55	R
524006	\$64,772	\$27,148	\$0	\$91,920	7	S	0.00011	\$10	N	0.002	Y	1	50	0.005485204	\$504.20	R
524007	\$68,065	\$46,539	\$0	\$114,605	6	S	0.00011	\$13	N	0.002	Y	1	50	0.005485204	\$628.63	R
524011	\$62,712	\$15,513	\$0	\$78,225	7	S	0.00011	\$9	N	0.002	Y	1	55	0.006032066	\$471.86	R
524013	\$51,006	\$19,391	\$0	\$70,397	6	S	0.00011	\$8	N	0.002	Y	1	45	0.00493804	\$347.62	R
524014	\$61,947	\$11,635	\$0	\$73,582	7	S	0.00011	\$8	N	0.002	Y	1	45	0.00493804	\$363.35	R
524015	\$63,211	\$46,539	\$0	\$109,751	7	S	0.00011	\$12	N	0.001	Y	1	51	0.0055946	\$614.01	R
524016	\$94,832	\$20,684	\$0	\$115,516	6	S	0.00011	\$13	N	0.002	Y	1	53	0.005813357	\$671.54	R
524020	\$75,213	\$19,391	\$0	\$94,605	6	S	0.00011	\$10	N	0.002	Y	1	47	0.005156941	\$487.87	R
524021	\$61,182	\$31,026	\$0	\$92,208	3	S	0.0013	\$120	N	0.002	Y	1	52	0.06540685	\$6,031.03	R
524022	\$335,300	\$136,204	\$580,000	\$1,051,503	7	S	0.00011	\$116	N	0.002	Y	1	57	0.006250727	\$6,572.66	R
524023	\$180,784	\$62,637	\$580,000	\$823,421	7	S	0.00011	\$91	N	0.002	Y	1	58	0.00636004	\$5,236.99	R
524100	\$57,046	\$19,391	\$0	\$76,437	7	S	0.00011	\$8	N	0.002	Y	1	60	0.006578628	\$502.85	R
524102	\$94,067	\$100,835	\$0	\$194,903	7	S	0.00011	\$21	N	0.002	Y	1	31	0.003404379	\$663.52	R
524103	\$94,067	\$42,661	\$0	\$136,729	6	O	0.00017	\$23	N	0.002	Y	1	36	0.006101828	\$834.30	R
524105	\$157,544	\$7,757	\$0	\$165,300	3	S	0.0013	\$215	N	0.002	Y	1	44	0.055629973	\$9,195.63	R
524107	\$93,303	\$92,433	\$0	\$185,735	6	S	0.00011	\$20	N	0.002	Y	1	31	0.003404379	\$632.31	R
524112	\$105,352	\$19,391	\$0	\$124,743	6	S	0.00011	\$14	N	0.002	Y	1	47	0.005156941	\$643.29	R
524113	\$64,241	\$32,319	\$0	\$96,560	6	O	0.00017	\$16	N	0.002	Y	1	37	0.006270791	\$605.51	R
524115	\$308,205	\$54,296	\$0	\$362,501	6	S	0.00011	\$40	N	0.002	Y	1	37	0.004061952	\$1,472.46	R
524117	\$77,851	\$38,783	\$0	\$116,634	3	S	0.0013	\$152	N	0.002	Y	1	41	0.051937334	\$6,057.66	R
524118	\$162,897	\$109,238	\$0	\$272,136	6	S	0.00011	\$30	N	0.002	Y	1	42	0.004609597	\$1,254.44	R
524119	\$94,067	\$51,711	\$0	\$145,778	2	S	0.006	\$875	N	0.002	N	1	41	0.218656938	\$31,875.37	R
524122	\$47,447	\$31,026	\$0	\$78,474	6	S	0.00011	\$9	N	0.002	Y	1	38	0.004171505	\$327.35	R
524123	\$54,627	\$15,513	\$0	\$70,140	7	S	0.00011	\$8	N	0.002	Y	1	39	0.004281046	\$300.27	R
524124	\$48,321	\$23,270	\$0	\$71,591	7	S	0.00011	\$8	N	0.002	Y	1	41	0.004500092	\$322.17	R
524125	\$64,241	\$41,368	\$0	\$105,610	6	S	0.00011	\$12	N	0.002	Y	1	43	0.00471909	\$498.38	R
524126	\$98,656	\$7,757	\$0	\$106,413	6	S	0.00011	\$12	N	0.002	Y	1	36	0.003952386	\$420.59	R
524127	\$63,476	\$41,368	\$0	\$104,845	3	S	0.0013	\$136	N	0.002	Y	1	36	0.04575082	\$4,796.74	R
524128	\$64,553	\$77,566	\$0	\$142,119	4	O	0.0006	\$85	N	0.002	Y	1	43	0.02547757	\$3,620.85	R
524129	\$57,686	\$11,635	\$0	\$69,321	7	S	0.00011	\$8	N	0.002	Y	1	44	0.004828571	\$334.72	R
524130	\$55,704	\$46,539	\$0	\$102,243	3	S	0.0013	\$133	N	0.002	Y	1	44	0.055629973	\$5,687.78	R
524132	\$54,299	\$64,638	\$0	\$118,937	6	S	0.00011	\$13	N	0.002	Y	1	45	0.00493804	\$587.32	R
524134	\$53,534	\$19,391	\$0	\$72,926	4	S	0.0005	\$36	N	0.002	Y	1	60	0.029561747	\$2,155.82	R
524136	\$69,126	\$7,757	\$0	\$76,883	6	S	0.00011	\$8	N	0.002	Y	1	36	0.003952386	\$303.87	R
524137	\$63,476	\$5,817	\$0	\$69,294	7	S	0.00011	\$8	N	0.002	Y	1	60	0.006578628	\$455.86	R
524138	\$126,953	\$54,296	\$0	\$181,249	6	S	0.00011	\$20	N	0.002	Y	1	60	0.006578628	\$1,192.37	R
524139	\$61,947	\$32,319	\$0	\$94,266	7	S	0.00011	\$10	N	0.002	Y	1	60	0.006578628	\$620.14	R
524140	\$57,358	\$32,319	\$0	\$89,677	6	S	0.00011	\$10	N	0.002	Y	1	60	0.006578628	\$589.95	R
524150	\$127,203	\$19,391	\$0	\$146,594	6	S	0.00011	\$16	N	0.0005	Y	1	66	0.007234106	\$1,060.48	R
524153	\$60,417	\$38,783	\$0	\$99,200	7	S	0.00011	\$11	N	0.0005	Y	1	68	0.007452503	\$739.29	R
524155	\$400,454	\$187,642	\$580,000	\$1,168,096	7	S	0.00011	\$128	N	0.0005	Y	1	68	0.007452503	\$8,705.24	R
524156	\$63,211	\$63,992	\$0	\$127,203	7	S	0.00011	\$14	N	0.0001	N	1	68	0.007452503	\$947.98	R
524157	\$91,773	\$100,835	\$0	\$192,609	7	S	0.00011	\$21	N	0.002	Y	1	68	0.007452503	\$1,435.42	R
524158	\$92,148	\$22,623	\$0	\$114,771	7	S	0.00011	\$13	N	0.002	Y	1	68	0.007452503	\$855.33	R
524159	\$57,717	\$71,102	\$0	\$128,819	3	O	0.0016	\$206	N	0.002	Y	1	56	0.085768774	\$11,048.65	R
524160	\$61,182	\$32,319	\$0	\$93,501	7	S	0.00011	\$10	N	0.002	Y	1	69	0.007561683	\$707.02	R
524161	\$163,756	\$38,783	\$0	\$202,539	7	S	0.00011	\$22	N	0.002	Y	1	53	0.005813357	\$1,177.43	R
524162	\$54,923	NA	\$0	\$54,923	7	S	0.00011	\$6	N	0.002	Y	1	69	0.007561683	\$415.31	R
524163	\$54,362	\$19,391	\$0	\$73,753	7	S	0.00011	\$8	N	0.002	Y	1	61	0.006687905	\$493.25	R
524164	\$93,303	\$84,030	\$0	\$177,332	7	S	0.00011	\$20	N	0.002	Y	1	70	0.007670851	\$1,360.29	R
524166	\$261,428	\$36,649	\$0	\$298,077	8	S	0.0000022	\$1	N	0.002	Y	1	72	0.000158388	\$47.21	R
524201	\$51,006	\$64,638	\$0	\$115,644	6	S	0.00011	\$13	N	0.002	Y	1	36	0.003952386	\$457.07	R
524202	\$92,538	\$31,026	\$0	\$123,564	6	S	0.00011	\$14	N	0.002	Y	1	36	0.003952386	\$488.37	R
524203	\$120,070	\$41,368	\$0	\$161,438	6	S	0.00011	\$18	N	0.002	Y	1	36	0.003952386	\$638.07	R
524204	\$185,076	\$41,368	\$0	\$226,444	6	S	0.00011	\$25	N	0.002	Y	1	36	0.003952386	\$894.99	R
524206	\$78,522	\$25,855	\$0	\$104,377	7	S	0.00011	\$11	N	0.002	Y	1	47	0.005156941	\$538.27	R
524207	\$58,529	\$31,026	\$0	\$89,555	6	S	0.00011	\$10	N	0.002	Y	1	41	0.004500092	\$403.01	R
524208	\$77,851	\$17,452	\$0	\$95,303	6	S	0.00011	\$10	N	0.002	Y	1	37	0.004061952	\$387.12	R
524209	\$249,317	\$38,783	\$0	\$288,100	3	S	0.0013	\$375	N	0.002	Y	1	47	0.059308231	\$17,086.70	R
524210	\$127,983	\$25,855	\$0	\$153,838	3	O	0.0016	\$246	N	0.002	Y	1	36	0.056016063	\$8,617.40	R
524212	\$64,241	\$51,711	\$0	\$115,952	6	S	0.00011	\$13	N	0.002	Y	1	36	0.003952386	\$458.29	R
524213	\$63,476	\$51,711	\$0	\$115,187	3	S	0.0013	\$150	N	0.002	Y	1	41	0.051937334	\$5,982.51	R
524214	\$63,991	\$51,711	\$0	\$115,702	6	S	0.00011	\$13	N	0.002	Y	1	35	0.003842809	\$444.62	R
524216	\$120,835	\$41,368	\$0	\$162,203	3	S	0.0013	\$211	N	0.002	Y	1	36	0.04575082	\$7,420.92	R
524217	\$73,824	\$25,855	\$0	\$99,680	3	S	0.0013	\$130	N	0.002	Y	1	39	0.049467556	\$4,930.93	R
524302	\$62,712	\$67,224	\$0	\$129,935	7	S	0.00011	\$14	N	0.001	Y	1	41	0.004500092	\$584.72	R
524303	\$56,593	\$42,015	\$0	\$98,608	6	S	0.00011	\$11	N	0.002	Y	1	45	0.00493804	\$486.93	R
524309	\$1,084,702	\$209,209	\$580,000	\$1,873,911	6	S	0.00011	\$206	N	0.002	Y	1	46	0.005047497	\$9,458.56	R
524310	\$149,896	\$62,053	\$0	\$211,949	6	S	0.00011	\$23	N	0.0005	Y	1	41	0.004500092	\$953.79	R
524402	\$181,252	\$134,447	\$0	\$315,699	6	S	0.00011	\$35	N	0.0005	Y	1	44	0.004828571	\$1,524.38	R
524501	\$52,005	\$48,479	\$0	\$100,483	7	S	0.00011	\$11	N	0.001	Y	1	38	0.004171505	\$419.17	R
524505	\$79,193	\$38,783	\$0	\$117,976	6	S	0.00011	\$13	N	0.0005	Y	1	36	0.003952386	\$466.29	R
524506	\$63,991	\$54,942	\$0	\$118,934	6	S	0.00011	\$13	N	0.001	Y	1	47	0.005156941	\$613.34	R
524507	\$141,484	\$38,783	\$0	\$180,266	6	S	0.00011	\$20	N	0.0005	Y	1	37	0.004061952	\$732.23	R
525403	\$112,625	\$65,931	\$0	\$178,556	7	S	0.00011	\$20	N	0.0005	Y					



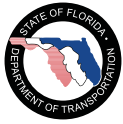
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
530005	\$8,606,818	\$18,658,076	\$2,900,000	\$30,164,894	7	S	0.00011	\$3,318	Y	0.002	Y	1	15	0.00164873	\$49,733.77	R
530014	\$1,803,819	\$787,520	\$580,000	\$3,171,339	7	S	0.00011	\$349	N	0.002	Y	1	40	0.004390575	\$13,924.00	R
530016	\$714,004	\$6,913,216	\$1,160,000	\$8,787,220	6	S	0.00011	\$967	N	0.001	Y	1	23	0.002526941	\$22,204.79	R
530026	\$1,627,310	\$802,170	\$580,000	\$3,009,480	5	S	0.00024	\$10	N	0.0005	Y	1	32	0.007651499	\$23,027.03	R
530041	\$1,584,887	\$239,670	\$580,000	\$2,404,557	7	S	0.00011	\$265	N	0.002	Y	1	34	0.00373322	\$8,976.74	R
530081	\$2,227,839	\$1,299,650	\$1,160,000	\$4,687,488	7	S	0.00011	\$516	Y	0.0005	Y	1	45	0.00493804	\$23,147.00	R
530910	\$795,429	\$1,294,200	\$2,900,000	\$4,989,630	7	S	0.00011	\$549	Y	0.0005	Y	1	28	0.003075431	\$15,345.26	R
534002	\$74,261	\$32,319	\$0	\$106,580	7	S	0.00011	\$12	N	0.0005	Y	1	57	0.006250727	\$666.20	R
534003	\$163,756	\$51,711	\$0	\$215,466	7	S	0.00011	\$24	N	0.001	Y	1	57	0.006250727	\$1,346.82	R
534005	\$140,906	\$27,148	\$0	\$168,054	7	S	0.00011	\$18	N	0.0005	Y	1	57	0.006250727	\$1,050.46	R
534009	\$69,501	\$19,391	\$0	\$88,892	7	S	0.00011	\$10	N	0.002	Y	1	57	0.006250727	\$556.64	R
534010	\$117,104	\$46,539	\$0	\$163,644	7	S	0.00011	\$18	N	0.002	Y	1	57	0.006250727	\$1,022.89	R
534011	\$71,405	\$25,855	\$0	\$97,260	7	S	0.00011	\$11	N	0.0005	Y	1	57	0.006250727	\$607.95	R
534012	\$139,954	\$31,026	\$0	\$170,980	7	S	0.00011	\$19	N	0.001	Y	1	57	0.006250727	\$1,068.75	R
534013	\$277,848	\$25,855	\$0	\$303,703	6	S	0.00011	\$33	N	0.001	Y	1	57	0.006250727	\$1,898.36	R
534014	\$277,848	\$31,026	\$0	\$308,874	6	S	0.00011	\$34	N	0.0005	Y	1	57	0.006250727	\$1,930.69	R
534015	\$237,580	\$82,737	\$0	\$320,317	7	S	0.00011	\$35	N	0.002	Y	1	57	0.006250727	\$2,002.21	R
534016	\$134,242	\$31,026	\$0	\$165,268	7	S	0.00011	\$18	N	0.002	Y	1	57	0.006250727	\$1,033.05	R
534017	\$70,453	\$25,855	\$0	\$96,308	7	S	0.00011	\$11	N	0.0005	Y	1	57	0.006250727	\$602.00	R
534018	\$293,955	\$45,247	\$0	\$339,202	6	S	0.00011	\$37	N	0.001	Y	1	57	0.006250727	\$2,120.26	R
534020	\$303,694	\$23,270	\$0	\$326,964	7	S	0.00011	\$36	N	0.002	Y	1	58	0.00636004	\$2,079.50	R
534021	\$209,455	\$25,855	\$0	\$235,310	7	S	0.00011	\$26	N	0.002	Y	1	58	0.00636004	\$1,496.58	R
534022	\$655,023	\$32,319	\$0	\$687,342	6	S	0.00011	\$76	N	0.002	Y	1	58	0.00636004	\$4,371.52	R
534024	\$112,250	\$22,623	\$0	\$134,874	7	S	0.00011	\$15	N	0.002	Y	1	58	0.00636004	\$857.80	R
534025	\$103,775	\$25,855	\$0	\$129,631	7	S	0.00011	\$14	N	0.002	Y	1	58	0.00636004	\$824.46	R
534026	\$105,680	\$38,783	\$0	\$144,462	7	S	0.00011	\$16	N	0.002	Y	1	58	0.00636004	\$918.78	R
534027	\$277,848	\$32,319	\$0	\$310,167	7	S	0.00011	\$34	N	0.002	Y	1	58	0.00636004	\$1,972.67	R
534028	\$277,848	\$32,319	\$0	\$310,167	7	S	0.00011	\$34	N	0.001	Y	1	58	0.00636004	\$1,972.67	R
534113	\$204,180	\$23,270	\$0	\$227,449	7	S	0.00011	\$25	N	0.0005	Y	1	59	0.00646934	\$1,471.44	R
534134	\$88,589	\$25,855	\$0	\$114,444	6	S	0.00011	\$13	N	0.002	Y	1	38	0.004171505	\$477.40	R
534152	\$74,261	\$19,391	\$0	\$93,653	7	S	0.00011	\$10	N	0.002	Y	1	59	0.00646934	\$605.87	R
534153	\$133,290	\$155,132	\$0	\$288,421	7	S	0.00011	\$32	N	0.002	Y	1	60	0.006578628	\$1,897.41	R
534155	\$70,453	\$38,783	\$0	\$109,236	7	S	0.00011	\$12	N	0.002	Y	1	60	0.006578628	\$718.62	R
534156	\$79,593	\$353,596	\$580,000	\$1,013,189	7	S	0.00011	\$111	N	0.002	Y	1	60	0.006578628	\$6,665.39	R
534157	\$68,705	\$19,391	\$0	\$88,096	7	S	0.00011	\$10	N	0.002	Y	1	60	0.006578628	\$579.55	R
534158	\$259,724	\$91,838	\$580,000	\$931,562	7	S	0.00011	\$102	N	0.002	Y	1	60	0.006578628	\$6,128.40	R
534159	\$241,919	\$100,835	\$0	\$342,754	7	S	0.00011	\$38	N	0.002	Y	1	60	0.006578628	\$2,254.85	R
534160	\$677,373	\$100,835	\$0	\$778,208	7	S	0.00011	\$86	N	0.002	Y	1	60	0.006578628	\$5,119.54	R
534161	\$72,576	\$23,270	\$0	\$95,846	7	S	0.00011	\$11	N	0.002	Y	1	61	0.006687905	\$641.00	R
534162	\$48,992	\$12,928	\$0	\$61,920	7	S	0.00011	\$7	N	0.0005	Y	1	61	0.006687905	\$414.12	R
534163	\$671,941	\$291,647	\$0	\$963,589	7	S	0.00011	\$106	N	0.002	Y	1	61	0.006687905	\$6,444.39	R
534164	\$204,695	\$126,691	\$0	\$331,385	7	O	0.00017	\$56	N	0.002	Y	1	61	0.010317289	\$3,418.99	R
534165	\$72,357	\$72,395	\$0	\$144,752	7	S	0.00011	\$16	N	0.002	Y	1	61	0.006687905	\$968.09	R
534168	\$195,970	\$46,539	\$0	\$242,509	6	S	0.00011	\$27	N	0.002	Y	1	61	0.006687905	\$1,621.88	R
534169	\$190,632	\$38,783	\$0	\$229,415	7	S	0.00011	\$25	N	0.001	Y	1	63	0.006906421	\$1,584.44	R
534174	\$105,477	\$31,026	\$0	\$136,503	7	S	0.00011	\$15	N	0.002	Y	1	64	0.007015662	\$957.66	R
534176	\$178,989	\$32,319	\$0	\$211,308	7	S	0.00011	\$23	N	0.002	Y	1	65	0.00712489	\$1,505.55	R
534177	\$195,970	\$32,319	\$0	\$228,289	7	S	0.00011	\$25	N	0.002	Y	1	65	0.00712489	\$1,626.53	R
534182	\$557,912	\$100,835	\$0	\$658,747	7	S	0.00011	\$72	N	0.002	Y	1	67	0.007343311	\$4,837.38	R
534183	\$72,357	\$15,513	\$0	\$87,870	6	S	0.00011	\$10	N	0.002	Y	1	61	0.006687905	\$587.67	R
540005	\$756,660	\$3,394,430	\$1,160,000	\$5,311,090	6	S	0.00011	\$584	Y	0.002	Y	1	15	0.00164873	\$8,756.55	R
540023	\$2,803,153	\$0	\$1,160,000	\$3,963,153	6	S	0.00011	\$436	Y	0.002	Y	1	20	0.002197703	\$8,709.83	R
540025	\$465,655	\$1,410,606	\$1,160,000	\$3,036,260	6	S	0.00011	\$334	N	0.002	Y	1	17	0.001868355	\$5,672.81	R
540043	\$550,386	\$2,101,591	\$580,000	\$3,231,976	4	S	0.0005	\$1,616	N	0.002	Y	1	21	0.010447666	\$33,766.61	R
540048	\$2,066,440	\$1,168,480	\$1,160,000	\$4,394,920	7	R	0.000077	\$338	Y	0.002	Y	1	17	0.001308194	\$5,749.41	R
540064	\$700,277	\$383,572	\$1,160,000	\$2,243,849	6	S	0.00011	\$247	N	0.002	Y	1	45	0.00493804	\$11,080.22	R
544077	\$72,576	\$20,684	\$0	\$93,260	6	S	0.00011	\$10	N	0.002	Y	1	62	0.006797169	\$633.90	R
550001	\$2,850,335	\$3,509,913	\$2,900,000	\$9,260,248	7	S	0.00011	\$1,019	N	0.002	Y	1	29	0.003185092	\$29,494.74	R
550005	\$1,324,810	\$1,872,984	\$2,900,000	\$6,097,794	7	R	0.000077	\$470	N	0.002	Y	1	39	0.002998611	\$18,284.91	R
550006	\$586,411	\$2,131,795	\$2,900,000	\$5,618,206	7	S	0.00011	\$618	N	0.002	Y	1	15	0.00164873	\$9,262.91	R
550008	\$548,578	\$1,357,412	\$1,160,000	\$3,065,990	8	S	0.000022	\$7	N	0.002	Y	1	15	3.29995E-05	\$101.18	R
550028	\$928,969	\$2,266,803	\$2,900,000	\$6,095,771	4	S	0.0005	\$3,048	Y	0.002	Y	1	15	0.007473807	\$45,558.61	R
550033	\$1,777,577	\$287,679	\$1,160,000	\$3,225,256	7	S	0.00011	\$355	N	0.002	Y	1	54	0.005922718	\$19,102.28	R
550034	\$486,959	NA	\$1,160,000	\$1,646,959	6	S	0.00011	\$181	N	0.002	Y	1	18	0.00197815	\$3,257.93	R
550051	\$308,002	\$87,957	\$580,000	\$975,959	7	S	0.00011	\$107	N	0.002	Y	1	16	0.001758549	\$1,716.27	R
550054	\$281,219	\$1,838,753	\$1,160,000	\$3,279,972	6	S	0.00011	\$361	N	0.002	Y	1	15	0.00164873	\$5,407.79	R
550058	\$668,352	\$2,050,834	\$1,160,000	\$3,879,186	6	S	0.00011	\$427	N	0.002	Y	1	24	0.002636663	\$10,228.11	R
550062	\$2,872,898	\$361,974	\$580,000	\$3,814,871	7	S	0.00011	\$420	N	0.002	Y	1	37	0.004061952	\$15,495.82	R
550065	\$3,664,954	\$650,637	\$1,160,000	\$5,475,591	7	S	0.00011	\$602	Y	0.002	Y	1	20	0.002197703	\$12,033.72	R
550073	\$731,438	\$1,872,984	\$2,900,000	\$5,504,422	7	S	0.00011	\$605	N	0.002	Y	1	15	0.00164873	\$9,075.31	R
550803	\$74,261	\$0	\$0	\$74,261	7	S	0.00011	\$8	N	0.001	Y	1	71	0.007780007	\$577.75	R
550804	\$917,310	\$232,697	\$1,160,000	\$2,310,007	8	S	0.000022	\$5	N	0.002	Y	1	61	0.000134191	\$309.98	R
554001	\$304,087	\$1,654,736	\$580,000	\$2,538,824	7	S	0.00011	\$279	N	0.002	Y	1	15	0.00164873	\$4,185.84	R
554033	\$568,447	\$424,768	\$580,000	\$1,573,215	7	S	0.00011	\$173	N	0.002	Y	1	58	0.00636004	\$10,005.71	R
554034	\$281,305	\$424,768	\$580,000	\$1,286,073	7	S	0.00011	\$141	N	0.002	Y	1	58	0.00636004	\$8,179.48	R
554035	\$287,125	\$424,768	\$580,000	\$1,291,893	7	S										



Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
555024	\$537,060	\$553,838	\$1,160,000	\$2,250,898	7	S	0.00011	\$248	N	0.002	Y	1	53	0.005813357	\$13,085.27	R
560008	\$742,613	\$103,421	\$0	\$846,034	6	S	0.00011	\$93	N	0.002	Y	1	30	0.003294742	\$2,787.46	R
560013	\$3,612,473	\$822,989	\$0	\$4,435,462	7	S	0.00011	\$488	N	0.002	Y	1	50	0.005485204	\$24,329.41	R
560023	\$603,951	\$87,502	\$580,000	\$1,271,454	6	S	0.00011	\$140	N	0.002	Y	1	16	0.001758549	\$2,235.91	R
560026	\$1,480,036	\$4,086,154	\$1,160,000	\$6,726,191	6	S	0.00011	\$740	N	0.002	Y	1	15	0.00164873	\$11,089.67	R
560027	\$863,085	\$4,086,154	\$1,160,000	\$6,109,239	7	S	0.00011	\$672	N	0.002	Y	1	15	0.00164873	\$10,072.49	R
560033	\$510,212	\$1,360,814	\$580,000	\$2,451,025	7	S	0.00011	\$270	N	0.002	Y	1	18	0.00197815	\$4,848.49	R
560037	\$428,524	\$1,397,275	\$580,000	\$2,405,799	7	S	0.00011	\$265	N	0.002	Y	1	24	0.002636663	\$6,343.28	R
560049	\$604,140	\$1,494,227	\$580,000	\$2,678,367	6	S	0.00011	\$295	N	0.002	Y	1	24	0.002636663	\$7,061.95	R
560058	\$2,603,952	\$399,149	\$0	\$3,003,102	7	S	0.00011	\$330	N	0.002	Y	1	50	0.005485204	\$16,472.63	R
560059	\$3,170,433	\$399,149	\$0	\$3,569,582	7	S	0.00011	\$393	N	0.002	Y	1	50	0.005485204	\$19,579.88	R
560060	\$1,704,053	\$15,739,815	\$1,160,000	\$18,603,868	8	R	0.0000017	\$32	Y	0.002	Y	1	56	9.51955E-05	\$1,771.01	R
560061	\$5,256,117	\$15,739,815	\$1,160,000	\$22,155,932	8	R	0.0000017	\$38	Y	0.002	Y	1	56	9.51955E-05	\$2,109.15	R
560062	\$773,352	\$22,627,064	\$1,160,000	\$24,560,416	7	S	0.00011	\$2,702	Y	0.002	Y	1	55	0.006032066	\$148,150.06	R
560809	\$111,392	\$51,308	\$0	\$162,700	7	O	0.00017	\$28	N	0.002	Y	1	67	0.011326337	\$1,842.80	R
564067	\$1,040,201	\$886,609	\$580,000	\$2,506,810	7	S	0.00011	\$276	N	0.002	Y	1	66	0.007234106	\$18,134.53	R
570006	\$14,547,098	\$1,966,313	\$2,900,000	\$19,413,411	7	S	0.00011	\$2,135	Y	0.002	Y	1	15	0.00164873	\$32,007.48	R
570016	\$1,112,398	\$4,614,066	\$1,160,000	\$6,886,463	7	S	0.00011	\$758	N	0.002	Y	1	26	0.002856071	\$19,668.23	R
570017	\$30,948,511	\$20,660,963	\$2,900,000	\$54,509,474	6	S	0.00011	\$5,996	Y	0.002	Y	1	24	0.002636663	\$143,723.12	T
570018	\$42,553,001	\$19,283,565	\$2,900,000	\$64,736,567	7	R	0.000077	\$4,985	Y	0.002	Y	1	24	0.001846365	\$119,527.30	M
570021	\$1,669,357	\$3,761,615	\$1,160,000	\$6,590,972	7	S	0.00011	\$725	N	0.002	Y	1	26	0.002856071	\$18,824.28	R
570026	\$1,060,597	\$1,569,069	\$580,000	\$3,209,666	7	S	0.00011	\$353	N	0.002	Y	1	26	0.002856071	\$9,167.03	R
570028	\$735,187	\$1,743,410	\$580,000	\$3,058,597	7	S	0.00011	\$336	N	0.002	Y	1	15	0.00164873	\$5,042.80	R
570032	\$555,438	\$157,623	\$1,160,000	\$1,873,061	6	S	0.00011	\$206	N	0.002	Y	1	31	0.003404379	\$6,376.61	R
570033	\$4,866,222	\$10,356,197	\$1,160,000	\$16,382,419	7	S	0.00011	\$1,802	Y	0.002	Y	1	15	0.00164873	\$27,010.19	R
570036	\$1,124,876	\$1,970,241	\$580,000	\$3,675,117	7	S	0.00011	\$404	N	0.002	Y	1	41	0.004500092	\$16,538.37	R
570040	\$5,662,734	\$1,834,201	\$580,000	\$8,076,935	7	S	0.00011	\$888	N	0.002	Y	1	15	0.00164873	\$13,316.69	R
570055	\$7,419,574	\$2,274,516	\$2,900,000	\$12,594,090	7	R	0.000077	\$970	Y	0.0005	Y	1	20	0.001538874	\$19,380.72	M
570085	\$1,062,383	\$458,550	\$580,000	\$2,100,933	7	S	0.00011	\$231	N	0.002	Y	1	48	0.005266374	\$11,064.30	R
570802	\$226,592	\$117,641	\$0	\$344,234	7	S	0.00011	\$38	N	0.002	Y	1	55	0.006032066	\$2,076.44	R
570803	\$157,091	\$16,160	\$0	\$173,251	7	S	0.00011	\$19	N	0.0005	Y	1	55	0.006032066	\$1,045.06	R
570804	\$100,638	\$95,343	\$0	\$195,981	8	S	0.0000022	\$0	N	0.001	Y	1	56	0.000123193	\$24.14	R
570805	\$100,638	\$90,493	\$0	\$191,132	8	S	0.0000022	\$0	N	0.002	Y	1	56	0.000123193	\$23.55	R
570806	\$162,804	\$84,030	\$0	\$246,833	7	S	0.00011	\$27	N	0.001	Y	1	56	0.006141403	\$1,515.90	R
570810	\$669,260	\$103,421	\$580,000	\$1,352,681	7	O	0.00017	\$230	N	0.0005	Y	1	62	0.010485535	\$14,183.58	R
570811	\$146,618	\$32,319	\$0	\$178,938	7	O	0.00017	\$30	N	0.0005	Y	1	62	0.010485535	\$1,876.26	R
570813	\$175,555	\$19,391	\$0	\$194,947	8	S	0.0000022	\$0	N	0.002	Y	1	66	0.000145419	\$28.30	R
574008	\$205,885	\$193,128	\$1,160,000	\$1,559,013	6	S	0.00011	\$171	N	0.001	Y	1	53	0.005813357	\$9,063.10	R
574009	\$78,013	\$53,096	\$580,000	\$711,109	6	S	0.00011	\$78	N	0.001	Y	1	15	0.00164873	\$1,172.43	R
574011	\$253,781	\$48,479	\$0	\$302,259	7	S	0.00011	\$33	N	0.002	Y	1	15	0.00164873	\$498.34	R
574012	\$311,045	\$19,391	\$0	\$330,437	6	S	0.00011	\$36	N	0.0005	Y	1	15	0.00164873	\$544.80	R
574013	\$533,526	\$103,421	\$580,000	\$1,216,947	6	O	0.00017	\$207	N	0.002	Y	1	42	0.007115173	\$8,658.79	R
574016	\$187,994	\$51,711	\$0	\$239,705	7	S	0.00011	\$26	N	0.002	Y	1	53	0.005813357	\$1,393.49	R
574038	\$257,495	\$32,319	\$0	\$289,814	6	S	0.00011	\$32	N	0.002	Y	1	15	0.00164873	\$477.83	R
574041	\$421,004	\$393,000	\$580,000	\$1,394,004	6	S	0.00011	\$153	N	0.002	Y	1	41	0.004500092	\$6,273.15	R
574054	\$99,015	\$90,493	\$0	\$189,508	7	S	0.00011	\$21	N	0.002	Y	1	36	0.003952386	\$749.01	R
574071	\$97,735	\$13,574	\$0	\$111,309	4	O	0.0006	\$67	N	0.0005	N	1	50	0.029563204	\$3,290.65	R
574072	\$232,242	\$13,574	\$0	\$245,816	4	O	0.0006	\$147	N	0.001	Y	1	50	0.029563204	\$7,267.11	R
574073	\$132,572	\$13,574	\$0	\$146,146	4	O	0.0006	\$88	N	0.002	Y	1	50	0.029563204	\$4,320.54	R
574081	\$202,119	\$127,984	\$0	\$330,103	5	S	0.00024	\$1	N	0.002	Y	1	41	0.009792915	\$3,232.67	R
574082	\$66,645	\$32,319	\$0	\$98,964	7	S	0.00011	\$11	N	0.002	Y	1	47	0.005156941	\$510.35	R
574085	\$536,639	\$64,638	\$0	\$601,277	6	S	0.00011	\$66	N	0.002	Y	1	26	0.002856071	\$1,717.29	R
574088	\$145,838	\$73,007	\$0	\$218,845	7	S	0.00011	\$24	N	0.002	Y	1	15	0.00164873	\$360.82	R
574090	\$166,105	\$233,623	\$580,000	\$979,727	7	S	0.00011	\$108	N	0.002	Y	1	26	0.002856071	\$2,798.17	R
574096	\$796,787	\$108,963	\$580,000	\$1,485,750	7	S	0.00011	\$163	N	0.0001	N	1	15	0.00164873	\$2,449.60	R
574097	\$243,998	\$54,482	\$580,000	\$878,479	7	S	0.00011	\$97	N	0.0005	Y	1	15	0.00164873	\$1,448.37	R
574100	\$292,207	\$53,096	\$580,000	\$925,303	3	S	0.0013	\$1,203	N	0.0005	N	1	50	0.062972161	\$58,268.33	R
574102	\$452,326	\$103,421	\$0	\$555,747	6	S	0.00011	\$61	N	0.0005	Y	1	50	0.005485204	\$3,048.39	R
574105	\$127,577	\$11,635	\$0	\$139,212	7	S	0.00011	\$15	N	0.0005	Y	1	61	0.006687905	\$931.04	R
574106	\$45,574	NA	\$0	\$45,574	4	O	0.0006	\$27	N	0.0001	N	1	50	0.029563204	\$1,347.31	R
574108	\$76,977	\$32,319	\$0	\$109,296	7	S	0.00011	\$12	N	0.0001	N	1	49	0.005375795	\$587.55	R
574110	\$507,015	\$38,783	\$0	\$545,798	7	S	0.00011	\$60	N	0.0001	N	1	52	0.005703985	\$3,113.22	R
574111	\$107,100	\$29,087	\$0	\$136,187	7	S	0.00011	\$15	N	0.0001	N	1	53	0.005813357	\$791.70	R
574112	\$229,353	\$65,378	\$580,000	\$874,731	7	S	0.00011	\$96	N	0.0005	Y	1	51	0.0055946	\$4,893.77	R
574115	\$336,072	\$94,192	\$580,000	\$1,010,264	7	S	0.00011	\$111	N	0.0005	Y	1	55	0.006032066	\$6,093.98	R
574116	\$201,695	\$108,963	\$580,000	\$890,658	7	S	0.00011	\$98	N	0.0005	Y	1	56	0.006141403	\$5,469.89	R
574118	\$154,953	\$85,322	\$0	\$240,275	7	S	0.00011	\$26	N	0.0005	Y	1	59	0.00646934	\$1,554.42	R
574119	\$153,611	\$77,566	\$0	\$231,176	6	S	0.00011	\$25	N	0.0005	Y	1	56	0.006141403	\$1,419.74	R
574120	\$106,257	\$25,855	\$0	\$132,112	6	S	0.00011	\$15	N	0.0005	Y	1	58	0.00636004	\$840.24	R
574121	\$455,120	\$36,844	\$0	\$491,963	7	S	0.00011	\$54	N	0.0001	N	1	59	0.00646934	\$3,182.68	R
574122	\$151,535	\$25,855	\$0	\$177,390	7	S	0.00011	\$20	N	0.0005	Y	1	59	0.00646934	\$1,147.60	R
574123	\$220,580	\$217,926	\$580,000	\$1,018,506	7	S	0.00011	\$112	N	0.002	Y	1	60	0.006578628	\$6,700.37	R
574124	\$105,102	\$32,319	\$0	\$137,421	7	S	0.00011	\$15	N	0.002	Y	1	60	0.006578628	\$904.04	R
574127	\$256,980	\$153,615	\$1,160,000	\$1,570,595	7	S	0.00011	\$173	N	0.0005	Y	1	62	0.006797169	\$10,675.60	R
574129	\$105,960	\$9,696	\$0	\$115,656	7	S	0.00011	\$13	N							



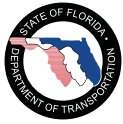
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
574135	\$189,134	\$25,855	\$0	\$214,989	7	S	0.00011	\$24	N	0.002	Y	1	65	0.00712489	\$1,531.77	R
574136	\$534,368	\$588,401	\$580,000	\$1,702,768	7	S	0.00011	\$187	N	0.002	Y	1	65	0.00712489	\$12,132.03	R
574137	\$339,233	\$382,117	\$1,160,000	\$1,881,350	7	S	0.00011	\$207	N	0.002	Y	1	65	0.00712489	\$13,404.41	R
574138	\$607,236	\$620,941	\$1,160,000	\$2,388,176	7	S	0.00011	\$263	N	0.002	Y	1	65	0.00712489	\$17,015.49	R
574139	\$402,881	\$39,822	\$0	\$442,703	7	S	0.00011	\$49	N	0.002	Y	1	65	0.00712489	\$3,154.21	R
574142	\$402,881	\$51,711	\$0	\$454,591	7	S	0.00011	\$50	N	0.0005	Y	1	67	0.007343311	\$3,338.20	R
574146	\$264,925	\$64,638	\$0	\$329,563	7	S	0.00011	\$36	N	0.0005	Y	1	70	0.007670851	\$2,528.03	R
574150	\$190,501	\$53,096	\$580,000	\$823,597	8	S	0.0000022	\$2	N	0.0005	Y	1	72	0.00158388	\$130.45	R
574151	\$400,454	\$127,430	\$580,000	\$1,107,884	8	S	0.0000022	\$2	N	0.0005	Y	1	73	0.00160587	\$177.91	R
574152	\$242,309	\$49,778	\$0	\$292,087	8	S	0.0000022	\$1	N	0.0005	Y	1	73	0.00160587	\$46.91	R
580002	\$4,860,322	\$3,177,581	\$2,900,000	\$10,937,903	7	S	0.00011	\$1,203	Y	0.0002	Y	1	36	0.003952386	\$43,230.82	R
580004	\$4,050,940	\$3,177,581	\$2,900,000	\$10,128,520	7	S	0.00011	\$1,114	Y	0.0005	Y	1	36	0.003952386	\$40,031.83	M
580005	\$17,013,141	\$3,177,581	\$2,900,000	\$23,090,721	7	S	0.00011	\$2,540	Y	0.0005	Y	1	36	0.003952386	\$91,263.45	M
580007	\$3,163,987	\$3,177,581	\$2,900,000	\$9,241,568	7	S	0.00011	\$1,017	Y	0.0005	Y	1	32	0.003514005	\$32,474.92	M
580013	\$2,537,963	\$17,605,020	\$2,900,000	\$23,042,984	4	S	0.0005	\$11,521	Y	0.0005	N	1	15	0.007473807	\$172,218.81	M
580030	\$508,404	\$3,551,004	\$2,900,000	\$6,959,408	7	S	0.00011	\$766	N	0.0005	Y	1	16	0.00175849	\$12,238.46	M
580088	\$4,454,624	\$2,462,802	\$1,160,000	\$8,077,426	7	S	0.00011	\$889	N	0.0005	Y	1	10	0.005485204	\$44,306.33	R
580096	\$1,781,054	\$15,287,684	\$2,900,000	\$19,968,737	7	S	0.00011	\$2,197	N	0.0005	Y	1	53	0.005813357	\$116,085.40	R
580102	\$2,722,914	\$43,440,343	\$2,900,000	\$49,063,258	7	S	0.00011	\$5,397	Y	0.0005	Y	1	60	0.006578628	\$322,768.95	R
580801	\$164,708	\$18,616	\$0	\$183,324	7	S	0.00011	\$20	N	0.0005	Y	1	54	0.005922718	\$1,085.78	R
580802	\$167,158	\$46,539	\$0	\$213,698	7	S	0.00011	\$24	N	0.0001	N	1	54	0.005922718	\$1,265.67	R
580803	\$70,453	\$119,466	\$0	\$189,919	7	S	0.00011	\$21	N	0.0001	N	1	52	0.005703985	\$1,083.30	R
580804	\$133,539	\$72,395	\$0	\$205,934	7	S	0.00011	\$23	N	0.0005	Y	1	56	0.006141403	\$1,264.72	R
580805	\$40,424	\$624,404	\$0	\$664,828	7	O	0.00017	\$113	N	0.0001	N	1	57	0.009644019	\$6,411.61	M
580806	\$162,804	\$49,771	\$0	\$212,575	8	O	0.0000085	\$2	N	0.0001	Y	1	58	0.000492881	\$104.77	R
580807	\$218,024	\$77,566	\$0	\$295,589	8	S	0.0000022	\$1	N	0.0002	Y	1	61	0.000134191	\$39.67	R
580809	\$140,890	\$38,783	\$0	\$179,673	8	S	0.0000022	\$0	N	0.0001	Y	1	63	0.000138591	\$24.90	R
580810	\$209,954	\$77,566	\$0	\$287,520	8	S	0.0000022	\$1	N	0.002	Y	1	64	0.00014079	\$40.48	R
580811	\$156,092	\$77,566	\$0	\$233,658	7	O	0.00017	\$40	N	0.002	Y	1	64	0.010821942	\$2,528.63	R
580812	\$261,023	\$122,812	\$0	\$383,835	7	S	0.00011	\$42	N	0.0005	Y	1	65	0.00712489	\$2,734.78	R
580813	\$260,913	\$27,148	\$0	\$288,061	7	S	0.00011	\$32	N	0.0001	N	1	65	0.00712489	\$2,052.40	R
580814	\$174,322	\$23,270	\$0	\$197,592	7	O	0.00017	\$34	N	0.002	Y	1	67	0.011326337	\$2,237.99	R
580818	\$58,903	\$23,893	\$0	\$82,797	7	O	0.00017	\$14	N	0.0002	Y	1	70	0.011830475	\$979.53	R
580819	\$396,747	\$23,658	\$0	\$420,405	7	S	0.00011	\$46	N	0.0005	Y	1	72	0.007889152	\$3,316.64	R
584042	\$100,919	\$32,319	\$0	\$133,238	7	S	0.00011	\$15	N	0.0005	Y	1	49	0.005375795	\$716.26	R
584046	\$61,791	\$11,635	\$0	\$73,426	7	O	0.00017	\$12	N	0.0005	Y	1	26	0.00441062	\$323.85	R
584047	\$60,636	\$23,270	\$0	\$83,906	7	O	0.00017	\$14	N	0.0005	Y	1	26	0.00441062	\$370.08	R
584050	\$99,967	\$15,513	\$0	\$115,480	6	O	0.00017	\$20	N	0.0005	Y	1	26	0.00441062	\$509.34	R
584059	\$80,317	\$116,349	\$0	\$196,666	5	O	0.00032	\$3	N	0.0005	Y	1	26	0.008286805	\$1,629.73	R
584065	\$335,783	\$32,319	\$0	\$368,102	7	S	0.00011	\$40	N	0.0005	Y	1	26	0.002856071	\$1,051.33	R
584067	\$68,923	\$106,653	\$0	\$175,576	6	S	0.00011	\$19	N	0.0001	N	1	26	0.002856071	\$501.46	R
584069	\$292,925	\$90,493	\$0	\$383,418	6	O	0.00017	\$65	N	0.0005	Y	1	26	0.00441062	\$1,691.11	R
584084	\$623,214	\$434,368	\$580,000	\$1,637,583	6	O	0.00017	\$278	N	0.0005	Y	1	41	0.006946354	\$11,375.23	R
584106	\$142,482	\$90,493	\$0	\$232,976	4	S	0.0005	\$116	N	0.0002	N	1	26	0.012919074	\$3,009.83	R
584111	\$227,259	\$73,884	\$580,000	\$881,143	7	S	0.00011	\$97	N	0.0005	Y	1	52	0.005703985	\$5,026.03	R
584113	\$343,697	\$217,184	\$0	\$560,881	5	O	0.00032	\$10	N	0.0005	Y	1	51	0.01619012	\$9,080.73	R
584116	\$101,871	\$32,689	\$0	\$134,560	7	O	0.00017	\$23	N	0.0002	Y	1	51	0.008633255	\$1,161.69	R
584117	\$104,727	\$31,026	\$0	\$135,754	4	S	0.0005	\$68	N	0.0002	N	1	51	0.025183838	\$3,418.81	R
584119	\$161,852	\$117,641	\$0	\$279,493	6	S	0.00011	\$31	N	0.0001	N	1	51	0.0055946	\$1,563.65	R
584122	\$67,597	\$31,858	\$0	\$99,454	7	S	0.00011	\$11	N	0.0002	Y	1	53	0.005813357	\$578.16	R
584123	\$42,156	\$26,548	\$0	\$68,704	7	S	0.00011	\$8	N	0.0005	Y	1	53	0.005813357	\$399.40	R
584125	\$171,372	\$42,015	\$0	\$213,387	7	O	0.00017	\$36	N	0.0001	N	1	56	0.00947563	\$2,021.98	R
584126	\$78,546	\$65,378	\$580,000	\$723,923	6	S	0.00011	\$80	N	0.0002	Y	1	52	0.005703985	\$4,129.25	R
584128	\$249,080	\$38,701	\$580,000	\$867,781	6	O	0.00017	\$148	N	0.002	Y	1	54	0.009138766	\$7,930.45	R
584129	\$96,159	\$20,684	\$0	\$116,843	6	O	0.00017	\$20	N	0.0002	Y	1	54	0.009138766	\$1,067.80	R
584132	\$125,798	\$90,493	\$0	\$216,291	6	O	0.00017	\$37	N	0.0002	Y	1	54	0.009138766	\$1,976.63	R
584134	\$181,179	\$79,644	\$580,000	\$840,823	7	S	0.00011	\$92	N	0.0002	Y	1	56	0.006141403	\$5,163.83	R
584135	\$224,117	\$79,644	\$580,000	\$883,761	6	S	0.00011	\$97	N	0.0002	Y	1	56	0.006141403	\$5,427.53	R
584136	\$95,207	\$23,270	\$0	\$118,477	7	S	0.00011	\$13	N	0.0005	Y	1	54	0.005922718	\$701.71	R
584137	\$429,523	\$719,723	\$1,160,000	\$2,309,246	7	S	0.00011	\$254	N	0.0002	Y	1	55	0.006032066	\$13,929.53	R
584139	\$194,222	\$48,479	\$0	\$242,700	7	S	0.00011	\$27	N	0.0001	N	1	56	0.006141403	\$1,490.52	R
584140	\$365,594	\$87,908	\$0	\$453,502	7	S	0.00011	\$50	N	0.0005	Y	1	57	0.006250727	\$2,834.72	R
584143	\$194,222	\$48,479	\$0	\$242,700	6	S	0.00011	\$27	N	0.002	Y	1	56	0.006141403	\$1,490.52	R
584145	\$135,098	\$451,514	\$580,000	\$1,166,612	7	S	0.00011	\$128	N	0.0001	N	1	57	0.006250727	\$7,292.17	R
584147	\$136,146	\$286,719	\$580,000	\$1,002,864	7	S	0.00011	\$110	N	0.001	Y	1	57	0.006250727	\$6,268.63	R
584148	\$122,817	\$32,319	\$0	\$155,136	7	S	0.00011	\$17	N	0.001	Y	1	58	0.00636004	\$986.67	R
584150	\$86,638	\$13,574	\$0	\$100,212	6	S	0.00011	\$11	N	0.001	Y	1	59	0.00646934	\$648.31	R
584151	\$100,638	\$62,053	\$0	\$162,691	7	S	0.00011	\$18	N	0.0005	Y	1	58	0.00636004	\$1,034.72	R
584152	\$273,219	\$126,277	\$580,000	\$979,496	7	S	0.00011	\$108	N	0.0005	Y	1	59	0.00646934	\$6,336.69	R
584153	\$86,638	\$139,618	\$0	\$226,257	7	O	0.00017	\$38	N	0.0001	N	1	60	0.010149015	\$2,296.29	R
584154	\$81,878	\$77,566	\$0	\$159,444	7	S	0.00011	\$18	N	0.002	Y	1	60	0.006578628	\$1,048.92	R
584155	\$82,830	\$77,566	\$0	\$160,396	7	S	0.00011	\$18	N	0.002	Y	1	60	0.006578628	\$1,055.19	R
584156	\$168,625	\$96,957	\$0	\$265,582	7	S	0.00011	\$29	N	0.002	Y	1	59	0.00646934	\$1,718.14	R
584158	\$180,873	\$917,081	\$1,160,000	\$2,257,955	6	S	0.00011	\$248	N	0.002	Y	1	59	0.00646934	\$14,607.48	R
584159	\$534,110	\$309,953	\$580,000	\$1,424,063	7	S	0.00011	\$157	N	0.002	Y	1	60	0.006578628	\$9,368.38	R
584161	\$89,026	NA	\$0	\$89,026	6	S	0.00011	\$10	N	0.002	Y	1	61	0.00		



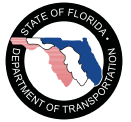
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
584169	\$105,960	\$122,812	\$0	\$228,773	7	S	0.00011	\$25	N	0.002	Y	1	62	0.006797169	\$1,555.01	R
584170	\$521,827	\$281,176	\$0	\$803,003	6	S	0.00011	\$88	N	0.002	Y	1	62	0.006797169	\$5,458.15	R
584172	\$173,183	\$51,711	\$0	\$224,893	7	O	0.00017	\$38	N	0.002	Y	1	63	0.010653753	\$2,395.95	R
584176	\$800,970	\$45,247	\$0	\$846,217	7	S	0.00011	\$93	N	0.002	Y	1	63	0.006906421	\$5,844.33	R
584178	\$1,206,117	\$507,200	\$580,000	\$2,293,317	7	S	0.00011	\$252	N	0.002	Y	1	65	0.00712489	\$16,339.63	R
584180	\$141,281	\$23,270	\$0	\$164,550	7	S	0.00011	\$18	N	0.002	Y	1	66	0.007234106	\$1,190.37	M
584182	\$143,559	\$20,684	\$0	\$164,244	8	S	0.0000022	\$0	N	0.002	Y	1	67	0.000147389	\$24.21	R
584188	\$119,008	\$42,661	\$0	\$161,670	7	S	0.00011	\$18	N	0.002	Y	1	69	0.007561683	\$1,222.50	R
584189	\$211,921	\$46,539	\$0	\$258,460	7	S	0.00011	\$28	N	0.002	Y	1	69	0.007561683	\$1,954.39	R
584190	\$174,322	\$135,094	\$0	\$309,416	7	S	0.00011	\$34	N	0.002	Y	1	70	0.007670851	\$2,373.48	R
584191	\$139,408	\$32,319	\$0	\$171,727	8	O	0.0000085	\$1	N	0.002	Y	1	70	0.000594826	\$102.15	R
584192	\$262,053	\$45,247	\$0	\$307,299	7	S	0.00011	\$34	N	0.002	Y	1	70	0.007670851	\$2,357.24	R
584193	\$498,197	\$51,711	\$0	\$549,907	7	O	0.00017	\$93	N	0.002	Y	1	62	0.010485535	\$5,766.07	T
584194	\$269,459	\$146,014	\$580,000	\$995,473	8	S	0.0000022	\$2	N	0.002	Y	1	71	0.000156188	\$155.48	R
584196	\$209,642	\$71,102	\$0	\$280,744	8	S	0.0000022	\$1	N	0.002	Y	1	72	0.000158388	\$44.47	R
584197	\$210,782	\$45,247	\$0	\$256,028	8	S	0.0000022	\$1	N	0.002	Y	1	72	0.000158388	\$40.55	R
584198	\$205,584	\$98,250	\$0	\$303,834	8	S	0.0000022	\$1	N	0.002	Y	1	73	0.000160587	\$48.79	R
584199	\$91,611	\$335,606	\$580,000	\$1,007,217	3	O	0.0016	\$1,612	N	0.002	Y	1	46	0.071011522	\$71,524.01	R
584200	\$141,281	\$19,391	\$0	\$160,672	8	S	0.0000022	\$0	N	0.002	Y	1	72	0.000158388	\$25.45	R
584201	\$116,557	\$1,982,555	\$580,000	\$2,679,112	8	S	0.0000022	\$6	N	0.002	Y	1	69	0.000151789	\$406.66	R
584202	\$127,768	NA	\$580,000	\$707,768	8	S	0.0000022	\$2	N	0.002	Y	1	72	0.000158388	\$112.10	R
584203	\$96,349	NA	\$580,000	\$676,349	8	S	0.0000022	\$1	N	0.002	Y	1	72	0.000158388	\$107.13	R
585001	\$205,335	\$95,573	\$580,000	\$880,907	7	S	0.00011	\$97	N	0.002	Y	1	58	0.00636004	\$5,602.60	R
590004	\$1,060,597	\$176,084	\$580,000	\$1,816,682	6	S	0.00011	\$200	N	0.002	Y	1	30	0.003294742	\$5,985.50	R
590017	\$1,043,919	\$263,872	\$1,160,000	\$2,467,791	7	S	0.00011	\$271	N	0.002	Y	1	15	0.00164873	\$4,068.72	M
590018	\$565,528	\$7,225,473	\$1,160,000	\$9,451,001	3	S	0.0013	\$12,286	N	0.002	Y	1	16	0.020598425	\$194,675.74	R
590020	\$423,374	\$1,552,724	\$1,160,000	\$3,136,098	7	S	0.00011	\$345	N	0.002	Y	1	16	0.001758549	\$5,514.98	R
590021	\$423,374	\$1,307,557	\$1,160,000	\$2,890,931	6	S	0.00011	\$318	N	0.002	Y	1	16	0.001758549	\$5,083.84	R
590023	\$772,018	\$7,289,833	\$1,160,000	\$9,221,851	7	S	0.00011	\$1,014	Y	0.002	Y	1	30	0.003294742	\$30,383.62	R
590801	\$148,523	\$2,628,254	\$0	\$2,776,776	7	S	0.00011	\$305	N	0.002	Y	1	46	0.005047497	\$14,015.77	R
594008	\$420,424	\$64,638	\$0	\$485,062	7	S	0.00011	\$53	N	0.002	Y	1	55	0.006032066	\$2,925.93	R
594053	\$49,820	\$22,623	\$0	\$72,443	7	S	0.00011	\$8	N	0.002	Y	1	60	0.006578628	\$476.58	R
594055	\$84,562	\$42,661	\$0	\$127,224	7	S	0.00011	\$14	N	0.002	Y	1	60	0.006578628	\$836.96	R
600019	\$1,189,402	\$1,856,478	\$1,160,000	\$4,205,880	7	S	0.00011	\$463	N	0.002	Y	1	22	0.002417207	\$10,166.48	R
600022	\$978,910	\$980,668	\$580,000	\$2,539,578	7	S	0.00011	\$279	N	0.001	N	1	24	0.002636663	\$6,696.01	R
600088	\$162,382	\$4,300,779	\$1,160,000	\$5,623,161	7	S	0.00011	\$619	N	0.001	N	1	36	0.003952386	\$22,224.91	M
600111	\$1,734,184	\$21,526,092	\$1,160,000	\$24,420,276	7	S	0.00011	\$2,686	Y	0.0005	Y	1	55	0.006032066	\$147,304.73	R
600802	\$221,816	NA	\$580,000	\$801,816	7	S	0.00011	\$88	N	0.001	Y	1	54	0.005922718	\$4,748.93	M
600920	\$3,353,839	\$98,397,678	\$2,900,000	\$104,651,516	7	S	0.00011	\$11,512	Y	0.0001	N	1	34	0.00373322	\$390,687.12	R
602506	\$407,797	\$103,421	\$0	\$511,218	6	S	0.00011	\$56	N	0.002	Y	1	15	0.00164873	\$842.86	R
604002	\$107,459	\$32,319	\$0	\$139,778	7	S	0.00011	\$15	N	0.002	Y	1	51	0.00055946	\$782.00	R
604003	\$46,651	\$19,391	\$0	\$66,043	7	S	0.00011	\$7	N	0.0005	Y	1	51	0.00055946	\$369.48	R
604004	\$105,539	\$25,855	\$0	\$131,394	7	O	0.00017	\$22	N	0.0002	Y	1	51	0.008633255	\$1,134.36	R
604008	\$133,071	\$19,391	\$0	\$152,462	7	S	0.00011	\$17	N	0.0005	Y	1	51	0.00055946	\$852.96	R
604009	\$78,007	\$51,711	\$0	\$129,718	7	S	0.00011	\$14	N	0.0005	Y	1	26	0.002856071	\$370.48	R
604016	\$99,873	\$19,391	\$0	\$119,265	7	S	0.00011	\$13	N	0.0002	Y	1	51	0.00055946	\$667.24	R
604024	\$94,832	\$19,391	\$0	\$114,224	6	S	0.00011	\$13	N	0.0005	Y	1	46	0.005047497	\$576.55	R
604026	\$120,959	\$19,391	\$0	\$140,351	7	S	0.00011	\$15	N	0.0005	Y	1	41	0.004500092	\$631.59	M
604095	\$118,618	\$15,513	\$0	\$134,131	7	S	0.00011	\$15	N	0.0005	Y	1	54	0.005922718	\$794.42	R
604109	\$138,253	\$25,855	\$0	\$164,108	6	S	0.00011	\$18	N	0.0005	Y	1	56	0.006141403	\$1,007.85	R
604111	\$83,501	\$15,513	\$0	\$99,014	7	S	0.00011	\$11	N	0.002	Y	1	56	0.006141403	\$608.08	R
604112	\$178,958	\$13,574	\$0	\$192,532	6	S	0.00011	\$21	N	0.0005	Y	1	46	0.005047497	\$971.80	R
604114	\$236,768	\$23,270	\$0	\$260,038	7	S	0.00011	\$29	N	0.0001	N	1	57	0.006250727	\$1,625.43	R
604121	\$257,558	\$25,209	\$0	\$282,767	6	S	0.00011	\$31	N	0.0002	Y	1	60	0.006578628	\$1,860.22	R
604124	\$158,371	\$21,331	\$0	\$179,702	6	S	0.00011	\$20	N	0.002	Y	1	60	0.006578628	\$1,182.19	R
604129	\$103,791	\$19,391	\$0	\$123,182	6	S	0.00011	\$14	N	0.001	Y	1	62	0.006797169	\$837.29	R
604130	\$355,293	\$71,102	\$0	\$426,395	7	S	0.00011	\$47	N	0.002	Y	1	66	0.007234106	\$3,084.59	R
604133	\$391,222	\$51,711	\$0	\$442,932	7	S	0.00011	\$49	N	0.0005	Y	1	63	0.006906421	\$3,059.08	R
604135	\$252,126	\$32,319	\$0	\$284,445	7	S	0.00011	\$31	N	0.0005	Y	1	63	0.006906421	\$1,964.50	R
604136	\$241,560	\$51,711	\$0	\$293,270	8	S	0.0000022	\$1	N	0.0005	Y	1	63	0.000138591	\$40.64	R
604138	\$236,753	\$19,391	\$0	\$256,144	7	S	0.00011	\$28	N	0.002	Y	1	63	0.006906421	\$1,769.04	R
604142	\$634,077	\$2,696,837	\$1,160,000	\$4,490,914	7	S	0.00011	\$494	N	0.0005	Y	1	64	0.007015662	\$31,506.73	M
604149	\$77,242	\$25,855	\$0	\$103,098	7	O	0.00017	\$18	N	0.002	Y	1	65	0.010990102	\$1,133.06	R
604152	\$255,201	\$23,270	\$0	\$278,471	7	S	0.00011	\$31	N	0.002	Y	1	65	0.00712489	\$1,984.08	R
604155	\$280,721	\$84,954	\$580,000	\$945,675	7	S	0.00011	\$104	N	0.002	Y	1	65	0.00712489	\$6,737.83	R
604157	\$255,201	\$38,783	\$0	\$293,984	7	S	0.00011	\$32	N	0.002	Y	1	66	0.007234106	\$2,126.71	R
604158	\$380,858	\$27,148	\$0	\$408,006	7	S	0.00011	\$45	N	0.001	Y	1	66	0.007234106	\$2,951.56	R
604159	\$402,881	\$25,855	\$0	\$428,736	7	S	0.00011	\$47	N	0.001	Y	1	66	0.007234106	\$3,101.52	R
604160	\$675,750	\$63,715	\$580,000	\$1,319,465	8	S	0.0000022	\$3	N	0.001	Y	1	66	0.00014519	\$191.57	R
604161	\$666,994	\$138,050	\$580,000	\$1,385,043	7	S	0.00011	\$152	N	0.0005	Y	1	66	0.007234106	\$10,019.55	R
604162	\$382,154	\$90,493	\$0	\$472,647	7	S	0.00011	\$52	N	0.0005	Y	1	66	0.007234106	\$3,419.18	R
604167	\$316,087	\$23,270	\$0	\$339,356	7	S	0.00011	\$37	N	0.0005	Y	1	67	0.007343311	\$2,492.00	R
604168	\$253,906	\$32,319	\$0	\$286,225	8	S	0.0000022	\$1	N	0.002	Y	1	67	0.000147389	\$42.19	R
604169	\$122,817	\$7,757	\$0	\$130,573	7	O	0.00017	\$22	N	0.002	Y	1	67	0.011326337	\$1,478.91	R
604173	\$81,160	\$5,817	\$0	\$86,977	7	S	0.00011	\$10	N	0.0001	N	1	68	0.007452503	\$648.20	R
604174	\$59,309	\$3,878	\$0	\$63,187	7	O	0.00017	\$11	N	0.0001	N	1	68	0.011494411	\$726.30	R
604175	\$338,796	\$19,391	\$0	\$358,187	8</											



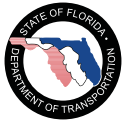
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
604178	\$154,485	\$31,026	\$0	\$185,511	7	O	0.00017	\$32	N	0.0005	Y	1	68	0.011494411	\$2,132.34	R
604179	\$294,205	\$1,264,890	\$1,160,000	\$2,719,095	8	S	0.000022	\$6	N	0.0005	Y	1	69	0.000151789	\$412.73	T
604180	\$838,506	\$108,592	\$0	\$947,099	7	S	0.00011	\$104	N	0.0001	N	1	69	0.007561683	\$7,161.66	R
604181	\$1,336,563	\$437,511	\$580,000	\$2,354,074	7	S	0.00011	\$259	N	0.0001	N	1	69	0.007561683	\$17,800.76	R
604183	\$304,662	\$27,148	\$0	\$331,810	7	S	0.00011	\$36	N	0.0005	Y	1	69	0.007561683	\$2,509.04	R
604184	\$59,653	NA	\$0	\$59,653	7	O	0.00017	\$10	N	0.0005	Y	1	70	0.011830475	\$705.72	R
604185	\$54,299	\$19,391	\$0	\$73,691	7	S	0.00011	\$8	N	0.0005	Y	1	70	0.007670851	\$565.27	R
604187	\$51,240	NA	\$0	\$51,240	7	O	0.00017	\$9	N	0.0005	Y	1	69	0.011662457	\$597.58	R
604191	\$379,188	\$825,373	\$1,160,000	\$2,364,562	8	S	0.000022	\$5	N	0.0005	Y	1	70	0.000153988	\$364.11	R
604192	\$59,653	\$46,539	\$0	\$106,192	7	O	0.00017	\$18	N	0.001	Y	1	70	0.011830475	\$1,256.30	R
604193	\$76,478	\$32,319	\$0	\$108,797	7	S	0.00011	\$12	N	0.002	Y	1	71	0.007780007	\$846.44	R
604195	\$242,309	\$32,319	\$0	\$274,628	8	S	0.000022	\$1	N	0.0001	Y	1	72	0.000158388	\$43.50	R
604196	\$417,443	\$32,319	\$0	\$449,762	7	S	0.00011	\$49	N	0.002	Y	1	72	0.007889152	\$3,548.24	R
604197	\$281,079	\$90,493	\$0	\$371,572	8	S	0.000022	\$1	N	0.002	Y	1	73	0.000160587	\$59.67	R
604316	\$118,540	\$9,696	\$0	\$128,236	7	S	0.00011	\$14	N	0.002	Y	1	44	0.004828571	\$619.20	R
604343	\$79,537	\$35,551	\$0	\$115,088	7	S	0.00011	\$13	N	0.002	Y	1	26	0.002856071	\$328.70	R
604348	\$47,416	\$23,270	\$0	\$70,686	7	S	0.00011	\$8	N	0.002	Y	1	26	0.002856071	\$201.88	R
604372	\$185,841	\$25,209	\$0	\$211,049	6	S	0.00011	\$23	N	0.002	Y	1	52	0.005703985	\$1,203.82	R
604373	\$168,251	\$29,087	\$0	\$197,338	6	S	0.00011	\$22	N	0.002	Y	1	52	0.005703985	\$1,125.61	R
604377	\$1,080,993	\$1,034,210	\$580,000	\$2,695,204	7	S	0.00011	\$296	N	0.002	Y	1	52	0.005703985	\$15,373.40	R
604382	\$128,482	\$22,623	\$0	\$151,106	6	S	0.00011	\$17	N	0.002	Y	1	51	0.0055946	\$845.38	R
610007	\$388,007	\$450,341	\$1,160,000	\$1,998,348	6	S	0.00011	\$220	N	0.002	Y	1	34	0.00373322	\$7,460.27	R
610008	\$8,372,703	\$10,049,667	\$2,900,000	\$21,322,370	4	S	0.0005	\$10,661	Y	0.002	Y	1	15	0.007473807	\$159,359.27	R
610034	\$551,622	\$1,459,875	\$1,160,000	\$3,171,497	7	S	0.00011	\$349	N	0.002	Y	1	17	0.001868355	\$5,925.48	R
610052	\$4,539,491	\$528,564	\$1,160,000	\$6,228,055	7	S	0.00011	\$685	N	0.002	Y	1	37	0.004061952	\$25,298.06	R
610083	\$4,303,767	\$437,511	\$580,000	\$5,321,278	7	S	0.00011	\$585	N	0.002	Y	1	61	0.006687905	\$35,588.20	R
610084	\$1,610,314	\$2,485,862	\$1,160,000	\$5,256,175	7	S	0.00011	\$578	N	0.002	Y	1	61	0.006687905	\$35,152.80	R
610803	\$177,693	\$103,421	\$0	\$281,114	8	S	0.000022	\$1	N	0.002	Y	1	69	0.000151789	\$42.67	R
610910	\$733,342	\$8,128,558	\$1,160,000	\$10,021,899	6	S	0.00011	\$1,102	Y	0.002	Y	1	15	0.00164873	\$16,523.41	R
614118	\$134,601	\$19,391	\$0	\$153,992	6	S	0.00011	\$17	N	0.002	Y	1	47	0.005156941	\$794.13	R
614128	\$71,015	\$38,783	\$0	\$109,798	6	S	0.00011	\$12	N	0.002	Y	1	45	0.00493804	\$542.19	R
614129	\$104,010	\$17,452	\$0	\$121,462	3	S	0.0013	\$158	N	0.002	Y	1	45	0.056857654	\$6,906.04	R
614130	\$98,328	\$23,893	\$0	\$122,222	6	S	0.00011	\$13	N	0.002	Y	1	45	0.00493804	\$603.54	R
614131	\$103,011	\$84,030	\$0	\$187,040	3	S	0.0013	\$243	N	0.002	Y	1	45	0.056857654	\$10,634.66	R
614132	\$70,359	\$19,911	\$0	\$90,270	6	S	0.00011	\$10	N	0.002	Y	1	46	0.005047497	\$455.64	R
614134	\$235,551	\$51,711	\$0	\$287,261	7	S	0.00011	\$32	N	0.002	Y	1	46	0.005047497	\$1,449.95	R
614135	\$69,595	\$26,548	\$0	\$96,143	6	S	0.00011	\$11	N	0.002	Y	1	46	0.005047497	\$485.28	R
614137	\$208,362	\$45,247	\$0	\$253,609	6	S	0.00011	\$28	N	0.002	Y	1	45	0.00493804	\$1,252.33	R
614138	\$104,774	\$25,209	\$0	\$129,983	3	S	0.0013	\$169	N	0.002	Y	1	46	0.058083739	\$7,549.90	R
614139	\$71,795	\$71,102	\$0	\$142,897	6	O	0.00017	\$24	N	0.002	Y	1	50	0.008464694	\$1,209.58	R
614140	\$119,867	\$19,911	\$0	\$139,778	3	S	0.0013	\$182	N	0.002	Y	1	50	0.062972161	\$8,802.12	R
614142	\$198,077	\$71,102	\$0	\$269,179	7	S	0.00011	\$30	N	0.002	Y	1	56	0.006141403	\$1,653.14	R
614144	\$73,356	\$46,539	\$0	\$119,896	7	O	0.00017	\$20	N	0.002	Y	1	68	0.011494411	\$1,378.13	R
700018	\$654,094	\$703,017	\$1,160,000	\$2,517,111	7	S	0.00011	\$277	Y	0.002	Y	1	33	0.003623618	\$9,121.05	R
700037	\$5,360,860	\$38,679,626	\$2,900,000	\$46,940,486	4	S	0.0005	\$23,470	Y	0.002	Y	1	15	0.007473807	\$350,824.12	T
700072	\$22,529,930	\$1,260,188	\$2,900,000	\$26,690,119	7	S	0.00011	\$2,936	N	0.002	Y	1	27	0.002965757	\$79,156.40	T
700110	\$23,423,710	\$2,058,995	\$2,900,000	\$28,382,705	5	S	0.00024	\$97	Y	0.002	Y	0.67	36	0.008603811	\$244,199.42	T
700185	\$3,369,758	\$2,360,878	\$2,900,000	\$8,630,637	7	S	0.00011	\$949	Y	0.002	Y	1	28	0.003075431	\$26,542.92	R
700186	\$2,138,251	\$28,664,407	\$2,900,000	\$33,702,658	7	S	0.00011	\$3,707	Y	0.002	Y	1	48	0.005266374	\$177,490.81	R
700190	\$3,218,551	\$2,360,878	\$2,900,000	\$8,479,430	7	S	0.00011	\$933	Y	0.002	Y	1	57	0.006250727	\$53,002.60	R
700194	\$1,408,436	\$31,943,594	\$2,900,000	\$36,252,030	8	R	0.000017	\$62	Y	0.002	Y	1	65	0.000110494	\$4,005.63	R
700196	\$8,158,566	\$91,363,322	\$2,900,000	\$102,421,888	6	S	0.00011	\$11,266	Y	0.002	Y	1	59	0.00646934	\$662,602.03	T
704004	\$1,119,632	\$4,036,559	\$1,160,000	\$6,316,191	6	S	0.00011	\$695	N	0.002	Y	1	38	0.004171505	\$26,348.02	R
704011	\$4,036,050	\$3,033,492	\$2,900,000	\$9,969,542	7	S	0.00011	\$1,097	N	0.002	Y	1	36	0.003952386	\$39,403.48	T
704013	\$224,844	\$1,187,158	\$1,160,000	\$2,572,002	7	S	0.00011	\$283	N	0.002	Y	1	41	0.004500092	\$11,574.25	T
704016	\$202,900	\$209,351	\$1,160,000	\$1,572,250	6	S	0.00011	\$173	N	0.002	Y	1	28	0.003075431	\$4,835.35	T
704017	\$125,501	NA	\$580,000	\$705,501	7	S	0.00011	\$78	Y	0.002	Y	1	43	0.00471909	\$3,329.32	T
704019	\$215,292	NA	\$580,000	\$795,292	6	S	0.00011	\$87	Y	0.0005	Y	1	41	0.004500092	\$3,578.89	R
704042	\$846,747	\$3,922,166	\$1,160,000	\$5,928,913	7	S	0.00011	\$652	N	0.002	Y	1	46	0.005047497	\$29,926.17	R
704048	\$874,285	\$37,337	\$580,000	\$1,491,622	6	O	0.00017	\$254	Y	0.002	Y	1	29	0.004918285	\$7,336.22	T
704049	\$43,926,216	\$31,426,381	\$2,900,000	\$78,252,597	4	S	0.0005	\$39,126	Y	0.002	Y	1	15	0.007473807	\$584,844.79	T
704063	\$16,991,586	\$3,887,506	\$1,160,000	\$22,039,092	7	S	0.00011	\$2,424	N	0.002	Y	1	15	0.00164873	\$36,336.51	T
704075	\$4,626,113	\$16,757,603	\$2,900,000	\$24,283,717	7	S	0.00011	\$2,671	Y	0.002	Y	1	51	0.0055946	\$135,857.69	R
704085	\$137,098	NA	\$0	\$137,098	7	S	0.00011	\$15	Y	0.002	Y	1	53	0.005813357	\$797.00	R
704086	\$185,419	NA	\$0	\$185,419	7	S	0.00011	\$20	Y	0.002	Y	1	53	0.005813357	\$1,077.91	R
704125	\$1,356,650	\$1,077,833	\$2,900,000	\$5,334,483	4	S	0.0005	\$2,667	Y	0.002	Y	1	15	0.007473807	\$39,868.90	T
704144	\$1,998,078	\$317,174	\$1,160,000	\$3,475,252	6	R	0.000077	\$268	N	0.001	Y	1	57	0.004379551	\$15,220.04	T
704154	\$1,872,733	\$5,998,198	\$1,160,000	\$9,030,931	7	R	0.000077	\$695	N	0.002	Y	1	33	0.002537872	\$22,919.35	R
704191	\$482,158	NA	\$580,000	\$1,062,158	7	S	0.00011	\$117	Y	0.002	Y	1	53	0.005813357	\$6,174.70	R
704256	\$1,019,805	\$323,507	\$1,160,000	\$2,503,312	7	R	0.000077	\$193	N	0.002	Y	1	58	0.004456213	\$11,155.29	R
705500	\$1,004,061	\$329,016	\$1,160,000	\$2,493,077	7	R	0.000077	\$192	N	0.002	Y	1	53	0.004072841	\$10,153.91	R
705601	\$202,486	\$265,983	\$1,160,000	\$1,628,469	7	S	0.00011	\$179	N	0.002	Y	1	26	0.002856071	\$4,651.02	R
705603	\$285,152	\$794,781	\$1,160,000	\$2,239,933	7	S	0.00011	\$246	N	0.002	Y	1	16	0.001758549	\$3,939.03	R
705906	\$2,057,715	\$1,782,170	\$2,900,000	\$6,739,885	7	S	0.00011	\$741	N	0.0005	Y	1	43	0.00471909	\$31,806.12	R
705907	\$471,695															



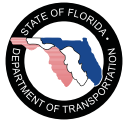
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
705912	\$1,395,700	\$2,154,882	\$2,900,000	\$6,450,583	6	S	0.00011	\$710	N	0.0005	Y	1	41	0.004500092	\$29,028.22	R
705913	\$471,695	\$350,454	\$1,160,000	\$1,982,149	7	S	0.00011	\$218	N	0.001	Y	1	41	0.004500092	\$8,919.85	R
705914	\$628,927	\$1,388,680	\$2,900,000	\$4,917,607	7	S	0.00011	\$541	N	0.0005	Y	1	41	0.004500092	\$22,129.68	R
705915	\$345,910	\$143,504	\$580,000	\$1,069,414	7	S	0.00011	\$118	N	0.002	Y	1	41	0.004500092	\$4,812.46	R
705916	\$628,927	\$1,336,643	\$2,900,000	\$4,865,570	7	S	0.00011	\$535	N	0.002	Y	1	41	0.004500092	\$21,895.51	R
705917	\$975,651	\$1,237,294	\$1,160,000	\$3,372,945	7	R	0.000077	\$260	N	0.002	Y	1	54	0.004149527	\$13,996.13	R
705918	\$1,664,558	\$994,004	\$1,160,000	\$3,818,562	6	R	0.000077	\$294	N	0.002	Y	1	59	0.004149527	\$15,845.23	R
705919	\$708,919	NA	\$580,000	\$1,288,919	6	S	0.00011	\$142	Y	0.002	Y	1	34	0.004281046	\$5,517.92	R
705953	\$4,738,176	\$2,850,120	\$2,900,000	\$10,488,296	7	S	0.00011	\$1,154	N	0.002	Y	1	38	0.004171505	\$43,751.98	R
710006	\$7,630,840	\$54,034,190	\$2,900,000	\$64,565,029	6	S	0.00011	\$7,102	Y	0.002	Y	1	39	0.004281046	\$276,405.86	M
710014	\$445,568	\$1,770,865	\$1,160,000	\$3,376,433	6	S	0.00011	\$371	N	0.002	Y	1	15	0.00164873	\$5,566.83	M
710017	\$1,221,027	\$317,692	\$1,160,000	\$2,698,719	6	S	0.00011	\$297	Y	0.002	Y	1	15	0.00164873	\$4,449.46	R
710027	\$779,744	\$885,433	\$1,160,000	\$2,825,176	6	S	0.00011	\$311	Y	0.002	Y	1	15	0.00164873	\$4,657.95	R
710033	\$1,221,027	\$317,692	\$1,160,000	\$2,698,719	6	S	0.00011	\$297	Y	0.002	Y	1	15	0.00164873	\$4,449.46	R
710045	\$2,109,658	\$4,813,220	\$2,900,000	\$9,822,877	6	S	0.00011	\$1,081	N	0.002	Y	1	25	0.002746373	\$26,977.28	R
710052	\$1,208,174	\$501,873	\$1,160,000	\$2,870,047	6	S	0.00011	\$316	N	0.002	Y	1	15	0.00164873	\$4,731.93	R
710053	\$1,005,711	\$983,978	\$1,160,000	\$3,149,689	6	S	0.00011	\$346	N	0.002	Y	1	15	0.00164873	\$5,192.99	R
710054	\$1,307,205	\$983,978	\$1,160,000	\$3,451,183	6	S	0.00011	\$380	Y	0.002	Y	1	15	0.00164873	\$5,690.07	R
710086	\$78,538	\$1,422	\$0	\$79,960	4	S	0.0005	\$40	N	0.002	Y	1	18	0.008961852	\$716.59	R
710089	\$142,061	\$0	\$0	\$142,061	2	S	0.006	\$852	N	0.002	N	1	18	0.102664356	\$14,584.60	R
710940	\$771,175	\$10,852,041	\$2,900,000	\$14,523,216	6	S	0.00011	\$1,598	N	0.002	Y	1	15	0.00164873	\$23,944.86	R
714040	\$1,665,553	\$1,142,288	\$1,160,000	\$3,967,841	7	R	0.000077	\$306	N	0.002	Y	1	59	0.00453287	\$17,985.71	M
714046	\$211,275	\$66,221	\$580,000	\$857,496	4	S	0.0005	\$429	N	0.002	Y	1	57	0.028104633	\$24,099.61	R
714052	\$169,109	NA	\$0	\$169,109	5	O	0.00032	\$3	N	0.002	Y	1	61	0.019333782	\$3,269.52	R
714053	\$172,543	\$41,798	\$0	\$214,341	6	O	0.00017	\$36	N	0.002	Y	1	61	0.010317289	\$2,211.42	R
714056	\$284,567	\$136,278	\$1,160,000	\$1,580,845	6	S	0.00011	\$174	N	0.002	Y	1	27	0.002965757	\$4,688.40	M
720005	\$24,460,384	\$2,224,617	\$2,900,000	\$29,585,000	6	S	0.00011	\$3,254	Y	0.002	Y	1	15	0.00164873	\$48,777.68	M
720007	\$573,800	\$2,691,069	\$2,900,000	\$6,164,869	7	S	0.00011	\$678	N	0.002	Y	1	15	0.00164873	\$10,164.21	R
720012	\$942,703	\$688,914	\$2,900,000	\$4,531,617	6	S	0.00011	\$498	Y	0.002	Y	1	15	0.00164873	\$7,471.41	M
720017	\$1,631,314	\$2,312,686	\$2,900,000	\$6,844,000	6	R	0.000077	\$527	Y	0.002	Y	1	15	0.001154378	\$7,900.56	M
720028	\$1,943,155	\$9,329,038	\$2,900,000	\$14,172,193	6	S	0.00011	\$1,559	N	0.002	Y	1	31	0.003404379	\$48,247.52	M
720031	\$2,136,877	\$3,544,175	\$2,900,000	\$8,581,052	7	S	0.00011	\$944	N	0.002	Y	1	15	0.00164873	\$14,147.84	T
720033	\$12,144,765	\$13,930,860	\$2,900,000	\$28,975,625	6	S	0.00011	\$3,187	N	0.002	Y	1	23	0.002526941	\$73,219.70	T
720042	\$6,109,342	\$8,809,220	\$2,900,000	\$17,818,562	6	S	0.00011	\$1,960	Y	0.002	Y	1	15	0.00164873	\$29,378.00	M
720058	\$3,118,787	\$3,068,562	\$2,900,000	\$9,087,349	6	S	0.00011	\$1,000	Y	0.002	Y	1	38	0.004171505	\$37,907.92	R
720060	\$9,805,987	\$0	\$2,900,000	\$12,705,987	6	S	0.00011	\$1,398	N	0.002	Y	1	21	0.002307461	\$29,318.57	T
720066	\$7,371,815	\$59,479,309	\$2,900,000	\$69,751,124	5	S	0.00024	\$237	Y	0.001	Y	1	15	0.003593598	\$250,682.63	M
720095	\$1,680,041	\$688,914	\$2,900,000	\$5,268,954	6	S	0.00011	\$580	Y	0.002	Y	1	32	0.003514005	\$18,515.13	M
720107	\$87,843,094	\$42,630,537	\$2,900,000	\$133,373,632	7	S	0.00011	\$14,671	Y	0.002	Y	0.67	33	0.003623618	\$483,295.15	T
720109	\$1,833,683	\$472,670	\$2,900,000	\$5,206,353	7	S	0.00011	\$573	Y	0.002	Y	1	33	0.003623618	\$18,865.84	T
720110	\$1,708,103	\$2,601,470	\$2,900,000	\$7,209,573	6	S	0.00011	\$793	Y	0.002	Y	1	33	0.003623618	\$26,124.74	M
720130	\$3,508,635	\$3,068,562	\$2,900,000	\$9,477,197	6	S	0.00011	\$1,042	Y	0.002	Y	1	38	0.004171505	\$39,534.17	R
720148	\$2,913,913	\$161,180	\$1,160,000	\$4,235,093	7	S	0.00011	\$466	Y	0.002	Y	1	27	0.002965757	\$12,560.26	R
720280	\$5,741,531	\$751,174	\$2,900,000	\$9,392,705	7	S	0.00011	\$1,033	Y	0.0005	Y	1	33	0.003623618	\$34,035.58	M
720281	\$1,427,165	\$2,601,470	\$2,900,000	\$6,928,635	6	S	0.00011	\$762	Y	0.002	Y	1	33	0.003623618	\$25,106.73	M
720288	\$3,951,487	\$29,270,770	\$2,900,000	\$36,122,257	7	S	0.00011	\$3,973	Y	0.002	Y	1	38	0.004171505	\$150,684.17	R
720292	\$4,867,720	\$15,434,681	\$2,900,000	\$23,202,401	7	S	0.00011	\$2,552	Y	0.002	Y	1	40	0.004390575	\$101,871.88	R
720359	\$1,566,511	\$5,080,435	\$2,900,000	\$9,546,946	6	S	0.00011	\$1,050	N	0.002	Y	1	35	0.003842809	\$36,687.09	R
720360	\$3,143,197	\$2,028,779	\$2,900,000	\$8,071,976	6	S	0.00011	\$888	N	0.001	Y	1	35	0.003842809	\$31,019.06	R
720401	\$3,903,416	\$6,965,430	\$2,900,000	\$13,768,846	7	S	0.00011	\$1,515	N	0.002	Y	1	41	0.004500092	\$61,961.08	R
720402	\$2,426,056	\$7,682,460	\$2,900,000	\$13,008,516	7	S	0.00011	\$1,431	N	0.002	Y	1	41	0.004500092	\$58,539.52	R
720425	\$3,563,418	\$14,352,366	\$2,900,000	\$20,815,784	7	S	0.00011	\$2,290	N	0.002	Y	1	44	0.004828571	\$100,510.49	M
720442	\$56,824,093	\$2,260,078	\$2,900,000	\$61,984,171	6	S	0.00011	\$6,818	Y	0.002	Y	1	45	0.00493804	\$306,080.31	T
720443	\$7,422,071	\$4,520,157	\$2,900,000	\$14,842,228	6	S	0.00011	\$1,633	Y	0.002	Y	1	44	0.004828571	\$71,666.75	T
720444	\$2,428,990	\$4,520,157	\$2,900,000	\$9,849,147	7	S	0.00011	\$1,083	Y	0.002	Y	1	44	0.004828571	\$47,557.31	T
720445	\$2,428,990	\$4,520,157	\$2,900,000	\$9,849,147	7	S	0.00011	\$1,083	Y	0.002	Y	1	44	0.004828571	\$47,557.31	T
720448	\$8,220,716	\$3,546,302	\$2,900,000	\$14,667,018	6	S	0.00011	\$1,613	Y	0.002	Y	1	44	0.004828571	\$70,820.74	R
720474	\$20,971,434	\$5,179,304	\$2,900,000	\$29,050,738	7	S	0.00011	\$3,196	Y	0.002	Y	0.67	50	0.005485204	\$159,349.21	T
720476	\$4,958,869	\$2,635,084	\$2,900,000	\$10,493,953	8	S	0.000022	\$23	Y	0.001	Y	1	50	0.000109994	\$1,154.27	M
720509	\$56,824,093	\$4,520,157	\$2,900,000	\$64,244,250	6	R	0.000077	\$4,947	Y	0.002	Y	1	54	0.004149527	\$266,583.24	R
720514	\$7,422,071	\$4,520,157	\$2,900,000	\$14,842,228	7	S	0.00011	\$1,633	Y	0.002	Y	1	54	0.005922718	\$87,906.33	T
720910	\$1,162,771	\$13,380,433	\$2,900,000	\$17,443,205	6	S	0.00011	\$1,919	Y	0.002	Y	1	15	0.00164873	\$28,759.14	M
724001	\$869,035	\$757,476	\$1,160,000	\$2,786,811	6	O	0.00017	\$474	N	0.002	Y	1	31	0.005256584	\$14,649.10	R
724007	\$193,457	NA	\$0	\$193,457	6	S	0.00011	\$21	Y	0.002	Y	1	33	0.003623618	\$701.01	R
724011	\$1,623,447	\$1,512,308	\$2,900,000	\$6,035,756	6	S	0.00011	\$664	N	0.002	Y	1	37	0.004061952	\$24,516.95	R
724027	\$440,292	\$3,175,355	\$2,900,000	\$6,515,647	6	O	0.00017	\$1,108	N	0.002	Y	1	26	0.00441062	\$28,738.04	R
724029	\$414,150	\$154,535	\$1,160,000	\$1,728,684	7	S	0.00011	\$190	N	0.002	Y	1	32	0.003514005	\$6,074.60	R
724031	\$482,511	\$1,357,506	\$1,160,000	\$3,000,017	3	S	0.0013	\$3,900	N	0.002	Y	1	31	0.039523936	\$118,572.48	R
724039	\$715,955	\$2,175,777	\$2,900,000	\$5,791,733	6	S	0.00011	\$637	N	0.002	Y	1	40	0.004390575	\$25,429.04	R
724041	\$334,176	\$885,433	\$1,160,000	\$2,379,609	3	O	0.0016	\$3,807	N	0.002	Y	1	25	0.039241338	\$93,379.04	R
724049	\$295,047	NA	\$0	\$295,047	3	S	0.0013	\$384	Y	0.002	Y					



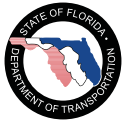
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
724080	\$497,760	\$1,346,383	\$2,900,000	\$4,744,143	6	S	0.00011	\$522	N	0.002	Y	1	15	0.00164873	\$7,821.81	R
724081	\$170,436	\$985,748	\$1,160,000	\$2,316,184	5	S	0.00024	\$8	N	0.002	Y	1	31	0.007413278	\$17,170.52	R
724085	\$104,024	\$53,126	\$580,000	\$737,150	6	O	0.00017	\$125	N	0.002	Y	1	15	0.002546968	\$1,877.50	R
724088	\$1,589,610	\$1,975,109	\$2,900,000	\$6,464,719	7	S	0.00011	\$711	N	0.002	Y	1	36	0.003952386	\$25,551.07	M
724095	\$213,953	NA	\$580,000	\$793,953	5	O	0.00032	\$13	Y	0.002	Y	1	48	0.015245058	\$12,103.86	R
724115	\$1,149,622	\$326,317	\$1,160,000	\$2,635,939	6	S	0.00011	\$290	N	0.002	Y	1	33	0.003623618	\$9,551.64	R
724116	\$552,199	\$293,338	\$1,160,000	\$2,005,538	6	S	0.00011	\$221	N	0.0005	Y	1	39	0.004281046	\$8,585.80	M
724117	\$662,639	\$277,329	\$1,160,000	\$2,099,968	4	S	0.0005	\$1,050	N	0.002	Y	1	38	0.0188253	\$39,532.53	M
724118	\$721,191	\$1,869,607	\$1,160,000	\$3,750,799	6	S	0.00011	\$413	N	0.0005	Y	1	36	0.003952386	\$14,824.61	R
724126	\$891,136	\$2,170,009	\$2,900,000	\$5,961,144	6	O	0.00017	\$1,013	N	0.0005	Y	1	28	0.004749092	\$28,310.02	M
724129	\$264,667	\$1,186,675	\$1,160,000	\$2,611,342	6	O	0.00017	\$444	N	0.0005	Y	1	17	0.002886073	\$7,536.52	R
724130	\$264,667	\$1,186,675	\$1,160,000	\$2,611,342	6	O	0.00017	\$444	N	0.0005	Y	1	17	0.002886073	\$7,536.52	R
724131	\$220,556	NA	\$1,160,000	\$1,380,556	6	O	0.00017	\$235	Y	0.0005	Y	1	17	0.002886073	\$3,984.39	M
724132	\$220,556	NA	\$1,160,000	\$1,380,556	7	S	0.00011	\$152	Y	0.002	Y	1	17	0.001868355	\$2,579.37	R
724147	\$5,114,821	\$1,770,244	\$2,900,000	\$9,785,064	4	S	0.0005	\$4,893	N	0.002	Y	1	30	0.014891756	\$145,716.78	M
724150	\$2,070,350	\$1,230,341	\$1,160,000	\$4,460,691	6	S	0.00011	\$491	N	0.002	Y	1	40	0.004390575	\$19,585.00	M
724174	\$690,639	\$2,722,105	\$2,900,000	\$6,312,745	6	S	0.00011	\$694	N	0.002	Y	1	42	0.004609597	\$29,099.21	M
724179	\$84,188	NA	\$0	\$84,188	3	S	0.0013	\$109	Y	0.0005	N	1	21	0.026948005	\$2,268.70	R
724183	\$99,557	\$283,158	\$1,160,000	\$1,542,715	5	O	0.00032	\$26	N	0.0005	Y	1	15	0.004789263	\$7,388.47	R
724185	\$492,695	\$831,734	\$1,160,000	\$2,484,429	6	S	0.00011	\$273	N	0.0005	Y	1	41	0.004500092	\$11,180.16	M
724190	\$2,647,841	\$628,743	\$1,160,000	\$4,436,584	6	O	0.00017	\$754	N	0.0001	N	1	21	0.003563938	\$15,811.71	T
724211	\$584,351	\$356,491	\$1,160,000	\$2,100,842	6	S	0.00011	\$231	N	0.002	Y	1	24	0.002636663	\$5,539.21	R
724214	\$10,284,206	\$6,110,149	\$2,900,000	\$19,294,355	6	S	0.00011	\$2,122	N	0.0001	N	1	23	0.002526941	\$48,755.20	T
724219	\$662,639	\$2,065,250	\$2,900,000	\$5,627,889	6	S	0.00011	\$619	N	0.002	Y	1	31	0.003404379	\$19,159.47	R
724222	\$251,552	\$39,339	\$580,000	\$870,891	7	S	0.00011	\$96	N	0.002	Y	1	70	0.007670851	\$6,680.48	T
724236	\$209,352	\$138,344	\$580,000	\$927,696	6	O	0.00017	\$158	N	0.002	Y	1	50	0.008464694	\$7,852.66	R
724237	\$315,178	\$138,344	\$580,000	\$1,033,522	6	O	0.00017	\$176	N	0.002	Y	1	50	0.008464694	\$8,748.45	R
724238	\$212,803	\$442,700	\$580,000	\$1,235,503	6	O	0.00017	\$210	N	0.002	Y	1	50	0.008464694	\$10,458.15	R
724252	\$1,446,269	\$1,775,209	\$2,900,000	\$6,121,478	6	S	0.00011	\$673	N	0.002	Y	1	26	0.002856071	\$17,483.38	R
724253	\$942,547	\$767,027	\$1,160,000	\$2,869,574	5	S	0.00024	\$10	N	0.002	Y	1	34	0.008127769	\$23,323.23	M
724258	\$568,338	\$1,923,570	\$2,900,000	\$5,391,908	6	S	0.00011	\$593	N	0.002	Y	1	15	0.00164873	\$8,889.80	R
724264	\$137,004	NA	\$1,160,000	\$1,297,004	6	O	0.00017	\$220	Y	0.002	Y	1	36	0.006101828	\$7,914.10	R
724268	\$474,844	\$396,362	\$1,160,000	\$2,031,205	6	S	0.00011	\$223	Y	0.002	Y	1	23	0.002526941	\$5,132.74	R
724274	\$223,773	\$137,565	\$580,000	\$941,338	6	O	0.00017	\$160	N	0.002	Y	1	45	0.007621459	\$7,174.37	R
724275	\$1,043,466	\$836,774	\$2,900,000	\$4,780,241	6	R	0.00077	\$368	N	0.002	Y	1	44	0.003382397	\$16,168.67	R
724277	\$227,958	\$560,882	\$1,160,000	\$1,948,840	6	S	0.00011	\$214	N	0.002	Y	1	45	0.00493804	\$9,623.45	R
724278	\$399,869	\$1,086,307	\$1,160,000	\$2,646,176	6	R	0.00077	\$204	N	0.002	Y	1	16	0.001231289	\$3,258.21	M
724279	\$291,590	\$224,526	\$1,160,000	\$1,676,116	6	S	0.00011	\$184	N	0.002	Y	1	45	0.00493804	\$8,276.73	T
724288	\$346,553	\$2,588,971	\$2,900,000	\$5,835,524	6	S	0.00011	\$642	N	0.002	Y	1	46	0.005047497	\$29,454.79	R
724290	\$512,571	\$1,159,825	\$1,160,000	\$2,832,397	7	S	0.00011	\$312	N	0.002	Y	1	46	0.005047497	\$14,296.51	R
724291	\$190,604	\$148,472	\$580,000	\$919,076	5	O	0.00032	\$16	N	0.002	Y	1	31	0.009872531	\$9,073.61	R
724292	\$1,070,811	\$3,810,602	\$2,900,000	\$7,781,413	6	S	0.00011	\$856	N	0.001	Y	1	48	0.005266374	\$40,979.83	R
724293	\$1,070,811	\$3,810,602	\$2,900,000	\$7,781,413	7	S	0.00011	\$856	N	0.002	Y	1	48	0.005266374	\$40,979.83	R
724295	\$326,956	NA	\$580,000	\$906,956	6	S	0.00011	\$100	Y	0.002	Y	1	22	0.002417207	\$2,192.30	M
724297	\$1,349,182	\$216,564	\$1,160,000	\$2,725,745	7	S	0.00011	\$300	N	0.002	Y	1	61	0.006687905	\$18,229.52	R
724301	\$264,925	NA	\$1,160,000	\$1,424,925	6	R	0.00077	\$110	Y	0.0005	Y	1	47	0.003612598	\$5,147.68	T
724304	\$17,812,597	\$545,511	\$1,160,000	\$19,518,107	3	S	0.0013	\$25,374	N	0.002	Y	1	27	0.034513186	\$673,632.07	T
724305	\$1,043,466	\$3,307,652	\$2,900,000	\$7,251,118	6	R	0.00077	\$558	N	0.002	Y	1	49	0.003766036	\$27,307.97	T
724307	\$696,914	\$3,080,777	\$2,900,000	\$6,677,691	6	R	0.00077	\$514	N	0.002	Y	1	25	0.001923222	\$12,842.68	R
724308	\$2,166,719	\$2,381,571	\$2,900,000	\$7,448,290	7	S	0.00011	\$819	N	0.002	Y	1	18	0.00197815	\$14,733.83	T
724312	\$6,594,740	\$609,958	\$1,160,000	\$8,364,698	4	S	0.0005	\$4,182	N	0.002	Y	1	27	0.013412615	\$112,192.47	T
724316	\$485,742	\$3,335,417	\$2,900,000	\$6,721,159	6	S	0.00011	\$739	N	0.002	Y	1	23	0.002526941	\$16,983.97	R
724317	\$526,970	\$496,342	\$1,160,000	\$2,183,312	6	S	0.00011	\$240	N	0.002	Y	1	21	0.002307461	\$5,037.91	R
724318	\$748,325	\$3,540,282	\$2,900,000	\$7,188,608	6	R	0.00077	\$554	N	0.002	Y	1	22	0.001692631	\$12,167.66	R
724320	\$522,685	\$1,158,940	\$1,160,000	\$2,841,626	5	S	0.00024	\$10	N	0.002	Y	1	21	0.005027922	\$14,287.47	T
724321	\$561,244	\$1,847,629	\$1,160,000	\$3,568,873	7	S	0.00011	\$393	N	0.002	Y	1	53	0.005813357	\$20,747.13	T
724322	\$724,293	\$727,665	\$1,160,000	\$2,611,958	6	R	0.00077	\$201	N	0.002	Y	1	52	0.003996148	\$10,437.77	T
724323	\$1,606,217	\$2,360,256	\$2,900,000	\$6,866,473	6	S	0.00011	\$755	N	0.002	Y	1	21	0.002307461	\$15,844.12	R
724326	\$1,043,466	\$2,048,997	\$2,900,000	\$5,992,464	7	S	0.00011	\$659	N	0.002	Y	1	24	0.002636663	\$15,800.11	R
724328	\$748,325	\$9,632,196	\$2,900,000	\$13,280,522	6	R	0.00077	\$1,023	N	0.002	Y	1	23	0.001769501	\$23,499.89	R
724329	\$696,914	\$3,472,014	\$2,900,000	\$7,068,927	6	R	0.00077	\$544	N	0.002	Y	1	32	0.002461061	\$17,397.06	R
724330	\$547,829	\$1,874,432	\$2,900,000	\$5,322,261	6	S	0.00011	\$585	N	0.002	Y	1	52	0.005703985	\$30,358.10	M
724332	\$410,966	\$318,945	\$1,160,000	\$1,889,910	6	S	0.00011	\$208	N	0.002	Y	1	26	0.002856071	\$5,397.72	R
724337	\$547,829	\$1,874,432	\$2,900,000	\$5,322,261	6	S	0.00011	\$585	N	0.002	Y	1	52	0.005703985	\$30,358.10	M
724338	\$1,468,370	\$277,916	\$1,160,000	\$2,906,285	6	S	0.00011	\$320	N	0.0005	Y	1	26	0.002856071	\$8,300.56	M
724339	\$384,823	NA	\$2,900,000	\$3,284,823	6	S	0.00011	\$361	Y	0.002	Y	1	52	0.005703985	\$18,736.58	M
724340	\$417,006	\$532,993	\$1,160,000	\$2,109,999	5	R	0.00018	\$6	N	0.001	Y	1	57	0.01020846	\$21,539.84	M
724341	\$411,579	\$141,083	\$580,000	\$1,132,662	6	S	0.00011	\$125	N	0.002	Y	1	55	0.006032066	\$6,832.29	R
724342	\$1,668,023	\$1,972,608	\$2,900,000	\$6,540,631	5	S	0.00024	\$22	N	0.002	Y	1	21	0.005027922	\$32,885.78	M
724348	\$6,659,379	\$1,336,853	\$1,160,000	\$9,156,232	6	S	0.00011	\$1,007	N	0.002	Y	1	54	0.005922718	\$54,229.78	R
724356	\$195,943	\$15,011	\$580,000	\$790,955	7	S	0.00011	\$87	Y	0.002	Y	1	56	0.006141003	\$4,857.57	T
724357	\$421,004	NA	\$580,000	\$1,001,004	6	S	0.00011	\$110	Y	0.001	Y	1	55	0.006		



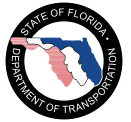
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
726601	\$123,699	NA	\$580,000	\$703,699	4	F	0.0007	\$493	Y	0.002	Y	1	26	0.018041638	\$12,695.88	M
730007	\$875,590	\$808,204	\$2,900,000	\$4,583,794	7	O	0.00017	\$779	Y	0.002	Y	1	15	0.002546968	\$11,674.78	R
730008	\$2,091,428	\$808,204	\$2,900,000	\$5,799,631	6	S	0.00011	\$638	Y	0.002	Y	1	15	0.00164873	\$9,562.03	R
730043	\$784,504	\$808,204	\$2,900,000	\$4,492,708	6	S	0.00011	\$494	Y	0.001	Y	1	23	0.002526941	\$11,352.81	R
730044	\$784,504	\$808,204	\$2,900,000	\$4,492,708	6	O	0.00017	\$764	Y	0.002	Y	1	23	0.003902697	\$17,533.68	R
730045	\$2,157,386	\$808,204	\$2,900,000	\$5,865,589	6	S	0.00011	\$645	Y	0.001	Y	1	23	0.002526941	\$14,822.00	R
734003	\$235,871	\$231,956	\$1,160,000	\$1,627,827	6	O	0.00017	\$277	N	0.0005	Y	1	15	0.002546968	\$4,146.02	R
734004	\$350,002	\$250,772	\$1,160,000	\$1,760,774	6	O	0.00017	\$299	N	0.0005	Y	1	15	0.002546968	\$4,484.63	R
734005	\$235,871	\$2,081,438	\$1,160,000	\$3,477,309	6	S	0.00011	\$383	N	0.0005	Y	1	15	0.00164873	\$5,733.14	R
734007	\$138,479	\$2,081,438	\$1,160,000	\$3,379,917	7	O	0.00011	\$372	N	0.001	Y	1	15	0.00164873	\$5,572.57	R
734008	\$1,509,574	\$4,086,310	\$1,160,000	\$6,755,884	5	O	0.00032	\$115	N	0.001	Y	1	15	0.004789263	\$32,355.70	R
734009	\$835,440	\$2,954,668	\$1,160,000	\$4,950,107	5	S	0.00024	\$17	N	0.002	Y	1	19	0.004550164	\$22,523.80	R
734011	\$1,445,075	\$885,259	\$1,160,000	\$3,490,334	6	R	0.000077	\$269	N	0.0005	Y	1	32	0.002461061	\$8,589.93	R
734012	\$784,598	\$265,578	\$1,160,000	\$2,210,175	6	R	0.000077	\$170	N	0.002	Y	1	32	0.002461061	\$5,439.38	R
734013	\$585,444	\$307,219	\$1,160,000	\$2,052,663	7	R	0.000077	\$158	N	0.002	Y	1	32	0.002461061	\$5,051.73	R
734046	\$86,591	\$16,712	\$0	\$103,303	6	O	0.00017	\$18	N	0.002	Y	1	46	0.007790163	\$804.75	R
734047	\$86,591	\$16,712	\$0	\$103,303	7	S	0.00011	\$11	N	0.002	Y	1	46	0.005047497	\$521.42	R
734048	\$95,250	\$574,654	\$580,000	\$1,249,904	7	S	0.00011	\$137	N	0.002	Y	1	47	0.005156941	\$6,445.68	R
734049	\$95,250	\$779,887	\$580,000	\$1,455,138	7	S	0.00011	\$160	N	0.002	Y	1	47	0.005156941	\$7,504.06	R
734052	\$107,506	\$16,712	\$0	\$124,217	6	O	0.00017	\$21	N	0.002	Y	1	50	0.008464694	\$1,051.46	R
734054	\$758,221	\$177,398	\$1,160,000	\$2,095,619	6	O	0.00017	\$356	N	0.002	Y	1	46	0.007790163	\$16,325.21	R
734055	\$292,275	\$308,366	\$580,000	\$1,180,641	7	O	0.00017	\$201	N	0.002	Y	1	46	0.007790163	\$9,197.39	R
734056	\$172,730	\$32,544	\$0	\$205,274	7	R	0.000077	\$16	N	0.002	Y	1	54	0.004149527	\$851.79	R
734057	\$172,730	\$11,033	\$0	\$183,763	7	R	0.000077	\$14	N	0.002	Y	1	54	0.004149527	\$762.53	R
734058	\$172,730	\$23,748	\$0	\$196,479	7	S	0.00011	\$22	N	0.002	Y	1	54	0.005922718	\$1,163.69	R
734059	\$133,914	\$48,552	\$580,000	\$762,466	7	S	0.00011	\$84	N	0.002	Y	1	55	0.006032066	\$4,599.25	R
734060	\$674,205	\$614,821	\$1,160,000	\$2,449,025	6	S	0.00011	\$269	N	0.002	Y	1	36	0.003952386	\$9,679.49	T
734061	\$1,546,213	\$3,140,424	\$1,160,000	\$5,846,637	6	S	0.00011	\$643	N	0.0001	N	1	41	0.004500092	\$26,310.41	T
734062	\$1,535,069	\$1,083,193	\$1,160,000	\$3,778,262	5	O	0.00024	\$13	N	0.0001	N	1	40	0.009555208	\$3,102.08	T
734063	\$1,001,092	\$111,578	\$580,000	\$1,692,670	6	O	0.00017	\$288	N	0.0002	Y	1	40	0.006777506	\$11,472.08	T
734064	\$992,679	\$144,158	\$580,000	\$1,716,837	7	S	0.00011	\$189	N	0.0001	N	1	40	0.004390575	\$7,537.90	T
734065	\$314,182	\$299,816	\$1,160,000	\$1,773,998	7	S	0.00011	\$195	N	0.0002	Y	1	42	0.004609597	\$8,177.42	R
734066	\$283,240	\$267,673	\$1,160,000	\$1,710,913	7	S	0.00011	\$188	N	0.0002	Y	1	42	0.004609597	\$7,886.62	R
734067	\$1,071,076	\$1,188,214	\$1,160,000	\$3,419,290	7	S	0.00011	\$376	N	0.0005	Y	1	44	0.004828571	\$16,510.28	T
734068	\$859,670	\$1,361,742	\$2,900,000	\$5,121,412	7	S	0.00011	\$563	N	0.0005	Y	1	51	0.0055946	\$28,652.25	T
734069	\$190,003	\$45,386	\$580,000	\$815,389	6	R	0.000077	\$63	N	0.0001	Y	1	55	0.004226207	\$3,446.00	R
734070	\$190,003	\$44,682	\$580,000	\$814,685	6	R	0.000077	\$63	N	0.002	Y	1	55	0.004226207	\$3,443.03	R
734071	\$39,551,085	\$13,335,564	\$2,900,000	\$55,786,649	7	R	0.000077	\$4,296	N	0.0005	Y	1	54	0.004149527	\$231,488.20	T
734072	\$190,003	\$45,034	\$580,000	\$815,037	6	R	0.000077	\$63	N	0.002	Y	1	56	0.004302882	\$3,507.01	R
734073	\$998,891	\$1,203,464	\$2,900,000	\$5,102,355	7	R	0.000077	\$393	N	0.002	Y	1	48	0.00368932	\$18,824.22	T
734079	\$444,819	\$1,188,478	\$1,160,000	\$2,793,296	7	S	0.00011	\$307	N	0.002	Y	1	49	0.005375959	\$15,016.19	T
734090	\$54,861	\$286,588	\$1,160,000	\$1,501,449	3	O	0.0016	\$2,402	N	0.002	Y	1	26	0.040778552	\$61,226.92	T
735002	\$333,892	\$0	\$580,000	\$913,892	7	N	NA	NA	Y	0.0005	N	1	46	NA	NA	R
735503	\$254,678	\$7,494,542	\$1,160,000	\$8,909,220	7	O	0.00017	\$1,515	Y	0.002	Y	1	36	0.006101828	\$54,362.53	R
740011	\$691,232	\$1,516,094	\$2,900,000	\$5,107,327	7	S	0.00011	\$562	Y	0.0005	Y	1	15	0.00164873	\$8,420.60	R
740014	\$695,228	\$1,373,872	\$2,900,000	\$4,969,100	6	S	0.00011	\$547	Y	0.0005	Y	1	15	0.00164873	\$8,192.70	R
740019	\$503,956	\$12,318,064	\$1,160,000	\$13,982,020	6	S	0.00011	\$1,538	Y	0.0001	N	1	15	0.00164873	\$23,052.58	R
740021	\$671,941	\$11,894,338	\$2,900,000	\$15,466,279	5	S	0.00024	\$53	Y	0.002	Y	1	15	0.003593958	\$55,585.16	R
740023	\$267,016	\$11,894,338	\$2,900,000	\$15,061,354	5	S	0.00024	\$51	Y	0.002	Y	1	15	0.003593958	\$54,129.88	R
740024	\$401,991	\$11,894,338	\$2,900,000	\$15,196,329	4	S	0.0005	\$7,598	Y	0.0002	N	1	15	0.007473807	\$113,574.43	R
740069	\$779,744	\$4,849,784	\$1,160,000	\$6,789,528	4	S	0.0005	\$3,395	N	0.002	Y	1	24	0.011931252	\$81,007.57	T
740095	\$727,461	\$153,046	\$580,000	\$1,460,507	6	S	0.00011	\$161	N	0.0005	Y	1	15	0.00164873	\$2,407.98	R
740920	\$402,725	\$12,318,064	\$1,160,000	\$13,880,789	6	S	0.00011	\$1,527	Y	0.002	Y	1	15	0.00164873	\$22,885.67	R
744001	\$484,868	\$152,029	\$0	\$636,897	5	S	0.00024	\$2	N	0.002	Y	1	44	0.010505693	\$6,691.04	R
744006	\$139,002	NA	\$0	\$139,002	5	O	0.00032	\$2	Y	0.002	Y	1	15	0.004789263	\$665.72	R
744007	\$413,673	\$556,007	\$580,000	\$1,549,680	6	S	0.00011	\$170	N	0.002	Y	1	15	0.00164873	\$2,555.00	T
744010	\$293,237	\$9,733	\$580,000	\$912,970	6	S	0.00011	\$100	N	0.002	Y	1	15	0.00164873	\$1,505.24	R
744306	\$649,310	\$138,344	\$580,000	\$1,367,654	4	S	0.0005	\$684	N	0.0002	N	1	15	0.007473807	\$10,221.58	T
750004	\$2,146,804	\$9,150,883	\$2,900,000	\$14,197,687	7	S	0.00011	\$1,562	Y	0.0005	Y	1	15	0.00164873	\$23,408.15	R
750013	\$3,428,194	\$2,762,830	\$2,900,000	\$9,091,024	6	S	0.00011	\$1,000	Y	0.002	Y	1	30	0.003294742	\$29,952.58	R
750057	\$2,207,767	\$1,633,200	\$2,900,000	\$6,740,967	5	S	0.00024	\$23	Y	0.0005	Y	1	33	0.007889662	\$53,183.95	R
750085	\$634,077	\$17,639,635	\$2,900,000	\$21,173,712	7	S	0.00011	\$2,329	Y	0.0002	Y	1	37	0.004061952	\$86,006.60	R
750121	\$31,998,221	\$8,614,422	\$2,900,000	\$43,512,643	7	S	0.00011	\$4,786	Y	0.0002	Y	1	39	0.004281046	\$186,279.63	R
750133	\$3,799,781	\$3,579,806	\$2,900,000	\$10,279,587	6	S	0.00011	\$1,131	Y	0.0005	Y	1	38	0.004171505	\$42,881.35	R
750169	\$3,221,236	\$2,762,830	\$2,900,000	\$8,884,066	6	S	0.00011	\$977	Y	0.002	Y	1	15	0.00164873	\$14,647.43	R
750183	\$56,703,696	\$8,877,745	\$2,900,000	\$68,481,441	7	R	0.000077	\$5,273	Y	0.0005	Y	1	39	0.002998611	\$205,349.19	R
750212	\$2,207,767	\$0	\$2,900,000	\$5,107,767	6	S	0.00011	\$562	Y	0.002	Y	1	33	0.003623618	\$18,508.60	R
750227	\$3,799,781	\$3,579,806	\$2,900,000	\$10,279,587	6	S	0.00011	\$1,131	Y	0.0005	Y	1	38	0.004171505	\$42,881.35	R
750247	\$32,102,230	\$4,307,211	\$2,900,000	\$39,309,442	7	S	0.00011	\$4,324	Y	0.0005	Y	1	39	0.004281046	\$168,285.53	R
750357	\$10,219,621	\$2,370,326	\$2,900,000	\$15,489,947	7	R	0.000077	\$1,193	Y	0.0005	Y	1	55	0.004226207	\$65,463.73	R
750358	\$10,219,621	\$2,370,326	\$2,900,000	\$15,489,947	7	S	0.00011	\$1,704	Y	0.002	Y	1	55	0.006032066	\$93,436.39	R
750393	\$18,525,711	\$5,071,395	\$2,900,000	\$26,497,106	7	R	0.000077	\$2,040	Y	0.0002	Y	1	56	0.004302882	\$11	



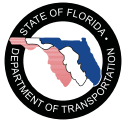
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
754004	\$1,336,703	\$24,866,741	\$2,900,000	\$29,103,444	6	S	0.00011	\$3,201	N	0.0005	Y	1	22	0.002417207	\$70,349.05	R
754005	\$1,225,311	\$886,577	\$1,160,000	\$3,271,888	6	S	0.00011	\$360	N	0.0005	Y	1	15	0.00164873	\$5,394.46	R
754006	\$248,410	\$91,124	\$580,000	\$919,534	6	O	0.00017	\$156	N	0.002	Y	1	27	0.00457987	\$4,211.35	R
754009	\$298,387	NA	\$0	\$298,387	7	O	0.00017	\$51	Y	0.002	Y	1	27	0.00457987	\$1,366.57	R
754016	\$248,410	\$90,420	\$580,000	\$918,830	6	O	0.00017	\$156	N	0.0005	Y	1	27	0.00457987	\$4,208.12	R
754017	\$248,410	\$90,420	\$580,000	\$918,830	7	O	0.00017	\$156	N	0.0005	Y	1	27	0.00457987	\$4,208.12	R
754019	\$913,985	\$625,376	\$1,160,000	\$2,699,361	7	R	0.000077	\$208	N	0.002	Y	1	41	0.003152143	\$8,508.77	R
754024	\$839,724	\$1,291,651	\$1,160,000	\$3,291,375	7	S	0.00011	\$362	N	0.002	Y	1	34	0.00373322	\$12,287.43	R
754027	\$338,741	\$611,127	\$1,160,000	\$2,109,868	7	O	0.00017	\$359	N	0.002	Y	1	28	0.004749092	\$10,019.96	R
754032	\$165,660	\$8,796	\$0	\$174,456	5	O	0.00032	\$3	N	0.002	Y	1	32	0.010189372	\$1,777.60	R
754033	\$122,146	\$8,796	\$0	\$130,941	6	O	0.00017	\$22	N	0.0005	Y	1	32	0.00542569	\$770.45	R
754051	\$246,848	NA	\$580,000	\$826,848	7	O	0.00017	\$141	Y	0.0002	Y	1	27	0.00457987	\$3,786.86	R
754057	\$517,834	\$592,714	\$580,000	\$1,690,549	4	S	0.0005	\$845	N	0.0001	N	1	31	0.01538431	\$26,007.93	R
754059	\$246,848	\$94,290	\$580,000	\$921,138	7	S	0.00011	\$101	N	0.0001	N	1	27	0.002965757	\$2,731.87	R
754064	\$474,692	\$1,436,087	\$2,900,000	\$4,810,778	7	O	0.00017	\$818	N	0.0002	Y	1	45	0.007621459	\$36,665.15	R
754067	\$1,464,624	\$622,900	\$2,900,000	\$4,987,523	7	S	0.00011	\$549	N	0.0002	Y	1	38	0.004171505	\$20,805.48	R
754068	\$422,344	\$8,774,837	\$2,900,000	\$12,097,180	7	S	0.00011	\$1,331	N	0.0002	Y	1	47	0.005156941	\$62,384.45	R
754069	\$3,336,046	\$659,355	\$2,900,000	\$6,895,401	7	R	0.000077	\$531	N	0.0001	Y	1	53	0.004072841	\$28,083.87	R
754072	\$1,553,775	\$3,608,408	\$2,900,000	\$8,062,183	6	S	0.00011	\$887	N	0.0001	N	1	50	0.005485204	\$44,222.71	R
754073	\$1,620,607	\$6,383,343	\$2,900,000	\$10,903,950	7	S	0.00011	\$1,199	N	0.0002	Y	1	49	0.005375795	\$58,617.40	R
754074	\$676,780	\$5,424,496	\$1,160,000	\$7,261,276	7	S	0.00011	\$799	N	0.0001	N	1	51	0.0055946	\$40,623.94	R
754076	\$319,216	\$547,797	\$1,160,000	\$2,027,013	7	S	0.00011	\$223	N	0.0001	N	1	53	0.005813357	\$11,783.75	R
754077	\$936,554	NA	\$1,160,000	\$2,096,554	7	S	0.00011	\$231	Y	0.0001	N	1	54	0.005927218	\$12,417.30	R
754078	\$551,154	\$945,980	\$1,160,000	\$2,657,133	7	R	0.000077	\$205	N	0.0001	Y	1	54	0.004149527	\$11,025.84	R
754079	\$4,369,711	\$4,321,270	\$2,900,000	\$11,590,980	7	S	0.00011	\$1,275	Y	0.0001	N	1	53	0.005813357	\$67,382.51	R
754080	\$4,126,949	\$2,104,482	\$2,900,000	\$9,131,431	7	S	0.00011	\$1,004	N	0.0001	N	1	53	0.005813357	\$53,084.27	R
754082	\$2,993,301	\$4,941,744	\$2,900,000	\$10,835,045	7	S	0.00011	\$1,192	N	0.0001	N	1	55	0.006032066	\$65,357.71	R
754083	\$2,448,937	\$2,014,005	\$2,900,000	\$7,362,942	7	R	0.000077	\$567	Y	0.0001	Y	1	55	0.004226207	\$31,117.32	R
754084	\$831,077	\$2,180,994	\$2,900,000	\$5,912,071	7	R	0.000077	\$455	Y	0.0001	Y	1	55	0.004226207	\$24,985.64	R
754085	\$3,336,046	\$1,423,813	\$2,900,000	\$7,659,858	7	R	0.000077	\$590	N	0.0001	Y	1	55	0.004226207	\$32,372.15	R
754092	\$831,077	\$1,138,712	\$2,900,000	\$4,869,789	7	R	0.000077	\$375	Y	0.0001	Y	1	55	0.004226207	\$20,580.74	R
754093	\$2,448,937	\$1,162,966	\$2,900,000	\$6,511,904	7	R	0.000077	\$501	Y	0.0005	Y	1	55	0.004226207	\$27,520.66	R
754099	\$537,778	\$20,952,653	\$2,900,000	\$24,390,431	7	S	0.00011	\$2,683	N	0.0005	Y	1	51	0.0055946	\$136,454.71	R
754108	\$1,428,102	\$5,248,383	\$2,900,000	\$9,576,485	7	R	0.000077	\$737	N	0.0002	Y	1	63	0.004839439	\$46,344.81	R
754110	\$1,492,842	\$639,522	\$2,900,000	\$5,032,365	7	S	0.00011	\$554	N	0.0002	Y	1	64	0.007015662	\$35,305.37	R
754113	\$1,313,105	\$560,727	\$1,160,000	\$3,033,832	7	R	0.000077	\$234	N	0.0002	Y	1	65	0.004992688	\$15,146.98	R
754123	\$2,056,467	\$4,387,130	\$1,160,000	\$7,603,597	7	S	0.00011	\$836	N	0.0001	N	1	69	0.007561683	\$57,495.99	R
754131	\$4,073,602	\$514,489	\$2,900,000	\$7,488,091	7	S	0.00011	\$824	N	0.0001	N	1	69	0.007561683	\$56,622.57	R
754138	\$2,262,113	\$176,002	\$1,160,000	\$3,598,116	7	S	0.00011	\$396	N	0.0001	N	1	57	0.006250727	\$22,490.84	R
754139	\$2,262,113	\$176,002	\$1,160,000	\$3,598,116	7	S	0.00011	\$396	N	0.0001	N	1	57	0.006250727	\$22,490.84	R
754141	\$8,929,579	NA	\$580,000	\$9,509,579	7	S	0.00011	\$1,046	Y	0.0001	N	1	70	0.007670851	\$72,946.57	R
754311	\$3,824,660	\$486,339	\$2,900,000	\$7,210,999	7	S	0.00011	\$793	N	0.0001	N	1	47	0.005156941	\$37,186.70	R
754314	\$2,499,998	\$726,430	\$1,160,000	\$4,386,427	7	S	0.00011	\$483	N	0.0001	N	1	49	0.005375795	\$23,580.53	R
754321	\$1,054,080	\$1,889,502	\$1,160,000	\$4,103,582	7	S	0.00011	\$451	N	0.0001	N	1	48	0.005266374	\$21,611.00	R
755100	\$797,162	\$1,554,643	\$1,160,000	\$3,511,805	6	S	0.00011	\$386	N	0.0001	N	1	15	0.00164873	\$5,790.02	R
755400	\$171,138	NA	\$1,160,000	\$1,331,138	7	S	0.00011	\$146	Y	0.0001	N	1	31	0.003404379	\$4,531.70	R
755800	\$2,386,850	\$8,408,226	\$2,900,000	\$13,695,076	6	O	0.00017	\$2,328	N	0.002	Y	1	26	0.00441062	\$60,403.78	R
755801	\$2,532,501	\$3,961,642	\$2,900,000	\$9,394,142	7	S	0.00011	\$1,033	N	0.002	Y	1	39	0.004281046	\$40,216.75	R
755803	\$473,849	\$584,739	\$1,160,000	\$2,218,588	7	S	0.00011	\$244	N	0.0005	Y	1	24	0.002636663	\$5,849.67	R
755804	\$347,489	\$71,361	\$580,000	\$998,850	7	S	0.00011	\$110	N	0.002	Y	1	24	0.002636663	\$2,633.63	R
755806	\$471,274	\$314,535	\$1,160,000	\$1,945,809	7	S	0.00011	\$214	N	0.0005	Y	1	15	0.00164873	\$3,208.11	R
755807	\$285,480	\$518,508	\$1,160,000	\$1,963,988	7	S	0.00011	\$216	N	0.0005	Y	1	15	0.00164873	\$3,238.09	R
755808	\$744,111	\$1,786,258	\$1,160,000	\$3,690,369	6	S	0.00011	\$406	N	0.002	Y	1	40	0.004390575	\$16,202.84	R
755809	\$834,386	\$1,801,668	\$2,900,000	\$5,536,054	7	S	0.00011	\$609	N	0.002	Y	1	37	0.004061952	\$22,487.18	R
755812	\$3,955,483	\$3,381,298	\$2,900,000	\$10,236,781	8	S	0.000022	\$23	N	0.002	Y	1	57	0.000125392	\$1,283.61	R
755813	\$601,769	\$784,414	\$1,160,000	\$2,546,184	7	R	0.000077	\$196	N	0.0005	Y	1	58	0.004456213	\$11,346.34	R
755814	\$3,358,895	\$7,028,072	\$2,900,000	\$13,286,967	7	S	0.00011	\$1,462	Y	0.002	Y	1	61	0.006687905	\$88,861.97	R
755815	\$1,281,312	NA	\$0	\$1,281,312	7	O	0.00017	\$218	N	0.0005	Y	1	36	0.006101828	\$7,818.35	R
755817	\$1,744,742	\$641,736	\$1,160,000	\$3,546,478	7	S	0.00011	\$390	N	0.0005	Y	1	65	0.00712489	\$25,268.27	R
755904	\$3,694,773	\$22,626,274	\$2,900,000	\$29,221,047	7	S	0.00011	\$3,214	N	0.0005	Y	1	47	0.005156941	\$150,691.23	R
755905	\$3,156,558	\$6,775,555	\$2,900,000	\$12,832,113	7	S	0.00011	\$1,412	N	0.0005	Y	1	47	0.005156941	\$66,174.46	R
755916	\$1,103,244	\$181,544	\$1,160,000	\$2,444,787	7	R	0.000077	\$188	N	0.002	Y	1	54	0.004149527	\$10,144.71	R
755917	\$1,922,155	\$609,192	\$1,160,000	\$3,691,346	7	R	0.000077	\$284	N	0.002	Y	1	56	0.004302882	\$15,883.43	R
755941	\$4,657,953	\$0	\$2,900,000	\$7,557,953	8	R	0.0000017	\$13	N	0.002	Y	1	59	0.000100295	\$758.03	R
755944	\$1,536,478	\$459,858	\$1,160,000	\$3,156,336	8	R	0.0000017	\$5	N	0.002	Y	1	69	0.000117293	\$370.22	R
755947	\$2,525,071	\$969,744	\$2,900,000	\$6,394,816	7	R	0.000077	\$492	N	0.002	Y	1	69	0.005299114	\$33,886.86	R
755948	\$4,657,953	\$2,136,725	\$2,900,000	\$9,694,678	7	R	0.000077	\$746	N	0.002	Y	1	69	0.005299114	\$51,373.21	R
756000	\$520,040	\$202,302	\$1,160,000	\$1,882,341	7	R	0.000077	\$145	N	0.002	Y	1	38	0.002921836	\$5,499.89	R
756001	\$520,040	\$222,620	\$1,160,000	\$1,902,659	7	R	0.000077	\$147	N	0.0005	Y	1	38	0.002921836	\$5,559.26	R
756002	\$2,353,980	\$1,636,885	\$2,900,000	\$6,890,865	7	R	0.000077	\$531	N	0.002	Y	1	47	0.003612598	\$24,893.93	R
756003	\$2,395,278	\$1,868,699	\$2,900,000	\$7,163,977	7	R	0.000077	\$552	N	0.002	Y	1	47	0.003612598	\$25,880.57	R
756004	\$3,320,813	\$21,033,501	\$2,900,													



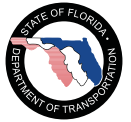
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
756020	\$2,212,606	\$874,558	\$2,900,000	\$5,987,164	7	R	0.000077	\$461	N	0.0005	Y	1	55	0.004226207	\$25,303.00	R
756021	\$2,212,606	\$801,060	\$2,900,000	\$5,913,666	8	R	0.000017	\$10	N	0.002	Y	1	55	9.34957E-05	\$552.90	R
756022	\$1,186,963	\$2,736,495	\$2,900,000	\$6,823,459	7	S	0.00011	\$751	N	0.002	Y	1	54	0.005922718	\$40,413.42	R
756026	\$988,090	\$423,131	\$2,900,000	\$4,311,221	7	R	0.000077	\$332	N	0.002	Y	1	59	0.00453287	\$19,542.21	R
756027	\$988,090	\$388,219	\$2,900,000	\$4,276,309	8	R	0.000017	\$7	N	0.002	Y	1	59	0.000100295	\$428.89	R
756028	\$2,116,900	\$423,131	\$2,900,000	\$5,440,030	N	N	NA	NA	N	0.0005	N	1	59	NA	NA	R
756029	\$3,477,763	\$388,219	\$2,900,000	\$6,765,982	N	N	NA	NA	N	0.0005	N	1	59	NA	NA	R
756032	\$6,279,528	\$1,466	\$0	\$6,280,994	7	O	0.00017	\$1,068	Y	0.002	Y	1	66	0.011158234	\$70,084.80	R
756033	\$6,279,528	\$1,466	\$0	\$6,280,994	7	R	0.000077	\$484	Y	0.002	Y	1	66	0.005069303	\$31,840.26	R
756046	\$355,074	\$2,550,691	\$2,900,000	\$5,805,766	7	S	0.00011	\$639	N	0.002	Y	1	36	0.003952386	\$22,946.63	R
756411	\$364,962	\$1,319,358	\$1,160,000	\$2,844,320	7	R	0.000077	\$219	N	0.002	Y	1	38	0.002921836	\$8,310.64	R
756417	\$398,394	\$1,194,661	\$1,160,000	\$2,753,054	7	R	0.000077	\$212	N	0.002	Y	1	38	0.002921836	\$8,043.97	R
756420	\$281,438	\$33,679,943	\$2,900,000	\$36,861,381	7	R	0.000077	\$2,838	N	0.002	Y	1	37	0.002845055	\$104,872.65	R
756421	\$837,820	\$12,121,957	\$2,900,000	\$15,859,777	7	R	0.000077	\$1,221	N	0.002	Y	1	35	0.002691475	\$42,686.20	R
756422	\$696,200	\$483,654	\$1,160,000	\$2,339,853	7	R	0.000077	\$180	N	0.0005	Y	1	55	0.004226207	\$9,888.70	R
756426	\$1,542,631	\$1,444,245	\$2,900,000	\$5,886,876	8	S	0.0000022	\$13	N	0.002	Y	1	55	0.000120993	\$712.27	R
756427	\$584,492	\$976,325	\$1,160,000	\$2,720,817	7	S	0.00011	\$299	N	0.002	Y	1	69	0.007561683	\$20,573.96	R
756428	\$829,641	\$1,002,173	\$2,900,000	\$4,731,814	7	R	0.000077	\$364	N	0.002	Y	1	56	0.004302882	\$20,360.44	R
756429	\$508,048	\$87,957	\$580,000	\$1,176,006	7	S	0.00011	\$129	N	0.002	Y	1	55	0.006032066	\$7,093.75	R
756500	\$898,721	\$427,423	\$0	\$1,326,144	7	N	NA	NA	Y	0.002	N	1	69	NA	NA	R
756702	\$520,040	\$1,834,787	\$1,160,000	\$3,514,827	7	S	0.00011	\$387	N	0.002	Y	1	42	0.004609597	\$16,201.94	R
764002	\$500,351	\$2,164,752	\$1,160,000	\$3,825,102	5	S	0.00024	\$13	N	0.002	Y	1	21	0.005027922	\$19,232.32	T
764033	\$348,480	\$293,505	\$1,160,000	\$1,801,985	6	S	0.00011	\$198	N	0.002	Y	1	21	0.002307641	\$4,158.01	R
764042	\$148,523	NA	\$0	\$148,523	6	S	0.00011	\$16	N	0.0005	Y	1	57	0.006250727	\$928.38	R
764045	\$71,889	\$24,045	\$0	\$95,934	5	R	0.00018	\$0	N	0.002	Y	1	59	0.010564753	\$1,013.52	R
770002	\$772,861	\$1,806,650	\$2,900,000	\$5,479,510	6	S	0.00011	\$603	Y	0.0005	Y	1	15	0.00164873	\$9,034.23	R
770030	\$3,201,570	\$24,034,003	\$2,900,000	\$30,135,573	7	S	0.00011	\$3,315	Y	0.0005	Y	1	43	0.00471909	\$142,212.48	R
770035	\$4,556,191	\$45,021,222	\$2,900,000	\$52,477,413	7	S	0.00011	\$5,773	Y	0.002	Y	1	53	0.005813357	\$305,069.95	R
770037	\$10,014,318	\$17,318,651	\$2,900,000	\$30,232,969	7	R	0.000077	\$2,328	Y	0.002	Y	1	55	0.004226207	\$127,770.80	R
774003	\$371,236	\$676,303	\$1,160,000	\$2,207,539	7	S	0.00011	\$243	N	0.002	Y	1	28	0.003075431	\$6,789.13	R
774004	\$357,572	\$1,216,473	\$2,900,000	\$4,474,045	6	S	0.00011	\$492	N	0.002	Y	1	37	0.004061952	\$18,173.35	R
774006	\$463,610	\$1,283,945	\$2,900,000	\$4,647,555	7	S	0.00011	\$511	N	0.0005	Y	1	27	0.002965757	\$13,783.52	R
774007	\$227,248	\$4,511,778	\$2,900,000	\$7,639,025	6	S	0.00011	\$840	N	0.002	Y	1	15	0.00164873	\$12,594.69	R
774008	\$181,088	\$406,890	\$1,160,000	\$1,747,978	6	S	0.00011	\$192	N	0.0005	Y	1	31	0.003404379	\$5,950.78	R
774009	\$422,718	\$1,824,820	\$2,900,000	\$5,147,538	6	S	0.00011	\$566	N	0.002	Y	1	33	0.003623618	\$18,652.71	R
774014	\$332,131	\$1,216,473	\$2,900,000	\$4,448,605	7	S	0.00011	\$489	N	0.0005	Y	1	42	0.004609597	\$20,506.28	R
774016	\$2,356,368	NA	\$1,160,000	\$3,516,368	7	S	0.00011	\$387	Y	0.0005	Y	1	47	0.005156941	\$18,133.70	R
774033	\$7,430,094	\$1,915,855	\$2,900,000	\$12,245,949	6	R	0.000077	\$943	N	0.0005	Y	1	59	0.00453287	\$55,509.30	R
774034	\$3,898,039	\$1,370,989	\$1,160,000	\$6,429,028	6	R	0.000077	\$495	N	0.0005	Y	1	61	0.004686166	\$30,127.49	R
774035	\$1,121,817	\$962,683	\$2,900,000	\$4,984,500	6	S	0.00011	\$548	N	0.002	Y	1	64	0.007015662	\$34,969.57	R
774036	\$931,122	\$801,738	\$2,900,000	\$4,632,860	7	S	0.00011	\$510	N	0.002	Y	1	63	0.006906421	\$31,996.48	R
774040	\$931,122	\$1,596,395	\$2,900,000	\$5,427,517	7	S	0.00011	\$597	N	0.0005	Y	1	63	0.006906421	\$37,484.72	R
774042	\$1,121,817	\$962,683	\$2,900,000	\$4,984,500	7	S	0.00011	\$548	N	0.0005	Y	1	64	0.007015662	\$34,969.57	R
774048	\$633,671	\$2,719,778	\$2,900,000	\$6,253,449	5	S	0.00024	\$21	N	0.002	Y	1	55	0.013114826	\$82,012.89	R
774050	\$2,069,702	\$2,536,800	\$2,900,000	\$7,506,502	8	S	0.0000022	\$17	N	0.0005	Y	1	70	0.000153988	\$1,155.91	R
775100	\$181,088	\$686,066	\$1,160,000	\$2,027,154	7	S	0.00011	\$223	N	0.0005	Y	1	40	0.004390575	\$8,900.37	R
775101	\$181,088	\$1,213,370	\$1,160,000	\$2,554,458	6	S	0.00011	\$281	N	0.002	Y	1	36	0.003952386	\$10,096.21	R
775102	\$206,653	\$1,212,226	\$1,160,000	\$2,578,879	6	S	0.00011	\$284	N	0.0005	Y	1	40	0.004390575	\$11,322.76	R
775501	\$2,937,957	\$19,913,678	\$2,900,000	\$25,751,635	7	S	0.00011	\$2,833	N	0.002	Y	1	54	0.005922718	\$152,519.67	R
775502	\$6,148,470	\$1,828,627	\$1,160,000	\$9,137,097	6	R	0.000077	\$704	N	0.0005	Y	1	63	0.004839439	\$44,218.42	R
775702	\$301,540	\$906,927	\$1,160,000	\$2,368,467	7	S	0.00011	\$261	N	0.0005	Y	1	39	0.004281046	\$10,139.52	R
775703	\$356,510	\$760,742	\$1,160,000	\$2,277,252	6	O	0.00017	\$387	N	0.002	Y	1	39	0.006060863	\$15,049.52	R
775707	\$432,645	\$1,384,711	\$2,900,000	\$4,717,356	7	S	0.00011	\$519	N	0.0005	Y	1	38	0.004171505	\$19,678.47	R
775708	\$326,942	\$868,138	\$1,160,000	\$2,355,079	7	S	0.00011	\$259	N	0.0005	Y	1	38	0.004171505	\$9,824.22	R
775709	\$712,038	\$704,537	\$1,160,000	\$2,576,575	6	O	0.00017	\$438	N	0.002	Y	1	47	0.007958839	\$20,506.54	R
775710	\$712,038	\$704,801	\$1,160,000	\$2,576,839	6	S	0.00011	\$283	N	0.002	Y	1	47	0.005156941	\$13,288.61	R
775711	\$1,877,665	\$3,319,338	\$2,900,000	\$8,097,003	6	S	0.00011	\$891	N	0.002	Y	1	48	0.005266374	\$42,641.85	R
775712	\$1,050,521	\$5,673,348	\$2,900,000	\$9,623,869	6	O	0.00017	\$1,636	N	0.002	Y	1	53	0.008970291	\$86,328.90	R
775713	\$257,630	NA	\$580,000	\$837,630	7	S	0.00011	\$92	Y	0.0005	Y	1	61	0.006687905	\$5,601.99	R
780071	\$3,517,969	\$21,903,876	\$2,900,000	\$28,321,845	6	S	0.00011	\$3,115	N	0.002	Y	1	22	0.002417207	\$68,459.76	T
784001	\$133,914	\$82,328	\$580,000	\$796,242	5	S	0.00024	\$3	N	0.002	Y	1	15	0.003593958	\$2,861.66	R
784002	\$178,255	\$380,239	\$1,160,000	\$1,718,494	4	S	0.0005	\$859	N	0.0005	N	1	15	0.007473807	\$12,843.69	R
784017	\$490,125	\$591,403	\$580,000	\$1,661,528	6	S	0.00011	\$183	N	0.0002	Y	1	20	0.002197703	\$3,651.54	R
784023	\$445,568	\$3,900,802	\$1,160,000	\$5,506,369	6	S	0.00011	\$606	N	0.002	Y	1	23	0.002526941	\$13,914.27	R
784038	\$329,617	\$105,900	\$580,000	\$1,015,517	4	S	0.0005	\$508	N	0.0001	N	1	44	0.021765147	\$22,102.88	T
784046	\$451,873	\$35,417	\$580,000	\$1,067,291	6	S	0.00011	\$117	N	0.0001	N	1	54	0.005922718	\$6,321.26	R
784051	\$118,205	NA	\$580,000	\$698,205	7	R	0.000077	\$54	Y	0.0001	Y	1	57	0.004379551	\$3,057.82	R
790012	\$2,498,008	\$22,784,529	\$2,900,000	\$28,182,536	6	S	0.00011	\$3,100	Y	0.0001	N	1	15	0.00164873	\$46,465.40	T
790013	\$1,032,042	\$5,838,669	\$2,900,000	\$9,770,711	7	S	0.00011	\$1,075	Y	0.0001	N	1	15	0.00164873	\$16,109.27	T
790021	\$1,508,076	\$2,232,182	\$2,900,000	\$6,640,257	6	S	0.00011	\$730	Y	0.001	Y	1	15	0.00164873	\$10,947.99	R
790028	\$1,698,926	\$18,467,390	\$2,900,000	\$23,066,316	7	S	0.00011	\$2,537	Y	0.001	Y	1	35	0.003842809	\$88,639.45	R
790029	\$1,834,619	\$18,467,390	\$2,900,000	\$23,202,009	7	S	0.00011	\$2,552	Y	0.001	Y					



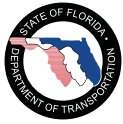
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
794008	\$266,891	\$13,152,112	\$2,900,000	\$16,319,003	6	S	0.00011	\$1,795	N	0.002	Y	1	27	0.002965757	\$48,398.19	R
794009	\$621,560	\$9,861,879	\$2,900,000	\$13,383,439	7	S	0.00011	\$1,472	N	0.002	Y	1	28	0.003075431	\$41,159.84	R
794010	\$211,141	\$3,218,498	\$2,900,000	\$6,329,639	7	S	0.00011	\$696	N	0.002	Y	1	28	0.003075431	\$19,466.37	R
794011	\$1,094,160	\$5,872,014	\$2,900,000	\$9,866,174	7	S	0.00011	\$1,085	Y	0.002	Y	1	28	0.003075431	\$30,342.73	R
794014	\$169,031	\$833,306	\$1,160,000	\$2,162,338	6	S	0.00011	\$238	N	0.001	Y	1	28	0.003075431	\$6,650.12	R
794015	\$2,910,144	\$422,370	\$1,160,000	\$4,492,514	6	S	0.00011	\$494	N	0.001	Y	1	28	0.003075431	\$13,816.41	T
794016	\$1,573,909	\$2,341,333	\$1,160,000	\$5,075,241	6	S	0.00011	\$558	N	0.002	Y	1	30	0.003294742	\$16,721.61	T
794019	\$252,064	\$7,516,690	\$2,900,000	\$10,668,753	7	S	0.00011	\$1,174	N	0.002	Y	1	31	0.003404379	\$36,320.48	R
794020	\$110,908	\$65,440	\$580,000	\$756,348	7	S	0.00011	\$83	N	0.002	Y	1	31	0.003404379	\$2,574.90	R
794022	\$1,399,540	\$2,971,810	\$1,160,000	\$5,531,350	6	S	0.00011	\$608	N	0.002	Y	1	33	0.003623618	\$20,043.50	T
794025	\$16,298,105	\$1,556,491	\$1,160,000	\$19,014,596	5	S	0.00024	\$65	Y	0.002	Y	1	21	0.005027922	\$95,603.91	T
794032	\$513,165	\$2,262,494	\$580,000	\$3,355,658	6	S	0.00011	\$369	Y	0.0005	Y	1	35	0.003842809	\$12,895.15	R
794035	\$659,611	\$10,853,080	\$2,900,000	\$14,412,691	6	S	0.00011	\$1,585	N	0.0005	Y	1	41	0.004500092	\$64,858.44	R
794036	\$367,280	\$6,327,925	\$2,900,000	\$9,595,205	7	S	0.00011	\$1,055	N	0.002	Y	1	41	0.004500092	\$43,179.31	R
794038	\$1,786,298	\$4,797,977	\$1,160,000	\$7,744,275	7	S	0.00011	\$852	N	0.002	Y	1	34	0.00373322	\$28,911.08	R
794045	\$252,345	\$10,352,702	\$2,900,000	\$13,505,047	6	S	0.00011	\$1,486	N	0.002	Y	1	27	0.002965757	\$40,052.68	R
794061	\$236,316	\$924,430	\$1,160,000	\$2,320,746	7	S	0.00011	\$255	N	0.002	Y	1	39	0.004281046	\$9,935.22	T
794063	\$238,610	\$925,310	\$1,160,000	\$2,323,920	7	S	0.00011	\$256	N	0.0005	Y	1	39	0.004281046	\$9,948.81	R
794065	\$125,158	NA	\$0	\$125,158	5	S	0.00024	\$0	Y	0.0005	Y	1	15	0.003593958	\$449.81	R
794067	\$243,199	\$2,053,097	\$1,160,000	\$3,456,296	7	S	0.00011	\$380	N	0.002	Y	1	41	0.004500092	\$15,553.65	R
794117	\$968,253	\$1,330,792	\$1,160,000	\$3,459,045	7	S	0.00011	\$380	N	0.002	Y	1	50	0.005485204	\$18,973.57	T
794118	\$798,941	\$2,927,743	\$1,160,000	\$4,886,684	6	S	0.00011	\$538	N	0.0002	Y	1	50	0.005485204	\$26,804.46	R
794120	\$4,098,980	\$4,316,198	\$2,900,000	\$11,315,178	7	R	0.000077	\$871	N	0.001	Y	1	55	0.004226207	\$47,820.29	T
794121	\$4,762,868	\$2,324,463	\$2,900,000	\$9,987,331	7	R	0.000077	\$769	N	0.001	Y	1	57	0.004379551	\$43,740.02	R
794122	\$390,855	\$186,614	\$1,160,000	\$1,737,469	6	S	0.00011	\$191	N	0.002	Y	1	54	0.005922718	\$10,290.54	T
794123	\$280,563	\$942,901	\$1,160,000	\$2,383,465	7	S	0.00011	\$262	N	0.002	Y	1	46	0.005047497	\$12,030.53	T
794124	\$288,430	\$942,901	\$1,160,000	\$2,391,331	7	S	0.00011	\$263	N	0.0001	N	1	46	0.005047497	\$12,070.24	T
794126	\$679,121	\$1,203,958	\$1,160,000	\$3,043,079	7	S	0.00011	\$335	N	0.002	Y	1	54	0.005922718	\$18,023.30	T
794130	\$281,992	\$855,031	\$1,160,000	\$2,297,022	6	S	0.00011	\$253	N	0.0001	N	1	54	0.005922718	\$13,604.61	T
794131	\$273,446	\$610,325	\$1,160,000	\$2,043,771	7	S	0.00011	\$225	N	0.0001	N	1	53	0.005813357	\$11,881.17	R
794133	\$273,446	\$610,325	\$1,160,000	\$2,043,771	7	O	0.00017	\$347	N	0.0001	N	1	53	0.008970291	\$18,333.22	R
794139	\$440,336	\$1,303,174	\$580,000	\$2,323,510	7	S	0.00011	\$256	N	0.0001	N	1	51	0.0055946	\$12,999.11	R
794141	\$679,558	\$2,178,909	\$1,160,000	\$4,018,467	7	S	0.00011	\$442	N	0.0001	N	1	51	0.0055946	\$22,481.72	R
794146	\$444,044	\$60,515	\$580,000	\$1,084,559	7	S	0.00011	\$119	N	0.0001	N	1	49	0.005375795	\$5,830.37	R
794162	\$268,483	\$802,170	\$1,160,000	\$2,230,653	7	R	0.000077	\$172	N	0.0005	Y	1	53	0.004072841	\$9,085.09	R
794184	\$140,609	NA	\$0	\$140,609	6	S	0.00011	\$15	Y	0.001	Y	1	54	0.005922718	\$832.79	R
794185	\$140,609	NA	\$0	\$140,609	6	S	0.00011	\$15	Y	0.0001	N	1	54	0.005922718	\$832.79	R
795000	\$510,745	\$2,068,688	\$2,900,000	\$5,479,434	6	S	0.00011	\$603	N	0.002	Y	1	21	0.002307461	\$12,643.58	T
795502	\$155,827	\$200,116	\$1,160,000	\$1,515,943	6	R	0.000077	\$117	N	0.002	Y	1	15	0.001154378	\$1,749.97	T
795503	\$268,102	\$115,719	\$580,000	\$963,821	7	S	0.00011	\$106	N	0.0005	Y	1	65	0.00712489	\$6,867.12	R
795521	\$374,272	\$1,805,196	\$2,900,000	\$5,079,468	7	S	0.00011	\$559	N	0.002	Y	1	31	0.003404379	\$17,292.44	R
795700	\$263,333	\$571,282	\$1,160,000	\$1,994,615	6	O	0.00017	\$339	N	0.001	Y	1	31	0.005256584	\$10,484.86	T
795701	\$139,954	NA	\$1,160,000	\$1,299,954	7	S	0.00011	\$143	Y	0.0001	N	1	31	0.003404379	\$4,425.54	T
795713	\$338,062	\$1,007,989	\$1,160,000	\$2,506,052	7	S	0.00011	\$276	N	0.0001	N	1	28	0.003075431	\$7,707.19	T
796000	\$3,195,452	\$1,277,110	\$2,900,000	\$7,372,562	7	S	0.00011	\$811	N	0.0001	N	1	45	0.00493804	\$36,406.01	R
796412	\$227,810	\$1,431,677	\$2,900,000	\$4,559,486	7	O	0.00017	\$775	N	0.0002	Y	1	28	0.004749092	\$21,653.42	T
796500	\$301,718	NA	\$580,000	\$881,718	6	S	0.00011	\$97	Y	0.0001	N	1	49	0.005375795	\$4,739.94	T
796518	\$437,702	\$726,438	\$1,160,000	\$2,324,140	7	O	0.00017	\$395	N	0.0001	N	1	31	0.005256584	\$12,217.04	T
796547	\$295,079	NA	\$1,160,000	\$1,455,079	6	S	0.00011	\$160	Y	0.0001	N	1	26	0.002856071	\$4,155.81	T
796566	\$301,540	NA	\$1,160,000	\$1,461,540	7	O	0.00017	\$248	Y	0.0001	N	1	38	0.006439725	\$9,411.92	T
860001	\$2,135,754	\$12,462,657	\$2,900,000	\$17,498,410	6	R	0.000077	\$1,347	Y	0.0001	Y	1	15	0.001154378	\$20,199.77	T
860060	\$40,469,935	\$4,814,341	\$2,900,000	\$48,184,276	7	R	0.000077	\$3,710	N	0.0001	Y	1	33	0.002537872	\$122,285.52	T
860063	\$2,470,195	\$15,544,928	\$2,900,000	\$20,915,123	6	R	0.000077	\$1,610	Y	0.0001	Y	1	15	0.001154378	\$24,143.95	T
860096	\$2,799,080	\$5,382,137	\$2,900,000	\$11,081,217	7	R	0.000077	\$853	Y	0.0001	Y	1	22	0.001692631	\$18,756.41	T
860139	\$3,839,861	\$12,486,558	\$2,900,000	\$19,226,420	7	R	0.000077	\$1,480	Y	0.0001	Y	1	31	0.002384245	\$45,840.50	T
860156	\$1,797,879	\$5,267,195	\$2,900,000	\$9,965,074	6	S	0.00011	\$1,096	N	0.0001	N	1	30	0.003294742	\$32,832.35	T
860159	\$1,760,732	\$5,790,210	\$2,900,000	\$10,450,943	6	S	0.00011	\$1,150	N	0.0001	N	1	30	0.003294742	\$34,433.16	T
860213	\$20,686,031	\$14,133,080	\$2,900,000	\$37,719,111	7	R	0.000077	\$2,904	Y	0.0001	Y	1	35	0.002691475	\$101,520.05	T
860274	\$1,874,981	\$9,800,770	\$2,900,000	\$14,575,750	7	S	0.00011	\$1,603	N	0.0001	N	1	40	0.004390575	\$63,995.93	T
860319	\$33,607,942	\$7,937,836	\$2,900,000	\$44,445,778	7	R	0.00011	\$4,889	N	0.0001	N	1	47	0.005156941	\$229,204.28	T
860431	\$57,619,040	\$21,388,058	\$2,900,000	\$81,907,098	7	R	0.000077	\$6,307	Y	0.002	Y	0.67	54	0.004149527	\$339,875.71	T
860466	\$29,158,917	\$1,843,790	\$2,900,000	\$33,902,707	7	R	0.000077	\$2,611	N	0.002	Y	1	55	0.004226207	\$143,279.87	T
860467	\$28,981,118	\$1,843,790	\$2,900,000	\$33,724,909	7	R	0.000077	\$2,597	N	0.002	Y	1	53	0.004072841	\$137,356.18	T
860574	\$3,360,019	\$20,212,082	\$2,900,000	\$26,472,101	7	R	0.000077	\$2,038	Y	0.0002	Y	1	56	0.004302882	\$113,906.33	T
860575	\$3,360,019	\$20,212,082	\$2,900,000	\$26,472,101	7	R	0.000077	\$2,038	Y	0.002	Y	1	56	0.004302882	\$113,906.33	T
860591	\$3,363,640	\$5,633,804	\$2,900,000	\$11,897,444	7	R	0.000077	\$916	N	0.002	Y	1	48	0.00368932	\$43,893.48	T
860592	\$9,557,388	\$3,207,754	\$2,900,000	\$15,665,142	7	R	0.000077	\$1,206	N	0.002	Y	1	50	0.003842746	\$60,197.16	T
864028	\$1,512,134	\$7,472,373	\$2,900,000	\$11,884,506	6	S	0.00011	\$1,307	N	0.002	Y	1	15	0.00164873	\$19,594.34	T
864031	\$685,348	\$3,540,540	\$1,160,000	\$5,386,888	6	S	0.00011	\$284	N	0.002	Y	1	24	0.002636663	\$6,799.66	T
864069	\$987,653	\$3,105,458	\$2,900,000	\$6,993,111	7	S	0.00011	\$769	N	0.002	Y	1	31	0.003404379	\$23,807.20	T
864070	\$859,608	\$3,348,003	\$2,900,000	\$7,107,611	7	S	0.00011	\$782	N	0.002	Y	1	15</			



Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
865710	\$672,316	\$1,742,090	\$2,900,000	\$5,314,406	6	S	0.00011	\$585	N	0.0002	Y	1	28	0.003075431	\$16,344.09	T
865712	\$187,175	NA	\$1,160,000	\$1,347,175	6	S	0.00011	\$148	Y	0.0002	Y	1	22	0.002417207	\$3,256.40	T
865713	\$192,794	NA	\$1,160,000	\$1,352,794	5	S	0.00024	\$5	Y	0.0005	Y	1	22	0.005266716	\$7,124.78	T
865720	\$857,423	\$2,982,843	\$2,900,000	\$6,740,266	6	S	0.00011	\$741	N	0.0002	Y	1	15	0.00164873	\$11,112.88	T
865725	\$407,009	NA	\$1,160,000	\$1,567,009	6	S	0.00011	\$172	Y	0.0005	Y	1	25	0.002746373	\$4,303.59	T
865727	\$237,900	NA	\$1,160,000	\$1,397,900	6	S	0.00011	\$154	Y	0.0005	Y	1	15	0.00164873	\$2,304.76	T
865728	\$477,244	\$1,286,123	\$1,160,000	\$2,923,366	6	S	0.00011	\$322	N	0.001	Y	1	19	0.002087932	\$6,103.79	T
865729	\$1,725,147	\$4,180,282	\$2,900,000	\$8,805,429	7	S	0.00011	\$969	Y	0.002	Y	1	15	0.00164873	\$14,517.78	T
865732	\$166,946	NA	\$580,000	\$746,946	6	S	0.00011	\$82	Y	0.0001	N	1	15	0.00164873	\$1,231.51	T
865733	\$892,759	NA	\$2,900,000	\$3,792,759	6	S	0.00011	\$417	Y	0.0002	Y	1	28	0.003075431	\$11,664.37	T
865737	\$308,311	NA	\$580,000	\$888,311	7	S	0.00011	\$98	Y	0.0002	Y	1	15	0.00164873	\$1,464.59	T
865738	\$777,730	NA	\$1,160,000	\$1,937,730	6	O	0.00017	\$329	Y	0.0001	N	1	32	0.00542569	\$10,513.52	T
865739	\$777,730	NA	\$1,160,000	\$1,937,730	6	O	0.00017	\$329	Y	0.0001	N	1	32	0.00542569	\$10,513.52	T
865740	\$770,004	NA	\$1,160,000	\$1,930,004	7	S	0.00011	\$212	Y	0.0002	Y	1	34	0.00373322	\$7,205.13	T
865742	\$770,004	NA	\$1,160,000	\$1,930,004	6	S	0.00011	\$212	Y	0.0001	N	1	34	0.00373322	\$7,205.13	T
865743	\$770,004	NA	\$1,160,000	\$1,930,004	6	S	0.00011	\$212	Y	0.0001	N	1	35	0.003842809	\$7,416.64	T
865748	\$11,387,356	\$1,424,759	\$2,900,000	\$15,712,115	6	S	0.00011	\$1,728	Y	0.0002	Y	1	15	0.00164873	\$25,905.04	T
865758	\$466,981	\$2,392,830	\$2,900,000	\$5,759,812	7	S	0.00011	\$634	N	0.002	Y	1	37	0.004061952	\$23,396.08	T
865762	\$594,457	NA	\$1,160,000	\$1,754,457	6	S	0.00011	\$193	Y	0.0002	Y	1	38	0.004171505	\$7,318.73	T
865763	\$635,232	NA	\$1,160,000	\$1,795,232	6	S	0.00011	\$197	Y	0.002	Y	1	38	0.004171505	\$7,488.82	T
865764	\$615,918	NA	\$1,160,000	\$1,775,918	6	S	0.00011	\$195	Y	0.0005	Y	1	38	0.004171505	\$7,408.25	T
865765	\$1,004,354	NA	\$1,160,000	\$2,164,354	6	S	0.00011	\$238	Y	0.0002	Y	1	18	0.00197703	\$4,281.42	T
865766	\$738,305	NA	\$1,160,000	\$1,898,305	6	S	0.00011	\$209	Y	0.002	Y	1	20	0.002197703	\$4,171.91	T
865767	\$749,753	NA	\$1,160,000	\$1,909,753	6	S	0.00011	\$210	Y	0.002	Y	1	20	0.002197703	\$4,197.07	T
865770	\$644,753	NA	\$1,160,000	\$1,804,753	5	S	0.00024	\$6	Y	0.002	Y	1	24	0.00574413	\$10,366.74	T
865771	\$537,294	NA	\$1,160,000	\$1,697,294	6	S	0.00011	\$187	Y	0.0002	Y	1	22	0.002417207	\$4,102.71	T
865772	\$642,646	NA	\$1,160,000	\$1,802,646	5	S	0.00024	\$6	Y	0.0005	Y	1	22	0.005266716	\$9,494.02	T
865773	\$1,041,812	NA	\$1,160,000	\$2,201,812	6	S	0.00011	\$242	Y	0.0005	Y	1	22	0.002417207	\$5,322.24	T
865774	\$642,646	NA	\$1,160,000	\$1,802,646	6	S	0.00011	\$198	Y	0.0005	Y	1	22	0.002417207	\$4,357.37	T
865775	\$936,835	\$2,019,456	\$2,900,000	\$5,856,291	6	S	0.00011	\$644	N	0.002	Y	1	18	0.00197815	\$11,584.62	T
865776	\$428,711	\$344,062	\$1,160,000	\$1,932,774	7	S	0.00011	\$213	N	0.0005	Y	1	41	0.004500092	\$8,697.66	T
865777	\$3,928,138	\$4,712,318	\$2,900,000	\$11,540,457	6	S	0.00011	\$1,269	N	0.0002	Y	1	25	0.002746373	\$31,694.40	T
865778	\$544,317	NA	\$1,160,000	\$1,704,317	4	S	0.0005	\$852	Y	0.002	Y	1	33	0.016368679	\$27,897.42	T
866100	\$4,625,364	\$1,721,486	\$2,900,000	\$9,246,850	7	S	0.00011	\$1,017	N	0.002	Y	1	44	0.004828571	\$44,649.07	T
866101	\$3,317,317	NA	\$2,900,000	\$6,217,317	7	S	0.00011	\$684	N	0.0002	Y	1	44	0.004828571	\$30,020.76	T
866102	\$5,650,039	\$1,375,892	\$2,900,000	\$9,925,931	6	S	0.00011	\$1,092	N	0.002	Y	1	36	0.003952386	\$39,231.12	T
866200	\$194,415	NA	\$580,000	\$774,415	4	S	0.0005	\$387	Y	0.002	Y	1	31	0.01538431	\$11,913.84	T
866303	\$382,919	\$276,542	\$1,160,000	\$1,819,461	7	S	0.00011	\$200	N	0.0005	Y	1	29	0.003185092	\$5,795.15	T
866304	\$645,877	\$2,233,035	\$2,900,000	\$5,778,912	7	S	0.00011	\$636	N	0.0002	Y	1	28	0.003075431	\$17,772.64	T
866305	\$656,552	\$2,233,035	\$2,900,000	\$5,789,587	6	S	0.00011	\$637	N	0.002	Y	1	31	0.003404379	\$19,709.95	T
867200	\$226,211	NA	\$580,000	\$806,211	6	O	0.00017	\$137	Y	0.0005	Y	1	16	0.002716535	\$2,190.10	T
867202	\$434,143	\$1,140,623	\$2,900,000	\$4,474,766	6	S	0.00011	\$492	N	0.002	Y	1	16	0.001758549	\$7,869.09	T
867204	\$434,143	\$1,140,623	\$2,900,000	\$4,474,766	6	S	0.00011	\$492	N	0.0005	Y	1	21	0.002307461	\$10,325.35	T
867208	\$113,874	NA	\$1,160,000	\$1,273,874	6	S	0.00011	\$140	Y	0.002	Y	1	16	0.001758549	\$2,240.17	T
867209	\$218,851	\$791,615	\$1,160,000	\$2,170,466	7	S	0.00011	\$239	N	0.002	Y	1	16	0.001758549	\$3,816.87	T
867602	\$142,740	\$754,206	\$1,160,000	\$2,056,946	6	S	0.00011	\$226	N	0.002	Y	1	24	0.002636663	\$5,423.47	T
867603	\$445,755	\$1,648,203	\$2,900,000	\$4,993,958	6	S	0.00011	\$549	N	0.002	Y	1	19	0.002087932	\$10,427.05	T
867604	\$124,549	\$171,953	\$1,160,000	\$1,456,502	4	O	0.0006	\$874	N	0.002	Y	1	26	0.01548356	\$22,551.84	T
867606	\$1,207,222	\$2,283,010	\$2,900,000	\$6,390,232	7	S	0.00011	\$703	N	0.002	Y	1	31	0.003404379	\$21,754.77	T
868101	\$862,831	\$257,425	\$1,160,000	\$2,280,256	7	S	0.00011	\$251	N	0.002	Y	1	37	0.004061952	\$9,262.29	R
868109	\$610,455	\$222,392	\$1,160,000	\$1,992,847	6	S	0.00011	\$219	N	0.0005	Y	1	25	0.002746373	\$5,473.10	R
870002	\$1,756,799	\$12,079,343	\$2,900,000	\$16,736,143	7	S	0.00011	\$1,841	Y	0.002	Y	1	15	0.00164873	\$27,593.38	@
870055	\$6,584,564	\$30,808,786	\$2,900,000	\$40,293,350	7	R	0.000077	\$3,103	Y	0.002	Y	1	19	0.001461987	\$58,908.34	T
870056	\$2,248,441	\$26,203,729	\$2,900,000	\$31,352,170	7	R	0.000077	\$2,414	Y	0.002	Y	1	33	0.002537872	\$79,567.79	M
870240	\$833,543	\$1,278,997	\$2,900,000	\$5,012,540	8	R	0.0000017	\$9	Y	0.002	Y	1	33	5.60985E-05	\$281.20	M
874003	\$377,998	\$508,947	\$1,160,000	\$2,046,945	6	S	0.00011	\$225	N	0.002	Y	1	45	0.00493804	\$10,107.90	@
874005	\$178,123	\$597,177	\$1,160,000	\$1,935,300	6	S	0.00011	\$213	N	0.002	Y	1	21	0.002307461	\$4,465.63	@
874017	\$563,187	\$346,911	\$1,160,000	\$2,070,098	7	S	0.00011	\$228	N	0.002	Y	1	23	0.002526941	\$5,231.02	@
874021	\$563,187	\$354,814	\$1,160,000	\$2,078,001	7	S	0.00011	\$229	N	0.002	Y	1	23	0.002526941	\$5,250.99	R
874023	\$542,140	\$541,295	\$1,160,000	\$2,243,435	6	S	0.00011	\$247	N	0.002	Y	1	23	0.002526941	\$5,669.03	R
874024	\$493,234	\$286,565	\$1,160,000	\$1,939,798	6	S	0.00011	\$213	N	0.002	Y	1	21	0.002307461	\$4,476.01	R
874030	\$2,693,041	\$3,641,691	\$2,900,000	\$9,234,732	6	S	0.00011	\$1,016	N	0.002	Y	1	30	0.003294742	\$30,426.06	R
874032	\$875,902	\$1,157,601	\$2,900,000	\$4,933,504	7	S	0.00011	\$543	N	0.002	Y	1	22	0.002417207	\$11,925.30	R
874093	\$412,792	\$1,197,396	\$1,160,000	\$2,770,187	7	S	0.00011	\$305	N	0.002	Y	1	32	0.003514005	\$9,734.45	R
874103	\$917,793	\$0	\$0	\$917,793	8	S	0.0000022	\$2	N	0.002	Y	1	70	0.000153988	\$141.33	R
874104	\$415,507	\$836,737	\$1,160,000	\$2,412,244	6	S	0.00011	\$265	N	0.002	Y	1	33	0.003623618	\$8,741.05	R
874105	\$550,389	\$1,393,531	\$2,900,000	\$4,843,920	5	S	0.00024	\$16	N	0.002	Y	1	32	0.007651499	\$37,063.25	@
874119	\$2,077,787	\$7,760,750	\$2,900,000	\$12,738,536	5	S	0.00024	\$43	N	0.0005	Y	1	25	0.005982752	\$76,211.50	R
874122	\$1,701,314	\$1,060,916	\$1,160,000	\$3,922,230	6	S	0.00011	\$431	N	0.002	Y	1	34	0.00373322	\$14,642.55	R
874129	\$1,147,601	\$2,078,170	\$2,900,000	\$6,125,770	6	S	0.00011	\$674	N	0.002	Y	1	15	0.00164873	\$10,099.74	R
874130	\$794,743	\$2,100,881	\$2,900,000	\$5,795,623	7	S	0.00011	\$638	N	0.0001	N	1	15	0.00164873	\$9,555.42	R
874149	\$899,314	\$6,568,400	\$2,900,000	\$10,367,714	7	S	0.00011	\$1,140	N	0.0001	N	1	26	0.002856071	\$29,610.93	M
874177	\$1,619,140	\$3,090,602	\$2,900,000</													



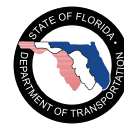
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
874225	\$284,790	\$96,105	\$580,000	\$960,896	7	S	0.00011	\$106	N	0.002	Y	1	32	0.003514005	\$3,376.59	R
874236	\$175,942	NA	\$580,000	\$755,942	7	S	0.00011	\$83	Y	0.002	Y	1	32	0.003514005	\$2,656.38	R
874238	\$498,197	\$3,659,853	\$2,900,000	\$7,058,050	8	S	0.0000022	\$16	Y	0.002	Y	1	26	5.71984E-05	\$403.71	R
874242	\$323,625	\$234,513	\$1,160,000	\$1,718,138	7	S	0.00011	\$189	N	0.002	Y	1	32	0.003514005	\$6,037.55	R
874250	\$456,243	\$1,174,756	\$1,160,000	\$2,791,000	6	S	0.00011	\$307	N	0.002	Y	1	32	0.003514005	\$9,807.59	R
874265	\$388,350	\$329,504	\$1,160,000	\$1,877,855	7	S	0.00011	\$207	N	0.001	Y	1	33	0.003623618	\$6,804.63	R
874307	\$174,088	\$225,170	\$580,000	\$979,258	7	O	0.00017	\$166	Y	0.001	Y	1	15	0.002546968	\$2,494.14	R
874308	\$456,062	\$71,916	\$580,000	\$1,107,978	7	S	0.00011	\$122	N	0.002	Y	1	32	0.003514005	\$3,893.44	R
874310	\$1,183,342	\$4,380,075	\$2,900,000	\$8,463,417	6	S	0.00011	\$931	N	0.002	Y	1	32	0.003514005	\$29,740.49	R
874315	\$158,043	NA	\$0	\$158,043	6	O	0.00017	\$27	N	0.0001	N	1	26	0.00441062	\$697.07	R
874317	\$495,075	\$227,975	\$1,160,000	\$1,883,050	6	S	0.00011	\$207	N	0.0001	N	1	22	0.002417207	\$4,551.72	R
874319	\$523,637	NA	\$1,160,000	\$1,683,637	7	S	0.00011	\$185	Y	0.0001	N	1	41	0.004500092	\$7,576.52	R
874334	\$3,131,835	\$5,194,118	\$2,900,000	\$11,225,953	7	S	0.00011	\$1,235	N	0.0001	N	1	32	0.003514005	\$39,448.05	@
874336	\$2,742,143	\$5,592,646	\$2,900,000	\$11,234,789	7	S	0.00011	\$1,236	N	0.0005	Y	1	30	0.003294742	\$37,015.73	@
874337	\$2,976,133	\$3,546,669	\$2,900,000	\$9,422,802	7	S	0.00011	\$1,037	N	0.002	Y	1	63	0.006906421	\$65,077.84	@
874342	\$388,350	\$312,833	\$1,160,000	\$1,861,183	7	S	0.00011	\$205	N	0.002	Y	1	33	0.003623618	\$6,744.22	R
874350	\$284,790	\$140,562	\$580,000	\$1,005,352	7	S	0.00011	\$111	N	0.0002	Y	1	32	0.003514005	\$3,532.81	R
874352	\$284,790	\$92,837	\$580,000	\$957,627	7	S	0.00011	\$105	N	0.002	Y	1	32	0.003514005	\$3,365.11	R
874355	\$391,066	\$311,362	\$1,160,000	\$1,862,428	7	S	0.00011	\$205	N	0.002	Y	1	32	0.003514005	\$6,544.58	R
874356	\$391,066	\$440,075	\$1,160,000	\$1,991,141	7	S	0.00011	\$219	N	0.002	Y	1	33	0.003623618	\$7,215.14	R
874357	\$323,079	\$173,166	\$1,160,000	\$1,656,245	7	S	0.00011	\$182	N	0.002	Y	1	32	0.003514005	\$5,820.05	R
874386	\$1,201,759	\$2,026,353	\$2,900,000	\$6,128,112	7	S	0.00011	\$674	N	0.0002	Y	1	30	0.003294742	\$20,190.55	@
874414	\$1,358,179	\$2,612,871	\$2,900,000	\$6,871,050	6	S	0.00011	\$756	N	0.001	Y	1	31	0.003404379	\$23,391.66	R
874422	\$716,954	\$3,273,752	\$2,900,000	\$6,890,706	6	S	0.00011	\$758	N	0.0005	Y	1	32	0.003514005	\$24,213.98	R
874423	\$883,519	\$6,241,901	\$2,900,000	\$10,025,420	7	S	0.00011	\$1,103	N	0.0002	Y	1	32	0.003514005	\$35,229.38	R
874433	\$997,049	\$588,401	\$1,160,000	\$2,745,450	7	S	0.00011	\$302	N	0.0002	Y	1	30	0.003294742	\$9,045.55	R
874437	\$461,675	\$364,533	\$1,160,000	\$1,986,208	7	S	0.00011	\$218	N	0.0005	Y	1	32	0.003514005	\$6,979.54	R
874440	\$372,056	\$385,399	\$1,160,000	\$1,917,455	7	S	0.00011	\$211	N	0.0002	Y	1	32	0.003514005	\$6,737.95	R
874441	\$365,641	\$350,957	\$1,160,000	\$1,876,598	7	S	0.00011	\$206	N	0.0005	Y	1	32	0.003514005	\$6,594.37	@
874443	\$496,074	\$2,287,050	\$2,900,000	\$5,683,124	7	S	0.00011	\$625	N	0.002	Y	1	32	0.003514005	\$19,970.53	@
874444	\$456,243	\$984,490	\$1,160,000	\$2,600,733	6	S	0.00011	\$286	N	0.002	Y	1	32	0.003514005	\$9,138.99	R
874445	\$453,528	\$1,198,769	\$1,160,000	\$2,812,296	7	S	0.00011	\$309	N	0.002	Y	1	32	0.003514005	\$9,882.42	R
874446	\$662,639	\$1,073,291	\$2,900,000	\$4,635,930	7	S	0.00011	\$510	N	0.0005	Y	1	32	0.003514005	\$16,290.68	R
874447	\$667,134	\$871,107	\$1,160,000	\$2,698,242	7	S	0.00011	\$297	N	0.0002	Y	1	32	0.003514005	\$9,481.64	R
874448	\$454,242	\$189,435	\$1,160,000	\$1,803,676	7	S	0.00011	\$198	N	0.002	Y	1	31	0.003404379	\$6,140.40	R
874455	\$372,555	NA	\$580,000	\$952,555	7	S	0.00011	\$105	Y	0.002	Y	1	32	0.003514005	\$3,347.28	R
874456	\$835,440	\$429,048	\$1,160,000	\$2,424,487	6	S	0.00011	\$267	N	0.002	Y	1	32	0.003514005	\$8,519.66	R
874476	\$576,157	\$668,532	\$1,160,000	\$2,404,689	7	S	0.00011	\$265	Y	0.002	Y	1	33	0.003623618	\$8,713.68	R
874479	\$133,539	\$776	\$0	\$134,315	4	S	0.0005	\$67	N	0.002	Y	1	33	0.016368679	\$2,198.56	@
874494	\$302,714	\$328,401	\$580,000	\$1,211,115	7	S	0.00011	\$133	N	0.0005	Y	1	35	0.003842809	\$4,654.08	@
874541	\$19,785,531	\$3,046,616	\$2,900,000	\$25,732,147	6	S	0.00011	\$2,831	Y	0.002	Y	1	15	0.00164873	\$42,425.37	T
874542	\$8,718,382	\$2,120,222	\$2,900,000	\$13,738,604	6	S	0.00011	\$1,511	Y	0.002	Y	1	51	0.0055946	\$76,862.00	T
874544	\$49,137,035	NA	\$2,900,000	\$52,037,035	4	O	0.0006	\$31,222	Y	0.002	Y	1	15	0.008962298	\$466,371.42	T
874545	\$96,988,434	NA	\$2,900,000	\$99,888,434	7	S	0.00011	\$10,988	Y	0.0002	Y	1	51	0.0055946	\$558,835.85	T
874712	\$3,292,282	\$2,179,377	\$2,900,000	\$8,371,659	6	S	0.00011	\$921	N	0.002	Y	1	22	0.002417207	\$20,236.03	T
875102	\$2,753,193	\$12,838,244	\$2,900,000	\$18,491,437	6	S	0.00011	\$2,034	Y	0.001	Y	1	24	0.002636663	\$48,755.69	T
875103	\$6,570,517	\$12,838,244	\$2,900,000	\$22,308,760	6	S	0.00011	\$2,454	Y	0.001	Y	1	29	0.003185092	\$71,055.46	T
875800	\$822,587	\$2,306,991	\$2,900,000	\$6,029,578	6	S	0.00011	\$663	N	0.001	Y	1	36	0.003952386	\$23,831.22	M
875801	\$825,490	\$5,196,196	\$2,900,000	\$8,921,685	7	S	0.00011	\$981	N	0.002	Y	1	36	0.003952386	\$35,261.95	R
875802	\$1,390,456	\$2,466,287	\$2,900,000	\$6,756,743	8	S	0.0000022	\$15	N	0.002	Y	1	36	7.9197E-05	\$535.11	R
875803	\$1,864,118	\$3,460,385	\$2,900,000	\$8,224,502	7	S	0.00011	\$905	N	0.002	Y	1	36	0.003952386	\$32,506.41	R
875805	\$310,780	\$19,391	\$0	\$330,171	8	S	0.0000022	\$1	N	0.0001	Y	1	71	0.000156188	\$51.57	R
876100	\$3,219,082	NA	\$1,160,000	\$4,379,082	6	O	0.00017	\$744	Y	0.0001	N	1	15	0.002546968	\$11,153.38	T
876417	\$187,081	\$658,887	\$1,160,000	\$2,005,969	6	O	0.00017	\$341	N	0.0001	N	1	15	0.002546968	\$5,109.14	R
876705	\$1,380,124	\$2,003,995	\$2,900,000	\$6,284,119	6	S	0.00011	\$691	N	0.0005	Y	1	15	0.00164873	\$10,360.82	T
876726	\$1,460,285	\$1,877,179	\$2,900,000	\$6,237,463	7	S	0.00011	\$686	N	0.0005	Y	1	40	0.004390575	\$27,386.05	T
876727	\$1,169,545	\$0	\$1,160,000	\$2,329,545	6	S	0.00011	\$256	Y	0.0005	Y	1	41	0.004500092	\$10,483.17	T
876728	\$1,628,270	\$1,431,367	\$1,160,000	\$4,219,637	7	S	0.00011	\$464	N	0.0001	N	1	49	0.005375795	\$22,683.90	T
876735	\$2,616,283	\$2,620,231	\$2,900,000	\$8,136,513	7	S	0.00011	\$895	N	0.0001	N	1	55	0.006032066	\$49,079.99	T
877301	\$654,960	NA	\$1,160,000	\$1,814,960	6	S	0.00011	\$200	Y	0.002	Y	1	36	0.003952386	\$7,173.42	T
877302	\$338,062	NA	\$1,160,000	\$1,498,062	6	R	0.000077	\$115	Y	0.0002	Y	1	21	0.001615756	\$2,420.50	T
877500	\$4,181,357	\$4,986,143	\$2,900,000	\$12,067,500	7	S	0.00011	\$1,327	N	0.0002	Y	1	22	0.002417207	\$29,169.64	M
877501	\$3,305,954	\$1,416,850	\$2,900,000	\$7,622,805	7	S	0.00011	\$839	N	0.0005	Y	1	28	0.003075431	\$23,443.41	M
878500	\$1,342,416	\$1,015,462	\$1,160,000	\$3,517,877	6	S	0.00011	\$387	N	0.0005	Y	1	47	0.005156941	\$18,141.49	T
880002	\$1,081,393	\$1,249,474	\$2,900,000	\$5,230,867	6	R	0.000077	\$403	Y	0.0002	Y	1	15	0.001154378	\$6,038.40	R
880005	\$13,864,067	\$1,688,778	\$1,160,000	\$16,712,845	5	R	0.00018	\$50	N	0.0005	Y	1	30	0.00538593	\$90,014.21	T
880062	\$544,973	\$885,138	\$1,160,000	\$2,590,111	5	S	0.00024	\$9	Y	0.0001	N	1	15	0.003593958	\$9,308.75	R
880077	\$116,124,250	\$4,951,566	\$2,900,000	\$123,975,816	7	R	0.000077	\$9,546	Y	0.0005	Y	1	45	0.003459137	\$428,849.30	T
890093	\$6,604,667	\$4,049,213	\$1,160,000	\$11,813,880	7	S	0.00011	\$1,300	N	0.0005	Y	1	46	0.005047497	\$59,630.52	R
890107	\$28,032,064	\$18,646,320	\$2,900,000	\$49,578,384	7	R	0.00011	\$5,454	Y	0.0005	Y	1	51	0.0055946	\$277,371.24	T
890138	\$2,370,649	\$8,536,066	\$2,900,000	\$13,806,715	7	R	0.000077	\$1,063	Y	0.0002	Y	1	53	0.004072841	\$56,232.55	T
894059	\$608,371	\$1,171,898	\$1,160,000	\$2,940,270												



Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
904153	\$570,655	NA	\$1,160,000	\$1,730,655	7	S	0.00011	\$190	Y	0.002	Y	1	27	0.002965757	\$5,132.70	T
904155	\$1,060,912	NA	\$1,160,000	\$2,220,912	7	S	0.00011	\$244	Y	0.002	Y	1	34	0.00373322	\$8,291.15	T
904160	\$351,173	\$776	\$0	\$351,948	6	S	0.00011	\$39	N	0.002	Y	1	34	0.00373322	\$1,313.90	T
904250	\$121,272	NA	\$1,160,000	\$1,281,272	6	S	0.00011	\$141	Y	0.001	Y	1	26	0.002856071	\$3,659.40	T
904255	\$808,290	NA	\$580,000	\$1,388,290	7	O	0.00017	\$236	Y	0.0005	Y	1	49	0.008296104	\$11,517.40	T
904260	\$519,174	NA	\$580,000	\$1,099,174	7	S	0.00011	\$121	Y	0.0005	Y	1	49	0.005375795	\$5,908.93	T
904305	\$159,058	\$543,575	\$1,160,000	\$1,862,633	7	S	0.00011	\$205	N	0.0002	Y	1	26	0.002856071	\$5,319.81	T
904307	\$132,548	\$200,612	\$1,160,000	\$1,493,160	7	S	0.00011	\$164	N	0.0002	Y	1	26	0.002856071	\$4,264.57	T
904310	\$192,724	NA	\$1,160,000	\$1,352,724	6	S	0.00011	\$149	Y	0.0005	Y	1	31	0.003404379	\$4,605.19	T
904320	\$16,725,648	NA	\$1,160,000	\$17,885,648	6	S	0.00011	\$1,967	Y	0.0005	Y	1	33	0.003623618	\$64,810.76	T
904490	\$11,527,493	NA	\$580,000	\$12,107,493	4	S	0.0005	\$6,054	Y	0.0005	N	1	26	0.012919074	\$156,417.60	T
904495	\$409,233	NA	\$1,160,000	\$1,569,233	6	S	0.00011	\$173	Y	0.0005	Y	1	33	0.003623618	\$5,686.30	T
904510	\$202,900	NA	\$1,160,000	\$1,362,900	7	O	0.00017	\$232	Y	0.002	Y	1	31	0.005256584	\$7,164.20	T
904512	\$202,900	NA	\$1,160,000	\$1,362,900	6	O	0.00017	\$232	Y	0.002	Y	1	33	0.00594768	\$7,625.11	T
904515	\$178,552	NA	\$580,000	\$758,552	7	O	0.00017	\$129	Y	0.002	Y	1	33	0.00594768	\$4,243.92	T
904517	\$178,552	\$5,125,625	\$580,000	\$5,884,177	7	O	0.00017	\$1,000	Y	0.001	Y	1	33	0.00594768	\$32,920.60	T
904540	\$238,017	NA	\$1,160,000	\$1,398,017	7	O	0.00017	\$238	Y	0.001	Y	1	43	0.007283964	\$10,183.11	T
904600	\$1,835,837	NA	\$1,160,000	\$2,995,837	6	S	0.00011	\$330	Y	0.002	Y	1	33	0.003623618	\$10,855.77	T
904602	\$345,476	NA	\$1,160,000	\$1,505,476	7	O	0.00017	\$256	Y	0.002	Y	1	21	0.003563938	\$5,365.42	T
904603	\$189,282	NA	\$1,160,000	\$1,349,282	6	O	0.00017	\$229	Y	0.002	Y	1	21	0.003563938	\$4,808.76	T
904604	\$253,878	NA	\$1,160,000	\$1,413,878	6	O	0.00017	\$240	Y	0.002	Y	1	21	0.003563938	\$5,038.97	T
904606	\$252,376	NA	\$1,160,000	\$1,412,376	6	S	0.00011	\$155	Y	0.0005	Y	1	21	0.002307461	\$3,259.00	T
904908	\$254,986	NA	\$580,000	\$834,986	6	S	0.00011	\$92	Y	0.0005	Y	1	61	0.006687905	\$5,584.31	T
904910	\$69,501	NA	\$0	\$69,501	7	S	0.00011	\$8	Y	0.002	Y	1	28	0.003075431	\$213.75	T
904980	\$2,657,580	\$5,066,418	\$1,160,000	\$8,883,999	6	O	0.00017	\$1,510	Y	0.0005	Y	1	34	0.005763816	\$51,205.74	T
904982	\$846,396	\$5,066,418	\$1,160,000	\$7,072,814	6	O	0.00017	\$1,202	Y	0.002	Y	1	35	0.005932837	\$41,961.85	T
904984	\$850,868	\$5,066,418	\$1,160,000	\$7,077,286	7	O	0.00017	\$1,203	Y	0.002	Y	1	35	0.005932837	\$41,988.38	T
904986	\$840,918	\$5,069,603	\$1,160,000	\$7,070,520	7	O	0.00017	\$1,202	Y	0.0005	Y	1	35	0.005932837	\$41,948.24	T
904990	\$20,013,653	\$5,831,298	\$1,160,000	\$27,004,951	6	O	0.00017	\$4,591	Y	0.002	Y	1	35	0.005932837	\$160,215.96	T
910006	\$3,063,473	\$2,603,737	\$2,900,000	\$8,567,210	7	S	0.00011	\$942	Y	0.002	Y	1	38	0.004171505	\$35,738.16	R
910057	\$1,346,817	\$7,005,050	\$2,900,000	\$11,251,867	7	S	0.00011	\$1,238	Y	0.0005	Y	1	38	0.004171505	\$46,937.22	R
910065	\$3,146,506	\$11,000,080	\$2,900,000	\$17,046,586	7	S	0.00011	\$1,875	Y	0.002	Y	1	38	0.004171505	\$71,109.92	R
910066	\$3,080,954	\$7,005,050	\$2,900,000	\$12,986,004	7	S	0.00011	\$1,428	Y	0.002	Y	1	38	0.004171505	\$54,171.18	R
910072	\$439,387	\$2,633,285	\$1,160,000	\$4,232,672	6	S	0.00011	\$466	Y	0.002	Y	1	15	0.00164873	\$6,978.53	R
910073	\$293,931	\$2,382,496	\$1,160,000	\$3,836,427	6	S	0.00011	\$422	Y	0.0001	N	1	15	0.00164873	\$6,325.23	R
910074	\$283,045	\$2,257,101	\$1,160,000	\$3,700,146	7	S	0.00011	\$407	Y	0.0005	Y	1	15	0.00164873	\$6,100.54	R
910075	\$973,919	\$2,006,312	\$1,160,000	\$4,140,231	6	S	0.00011	\$455	Y	0.0001	N	1	15	0.00164873	\$6,826.12	R
910076	\$1,003,885	\$7,899,854	\$1,160,000	\$10,063,739	6	S	0.00011	\$1,107	Y	0.0001	N	1	15	0.00164873	\$16,592.39	R
910077	\$563,047	\$7,649,065	\$1,160,000	\$9,372,111	7	S	0.00011	\$1,031	Y	0.0001	N	1	15	0.00164873	\$15,452.08	R
910081	\$4,920,162	\$56,574,258	\$2,900,000	\$64,394,420	7	S	0.00011	\$7,083	Y	0.0002	Y	1	49	0.005375795	\$346,171.19	R
914001	\$490,125	\$115,907	\$580,000	\$1,186,032	6	S	0.00011	\$130	N	0.0002	Y	1	23	0.002526941	\$2,997.03	R
914013	\$185,045	\$392,267	\$1,160,000	\$1,737,312	6	S	0.00011	\$191	N	0.0001	N	1	37	0.004061952	\$7,056.88	R
914015	\$195,650	NA	\$1,160,000	\$1,355,650	6	S	0.00011	\$149	Y	0.0005	Y	1	28	0.003075431	\$4,169.21	R
914016	\$797,396	\$1,180,345	\$1,160,000	\$3,137,741	6	S	0.00011	\$345	Y	0.0005	Y	1	37	0.004061952	\$12,745.35	R
914017	\$1,414,130	NA	\$580,000	\$1,994,130	5	S	0.00024	\$7	Y	0.0001	N	1	38	0.009079624	\$18,105.95	R
914022	\$923,701	NA	\$1,160,000	\$2,083,701	6	S	0.00011	\$229	Y	0.0002	Y	1	23	0.002526941	\$5,265.39	R
914023	\$527,758	\$1,080,701	\$580,000	\$2,188,459	6	S	0.00011	\$241	N	0.0002	Y	1	36	0.003952386	\$8,649.64	R
914024	\$453,144	\$125,886	\$580,000	\$1,159,030	6	S	0.00011	\$127	N	0.0001	N	1	35	0.003842809	\$4,453.93	R
914025	\$417,983	\$31,858	\$580,000	\$1,029,840	6	S	0.00011	\$113	N	0.0001	N	1	35	0.003842809	\$3,957.48	R
924001	\$541,012	NA	\$580,000	\$1,121,012	6	S	0.00011	\$123	Y	0.0002	Y	1	38	0.004171505	\$4,676.31	R
924002	\$439,855	NA	\$580,000	\$1,019,855	7	S	0.00011	\$112	Y	0.0002	Y	1	38	0.004171505	\$4,254.33	R
924007	\$403,802	NA	\$0	\$403,802	4	O	0.0006	\$242	Y	0.0005	N	1	29	0.023135203	\$9,342.04	R
924014	\$164,973	NA	\$0	\$164,973	7	O	0.00017	\$28	Y	0.002	Y	1	29	0.004918285	\$811.38	R
924015	\$58,123	NA	\$0	\$58,123	6	S	0.00011	\$6	Y	0.0002	Y	1	44	0.004828571	\$280.65	R
924030	\$231,743	\$1,139,520	\$2,900,000	\$4,271,263	6	S	0.00011	\$470	N	0.0002	Y	1	23	0.002526941	\$10,793.23	R
924037	\$927,657	\$4,739,182	\$2,900,000	\$8,566,839	6	S	0.00011	\$942	N	0.0002	Y	1	26	0.002856071	\$24,467.50	R
924038	\$374,834	\$3,159,847	\$2,900,000	\$6,434,680	5	S	0.00024	\$22	N	0.0005	Y	1	39	0.009317444	\$59,954.77	R
924045	\$636,325	\$1,891,432	\$1,160,000	\$3,687,756	6	S	0.00011	\$406	N	0.0005	Y	1	32	0.003514005	\$12,958.79	R
924046	\$625,438	\$2,392,050	\$1,160,000	\$4,177,489	3	S	0.0013	\$5,431	N	0.002	Y	1	22	0.028212973	\$117,859.38	R
924049	\$742,613	\$2,073,760	\$2,900,000	\$5,716,373	5	S	0.00024	\$19	N	0.002	Y	1	23	0.005054552	\$31,471.22	R
924051	\$584,351	\$1,891,432	\$1,160,000	\$3,635,783	6	S	0.00011	\$400	N	0.002	Y	1	21	0.002307461	\$8,389.43	R
924071	\$835,440	\$3,402,027	\$1,160,000	\$5,397,467	6	S	0.00011	\$594	N	0.0005	Y	1	24	0.002636663	\$14,231.30	R
924113	\$706,091	\$21,889,380	\$1,160,000	\$23,755,471	7	S	0.00011	\$2,613	N	0.002	Y	1	31	0.003404379	\$80,872.64	R
924114	\$891,136	\$21,889,380	\$1,160,000	\$23,940,515	7	S	0.00011	\$2,633	N	0.0005	Y	1	31	0.003404379	\$81,502.60	R
924115	\$1,585,053	\$21,889,380	\$1,160,000	\$24,634,432	6	S	0.00011	\$2,710	N	0.002	Y	1	31	0.003404379	\$83,864.95	R
924117	\$825,958	\$15,635,271	\$1,160,000	\$17,621,229	6	S	0.00011	\$1,938	N	0.002	Y	1	31	0.003404379	\$59,989.35	R
924141	\$540,220	\$2,652,693	\$1,160,000	\$4,352,913	7	S	0.00011	\$479	Y	0.0005	Y	1	38	0.004171505	\$18,158.20	R
924145	\$2,244,976	\$1,648,758	\$1,160,000	\$5,053,734	6	S	0.00011	\$556	N	0.002	Y	1	49	0.005375795	\$27,167.84	R
924148	\$1,447,393	\$42,352,764	\$2,900,000	\$46,700,157	7	R	0.000077	\$3,596	N	0.002	Y	1	51	0.00391945	\$183,038.93	R
924150	\$1,028,233	\$18,928,064	\$2,900,000	\$22,856,297	7	R	0.000077	\$1,760	Y	0.002	Y	1	47	0.003612598	\$82,570.62	R
924152	\$2,626,833	\$1,427,928	\$2,900,000	\$6,954,762	7	S	0.00011	\$765	Y	0.0005	Y	1	57	0.006250727	\$43,472.32	R
924153	\$1,929,857	\$1,891,189	\$2,900,000	\$6,721,047	7	R	0.000077	\$518	N	0.002	Y	1	57	0.004379551	\$29,435.17	R
924162	\$															



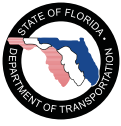
Bridge Number	Bridge Replacement Cost	Detour Cost	Loss of Life Cost	Total Cost of Failure	Scour Vulnerability	Overtopping Frequency	Annual Probability of Failure	Annual Unadjusted Risk	High Priority	MPL	Meets MPL	K1	Remaining Life	Lifetime Probability of Failure	Unadjusted Lifetime Risk	Scour Mode
924176	\$2,727,222	\$1,421,020	\$2,900,000	\$7,048,241	7	S	0.00011	\$775	Y	0.002	Y	1	65	0.00712489	\$50,217.94	R
924186	\$3,497,304	\$0	\$1,160,000	\$4,657,304	7	O	0.00017	\$792	N	0.002	Y	1	71	0.011998463	\$55,880.49	R
930004	\$36,612,817	\$8,809,220	\$2,900,000	\$48,322,037	6	R	0.000077	\$3,721	N	0.002	Y	1	22	0.001692631	\$81,791.38	T
930026	\$18,866,627	\$1,801,509	\$2,900,000	\$23,568,136	7	S	0.00011	\$2,592	Y	0.002	Y	1	15	0.00164873	\$38,857.50	T
930056	\$20,048,547	\$7,694,496	\$1,160,000	\$28,903,043	7	S	0.00011	\$3,179	Y	0.002	Y	1	35	0.003842809	\$111,068.88	T
930059	\$768,053	\$2,604,937	\$2,900,000	\$6,272,990	6	R	0.000077	\$483	N	0.002	Y	1	31	0.002384245	\$14,956.35	T
930061	\$1,546,158	\$1,377,827	\$2,900,000	\$5,823,985	7	S	0.00011	\$641	N	0.002	Y	1	41	0.004500092	\$26,208.47	T
930064	\$24,157,950	\$4,325,888	\$2,900,000	\$31,383,838	7	R	0.000077	\$2,417	N	0.002	Y	1	18	0.001385093	\$43,469.54	T
930094	\$27,155,602	\$9,894,745	\$2,900,000	\$39,950,347	6	S	0.00011	\$4,395	Y	0.002	Y	1	16	0.001758549	\$70,254.63	T
930097	\$25,045,284	\$5,508,131	\$2,900,000	\$33,453,415	4	R	0.0004	\$13,381	N	0.002	Y	1	16	0.006380836	\$213,460.75	T
930106	\$24,741,795	\$2,458,387	\$2,900,000	\$30,100,182	7	R	0.000077	\$2,318	Y	0.002	Y	1	32	0.002461061	\$74,078.40	T
930154	\$20,210,211	\$1,011,842	\$2,900,000	\$24,122,052	7	R	0.000077	\$1,857	N	0.002	Y	1	37	0.002845055	\$68,628.56	T
930157	\$55,853,501	\$4,430,804	\$2,900,000	\$63,184,304	4	R	0.0004	\$25,274	N	0.002	Y	1	15	0.005983229	\$378,046.17	T
930214	\$25,718,943	\$2,423,143	\$2,900,000	\$31,042,086	7	S	0.00011	\$3,415	Y	0.002	Y	1	33	0.003623618	\$112,484.68	T
930226	\$20,210,211	\$1,011,842	\$2,900,000	\$24,122,052	7	R	0.000077	\$1,857	N	0.002	Y	1	37	0.002845055	\$68,628.56	T
930227	\$2,205,551	\$4,604,696	\$2,900,000	\$9,710,247	6	S	0.00011	\$1,068	N	0.0005	Y	1	28	0.003075431	\$29,863.19	T
930322	\$86,447,031	\$26,385,986	\$2,900,000	\$115,733,018	6	S	0.00011	\$12,731	Y	0.002	Y	1	47	0.005156941	\$596,828.40	T
930339	\$32,057,062	\$7,877,833	\$2,900,000	\$42,834,895	7	R	0.000077	\$3,298	N	0.0005	Y	1	41	0.003152143	\$135,021.72	T
930349	\$32,008,942	\$1,229,194	\$2,900,000	\$36,138,135	7	R	0.000077	\$2,783	Y	0.002	Y	1	48	0.00368932	\$133,325.14	T
934347	\$630,425	\$3,847,884	\$2,900,000	\$7,378,309	7	S	0.00011	\$812	Y	0.002	Y	1	55	0.006032066	\$44,506.45	T
934408	\$16,418,117	\$8,969,655	\$2,900,000	\$28,287,772	4	S	0.0005	\$14,144	Y	0.002	Y	1	15	0.007473807	\$211,417.34	T
934464	\$1,062,570	\$905,506	\$2,900,000	\$4,868,076	7	S	0.00011	\$535	Y	0.0002	Y	1	32	0.003514005	\$17,106.44	T
934908	\$48,368,633	\$3,307,432	\$2,900,000	\$54,576,064	7	R	0.000077	\$4,202	Y	0.0005	Y	1	53	0.004072841	\$222,279.61	T
936653	\$195,858	NA	\$580,000	\$775,858	6	S	0.00011	\$85	Y	0.0005	Y	1	21	0.002307461	\$1,790.26	T
940007	\$1,298,558	\$3,872,455	\$2,900,000	\$8,071,013	7	S	0.00011	\$888	N	0.002	Y	1	29	0.003185092	\$25,706.92	R
940015	\$769,747	\$1,949,927	\$1,160,000	\$3,879,674	6	S	0.00011	\$427	Y	0.0005	Y	1	25	0.002746373	\$10,655.03	R
940029	\$1,646,976	\$393,395	\$1,160,000	\$3,200,370	5	S	0.00024	\$11	N	0.0005	Y	1	28	0.006698272	\$21,436.95	T
940045	\$37,635,582	\$23,168,506	\$2,900,000	\$63,704,088	6	R	0.000077	\$4,905	N	0.0005	Y	1	29	0.002230594	\$142,097.99	T
940067	\$416,959	\$154,226	\$1,160,000	\$1,731,185	6	S	0.00011	\$190	N	0.002	Y	1	24	0.002636663	\$4,564.55	R
940094	\$50,501,176	\$12,168,165	\$2,900,000	\$65,569,341	7	R	0.000077	\$5,049	N	0.0005	Y	1	40	0.00307538	\$201,650.63	T
940157	\$2,007,802	\$22,705,946	\$2,900,000	\$27,613,748	9	R	0.0000011	\$30	Y	0.0005	Y	1	73	8.02968E-05	\$2,217.30	R
940158	\$1,016,434	\$2,834,004	\$1,160,000	\$5,010,438	8	S	0.0000022	\$11	Y	0.002	Y	1	74	0.000162787	\$815.63	R
945007	\$239,266	\$228,823	\$1,160,000	\$1,628,088	6	S	0.00011	\$179	N	0.0005	Y	1	27	0.002965757	\$4,828.51	R



Appendix B

The following items are included in this Appendix:

- List of Historical Bridge Standard Drawings

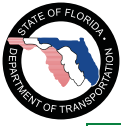


Please contact Charles Boyd at charles.boyd@dot.state.fl.us to report problems with this index.

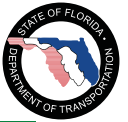
Index Number	Sheet Number or suffix	Date	Sheet Title	Sheet Subtitle
227		1919	Standard Wooden Truss-48 Foot Span	
497		1921	Standard Wood Truss-16'-0" Roadway	
535		1922	Standard Wood Bridge-20'-0" Roadway	
563	1 of 1	1922	Standard Concrete Slab Bridges-Span 8 ft to 20 ft-20 ft Roadway	Details of Existing Structures
581		1922	Standard Wood Bridge-18'-0" Roadway	
566		1926	Standard Concrete Box Culvert Spans 6'-0" to 10'-0"	
693	3	1926	Standard Slab Bridges	Reference Drawing No. 563
693	2	1926	Standard Slab Bridges	Reference Drawing No. 563
693	1	1926	Standard Slab Bridges	Reference Drawing No. 563
701		1927	Standard Slab Bridges	
722	1 of 2	1927	Standard Slab Bridges ~ Superstructure	Details of Existing Structure
723	3	1927	Standard Concrete Handrail	
724		1927	Standard Concrete Four Pile Bents	
722	2 of 2	1928	Standard Slab Bridges ~ Substructure	
792		1928	45' I-Beam Span Concrete Floor 20'-0" Roadway	
754	4	1929	Superstructure Details	
825		1930	Concrete Slab Approach	
837		1931	Double 6' x 5' x 46' Concrete Culvert for 4 : 1 Slopes	
839		1931	Standard Endwalls for Box Culverts	For Paved Sections .8' Cov.
844	2 of 2	1931	Slab Bridges ~ Substructure 16'-0" Span 24'-0" Roadway	
844	1 of 2	1931	Slab Bridges ~ Substructure 24' Roadway	
755	2 of 2	1932	Standard Timber Bridge - 20' RDWY.	
755	1 of 2	1932	Standard Timber Bridge - 20' RDWY.	
826	1 of 2	1932	Standard Timber Bridge - 24' RDWY	15' Span
854		1932	Standard Timber Pile Bent	
859		1932	Superstructure for Standard I-Beam Span Span 25'-0" 24'-0" Roadway	
861	2 of 2	1932	Superstructure Details Standard I-Beam Span 28'-0" Span 20'-0" Roadway	
861	1 of 2	1932	Superstructure Details Standard I-Beam Span 28'-0" Span 20'-0" Roadway	
884	2 of 2	1932	Standard Timber Bridges 24' RDWY	18' Span
884	1 of 2	1932	Standard Timber Bridges 24' RDWY	18' Span
889	2 of 2	1932	Concrete D.G. Superstructure 24' Roadway 30'-0" Span	Design Loading 2-Typ. 15 Ton Trucks Plus 30% Impact
899	1 of 2	1932	Concrete Pile Bent Superstructure 30' Rdway. 2-5' Sidewalks 30'-0" Span	
899	2 of 2	1932	Concrete D.G. Superstructure 30' Rdway. 2-5' Sidewalks 30'-0" Span	
924	1 of 1	1932	Standard Timber Bridge	15' Span 20' RDWY.
940	1 of 3	1932	270'-0" Swing Span ~ 24'-0" Roadway	
940	2 of 3	1932	270'-0" Swing Span ~ 24'-0" Roadway	
940	3 of 3	1932	270'-0" Swing Span ~ 24'-0" Roadway	
918		1933	Standard I-Beam Superstructure Span 20'-0" 24'-0" Roadway	
971		1933	Standard Timber Pile Bent	
976		1933	Sextuple Concrete Box Culvert	Spans 6'-0" , 8'-0" AND 10'-0" 1½ : 1 Slope
993		1933	Standard Concrete D.G. Superstructure 23' -0" Span 24'-0" Roadway	
1005	2 of 2	1933	159'-11 3/4" Span-24' Roadway	
1005	1 of 2	1933	159'11¾" Span - 24' Roadway	
1008		1933	Concrete Culvert	1 1/2 : 1 Slopes-6',8',10' Spans
1010	1 of 1	1933	Standard I-Beam Superstructure-25'-0" Span-24'-0" Roadway	For Use on Construction over Salt Water
1022	2 of 2	1933	120'-0 1/4" Span-24' Roadway	
1022	1 of 2	1933	120'-0¼" Span - 24' Roadway	
1026	1 of 2	1933	120'-0" Truss Span 24' Roadway	
1026	2 of 2	1933	120'-0" Truss Span 24' Roadway	
1038	3 of 3	1933	283'-11 1/2" Swing Span-24' Rdwy	
1038	2 of 3	1933	283'-11 1/2" Swing Span-24' Rdwy	
1038	1 of 3	1933	283'-11 1/2" Swing Span-24' Rdwy	
889	1 of 2	1934	Concrete (5 Pile) Substructure 24' Roadway 30'-0" Span	
1033	1 of 1	1934	Cantilever Suspended Type I-Beam Superstr-Spans: 66',83',66',-Rdwy:24'-0"-8" Concrete Slab	



1042	2 of 2	1934	I-Beam Span Superst. Details-25'-0" Span-24'-0" Roadway	For use on Salt Water Construction
1042	1 of 2	1934	I-Beam Span-Superstructure Details-25'-0" Span-24'-0" Roadway	
1044	2 of 2	1934	Standard I-Beam Superstructure-20'-0" Span-24'-0" Roadway	For use on Salt Water Construction
1044	1 of 2	1934	Timber Pile Bent	
1046	1 of 2	1934	Standard Timber Pile Bent	
1046	2 of 2	1934	Standard I-Beam Superstructure Span 25'-0" 24'-0" Roadway	
1047	2 of 2	1934	Standard I-Beam Superstructure Span 20'-0" 24'-0" Roadway	
1050	1050	1934	Standard Cypress Bridge	15' Span 24' RDWY
1059		1934	Concrete (5-Pile) Substructure 24'-0" Roadway 33'-0" Span	For Details Superstructure See Index No. 933
1064		1934	Standard I-Beam Superstructure Span 20'-0" 24'-0" Roadway	
1075	2 of 2	1934	Standard I-Beam Superstruct. Span 28'-0" 24'-0" Roadway	
1075	1 of 2	1934	Standard I-Beam Superstruct. Span 28'-0" 24'-0" Roadway	
1077		1934	Standard I-Beam Superstructure Span 25'-0" 24'-0" Roadway	
1098	2 of 2	1934	Standard I-Beam Superstruct. Span 20'-0" 24'-0" Roadway	
1098	1 of 2	1935	Standard I-Beam Superstruct. Span 20'-0" 24'-0" Roadway	
1124		1935	Standard I-Beam Superst.	Cantilever-Suspended Type Spans: 66'-83'-66' RDWY.: Slab 7½" for use over Fresh Water
1129		1935	U-Endwalls for Pipe Culverts	
1130		1935	Standard I-Beam Superstructure Span 40'-0" 24' Roadway	
1154		1935	Cantilever-Suspended Type I-Beam Supers. 20' RDWY. 56'-70'-56' Spans 7½" Slab	
1195	5	1935	Concrete D.G. Superstructure 36' Span 24' Roadway	
826	2 of 2	1936	Standard Timber Bridge - 24' RDWY	15' Span
947	1 of 2	1936	Details for I Beam Span Span = 45'-0" Roadway = 24'-0"	Details of Superstructure
1047	1 of 2	1936	Timber Pile Bent use with Superstructure - Index 1047 for Construction over Salt Water	
1050	2 of 2	1936	Standard Cypress Bridge	15'-0" Span 24'-0" RDWY
1058	1 of 2	1936	Standard Timber 4-Pile Bent for Construction over Fresh Water	
1149		1936	Concrete Deck Girder 24' Roadway 36' Span	
1159		1936	Standard Timber Pile Bent 4 Piles 20' Roadway	
1160		1936	I-Beam Superstr. For Salt Water Constr. 25'-0" Span 20'-0" Roadway	
1226		1936	Miscellaneous Bridges	Substructure and Superstructure
1231	3 of 3	1936	180'-0" Swing Span-24'-0" Rdwy	
1231	2 of 3	1936	180'-0" Swing Span-24'-0" Rdwy	
1231	1 of 3	1936	180'-0" Swing Span-24'-0" Rdwy	
1246		1936	Standard 26 ft Superstructure	Details of 26' Superstructure
1247		1936	Standard 32 ft Superstructure	Details 32' Superstructure
1265	1 of 1	1936	Standard Concrete D.G. Superstructure-38'-0" Span-24'-0" Roadway	
1275	2 of 2	1936	Standard I-Beam Superstructure-25'-0" Span-Skew 30° Rt Fwd-24'-0" Rdwy	
947	2 of 2	1937	Details for I Beam Span Span 45'-0" Roadway 24'-0"	Details of Superstructure
1058	2 of 2	1937	Standard I-Beam Superstructure 15'-0" Span 24'-0" Roadway	
1092		1937	Standard I-Beam Superstructure Span 39'-0" 24'-0" Roadway	
1121		1937	Standard I-Beam Superstructure Span 40'-0" 24' Roadway	
1297	2 of 3	1937	220'-0" Swing Span-24' Rdwy	
1297	1 of 3	1937	220'-0" Swing Span-24' Rdwy	
1297	3 of 3	1937	220'-0" Swing Span-24' Rdwy	
1312	1 of 1	1937	Stnd. 36' I-Beam Superstr.	
1318	1 of 1	1937	Steel H-Pile Bent-24 ft Roadway	
1319	1 of 1	1937	Standard 25' I-Beam Span-24' Roadway-Fresh Water Construction	
1322	1 of 1	1937	Treated Timber Pile Bent	24 ft Roadway
1323	1 of 1	1937	Standard I-Beam Superstructure-25'-0" Span-24'-0" Roadway	
1324	1 of 1	1937	Standard 6 Pile Bent (Treated Timber)	26 ft Roadway
1325	1 of 1	1937	Standard 25' I-Beam Span-26' Rdwy-Fresh Water	



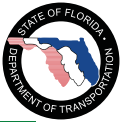
1333	1 of 1	1937	Treated Timber Pile Bent	24 ft Roadway
1334	1 of 1	1937	Stand. 20' I-Beam Span-24'-0" Roadway-Fresh Water	
1339	1 of 1	1937	Standard 20 ft I-Beam Span-28 ft Roadway-Fresh Water	
1342	1 of 1	1937	Standard Slab Bridge-10 ft Span-28 ft Roadway	
1349	1 of 1	1937	Standard 25 ft I-Beam Span-24 ft Roadway-Fresh Water	
1350	1 of 1	1937	Standard 6 Pile Bent (Treated Timber)	24 ft Roadway
1354	1 of 1	1937	Standard Slab Bridge-10 ft Span-28 ft Rdwy. Skew=30° Rt. Fwd.	
1364		1937	Standard Steel H-Pile Bent-24 ft Roadway	
1365		1937	Standard 34' I-Beam Span-24' Roadway-Fresh Water	
1366		1937	Standard Endwall for Pipe Culverts	
1367		1937	70' Deck Plate Girder Span-24'-0" Roadway-Fresh Water	
1043		1938	Standard Guard Rail-"Empire" Type	
1244	1 of 1	1938	Concrete Handrail	Type "C"
1338	1 of 1	1938	Standard 5-Pile Steel Bent-24 ft Roadway	
1373	1 of 1	1938	Standard Conc. D.G. Superstructure-26'-0" Span-24'-0" Roadway	
1374	1 of 1	1938	Standard Conc. D.G. Superstructure-32'-0" Span-24'-0" Roadway	
1376	1 of 1	1938	Standard Conc. D. G. Superstructure 30'-0" Span 24'-0" Roadway	
1378	1 of 1	1938	Standard 25 Ft. I-Beam Span 24 Ft. Roadway - Fresh Water	
1381	3 of 3	1938	Trunnion Type Bascule 80'-0" Clear Channel Opening 24'-0" Roadway 1-5'-0" Sidewalk	Details of Main Girder
1381	2 of 3	1938	Trunnion Type Bascule 80'-0" Clear Channel Opening 24'-0" Roadway 1-5'-0" Sidewalk	Details of Main Girder
1381	1 of 3	1938	Trunnion Type Bascule 80'-0" Clear Channel Opening 24'-0" Roadway 1-5'-0" Sidewalk	
1392	2 of 2	1938	Std. Conc. D.G. Superstr. 30 Ft. Span 24 Ft. RDWY.	
1392	1 of 2	1938	Standard Pile Bent 30' Span - 24' Roadway	
1395	2 of 2	1938	Standard Concr. D.G. Superstruct. 35 Ft. Span 26 Ft. Roadway	
1395	1 of 2	1938	Concrete Pile Bent 35 Ft. Span - 26 Ft. RDWY.	
1398	1 of 1	1938	Standard I-Beam Superstructure-20'-0" Span-24'-0" Roadway	
1401	1 of 1	1938	Standard I-Beam Superstructure-53 ft Span-24 ft Roadway	
1402	1 of 1	1938	Standard I-Beam Superstructure-45 ft Span-24 ft Roadway	
1407	1 of 1	1938	Standard I-Beam Superstructure-70 ft Span-24 ft Roadway	
1408	1 of 1	1938	Standard Approach Slab-No Skew-Spillway-24' Roadway	
1409	1 of 1	1938	Standard Steel H-Pile Bent-24' Rdwy	
1410	1 of 1	1938	Standard I-Beam Superstructure-45 ft Span-24 ft Roadway	
1420	1 of 1	1938	Standard 5 Pile Bent (Treated Timber)	24 ft Roadway
1421	1 of 1	1938	Standard 25 Ft. I-Beam Span 24 Ft. Roadway Fresh Water	
1425	1 of 1	1938	Standard 36 ft I-Beam Superstructure-Freshwater-24 ft Roadway	
1427	1 of 1	1938	Steel H-Pile Bent-36 ft Span-24 ft Roadway	Fresh Water Construction
1433	1 of 1	1938	Standard I-Beam Superstructure for Widening Existing Timber Bridges-15'-0" Span-28'-0" Roadway	
1440	1 of 1	1938	Pile Lagging for 10" Steel Piles	
1441	1 of 1	1938	Standard I-Beam Superstructure 15'-0" Span 24'-0" RDWY.	
1442	1 of 1	1938	Steel H-Pile Bent 36 Ft. Span 24 Ft. R'DW'Y Treated Timber Bulkhead	
1451	1 of 1	1938	Steel H-Pile Bent 36 Ft. Span 24 Ft. R'DW'Y. Salt Water Constr.	
1457	1 of 4	1938	Bob Tail Swing Span	Typical Sections Through Span
1457	2 of 4	1938	Bob Tail Swing Span	Long Arm of Main Girder
1457	3 of 4	1938	Bob Tail Swing Span	Short Arm of Main Girder
1457	4 of 4	1938	Bob Tail Swing Span	Flooring Details at Ends of Swing Span
1476	1 of 1	1939	Standard 25 Ft. I-Beam Span 28 Ft. Roadway Fresh Water	
1477	1 of 1	1939	Standard Concrete Pile Bent using 14"Sq. Piles, 28' Roadway, 25' Span	
1478	1 of 1	1939	Standard 5 Pile Bent (Treaded Timber)	28 Ft. Roadway
1480	1 of 2	1939	Standard Concrete Pile Bent 25' Span - 30' RDWY.	
1480	2 of 2	1939	Standard Concrete D.G.Superstr. 25' Span - 30' RDWY.	
1484	1 of 1	1939	Standard I-Beam Superstructure 36' Span 28' Roadway	
1485	1 of 1	1939	Steel H-Pile Bents for use with Index 1484 36 Ft. Span 28 Ft. Roadway Fresh Water Constr.	



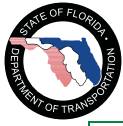
1486	1 of 1	1939	Standard I-Beam Superstructure 70' Span 28' Roadway	
1490	1 of 1	1939	Standard Slab Superstructure ~ 15 Ft. Span	
1491	1 of 1	1939	Standard H-Pile Abutment for 15 Ft. Slab Span - 24' & 26' Roadway	
1492	1 of 1	1939	Standard H-Pile Intermediate Bent for 15 Ft. Slab Span - 24 Ft. Roadway	
1502	1 of 1	1939	Standard 36' I-Beam Superstructure ~ 24'-0" Roadway	Superstructure for Fresh or Salt Water Construction (See General Plan & Elevation)
1505	1 of 1	1939	Treated Timber substructure	
1511	1 of 4	1939	Standard 36' I-Beam Superstructure-24' Roadway	Superstructure for Salt Water Construction
1511	2 of 4	1939	Standard 36' I-Beam Superstructure ~ 24' Roadway	Superstructure for Salt Water Construction (Span Adjoining Swing Span)
1511	4 of 4	1939	End, Intermediate & Tower Bents 36 Ft. Span - 24 Ft. RDWY.-Salt Water	
1513	1 of 6	1939	Plate Girder Swing Span-210 ft C-C End Wedges-24' Rd'y	Machinery Layout
1513	2 of 6	1939	Plate Girder Swing Span-210 ft C-C End Wedges-24' Rd'y	Typical Sections Thru Span
1513	3 of 6	1939	Plate Girder Swing Span-210 ft C-C End Wedges-24' Rd'y	Main Girder
1513	4 of 6	1939	Plate Girder Swing Span-210 ft C-C End Wedges-24' Rd'y	Main Girder
1513	5 of 6	1939	Plate Girder Swing Span-210 ft C-C End Wedges-24' Rd'y	Machinery Details
1518	2 of 2	1939	Standard I-Beam Superstructure-25'-0" Span-Skew 30° Lt Fwd-24'-0" Rdwy	
1518	1 of 2	1939	Standard I-Beam Superstructure 25'-0" Span ~ 30° Skew Lt. FWT 24'-0" RDWY	
1524	1 of 3	1939	Trunnion Type Bascule	Stresses and Member Sizes
1524	2 of 3	1939	Trunnion Type Bascule	Longitudinal Girder
1524	3 of 3	1939	Trunnion Type Bascule	Longitudinal Girder
1527	1 of 1	1939	Standard Slab Superstructure 15 Ft. Span - 30 Ft. RDWY.	
1522	1 of 1	1940	Standard I-Beam Superstructure 48 Ft. Span 24 Ft. Roadway	
1529	1 of 1	1940	Standard 39' I-Beam Span Superstr. 28 Ft. Roadway 4 Ft. Sidewalk	
1530	1 of 1	1940	Standard Steel Pile Bent 28 Ft. Roadway 4 Ft. Sidewalk	
1532	1 of 4	1940	Plate Girder Swing Span 150 Ft. C.-C. End Wedges - 28 Ft. R'DW'Y.	General Layout
1532	2 of 4	1940	Plate Girder Swing Span 150 Ft. C.-C. End Wedges - 28 Ft. R'DW'Y.	Typical Section Thru Span
1532	3 of 4	1940	Plate Girder Swing Span 150 Ft. C.-C. End Wedges - 28 Ft. R'DW'Y.	Longitudinal Girder
1532	4 of 4	1940	Plate Girder Swing Span 150 Ft. C.-C. End Wedges - 28 Ft. R'DW'Y.	Machinery Layout
1538	1 of 1	1940	Five Pile Steel Bent 24' RDWY	
1544	1 of 1	1940	Span Adjoining Bascule	
1548	1 of 1	1940	Standard 25 Ft. I-Beam Span 24 Ft. Roadway - Salt Water	
1550		1940	Standard 25 ft I-Beam Span-24' Rdwy for Salt & Fresh Water Construction	
1551	1 of 1	1940	Steel H-Pile Bent-25 ft Span-24 ft Roadway-Salt or Fresh Water Constr.	
1556	1 of 1	1940	Standard I-Beam Superstruct.-30 ft Span-Freshwater-28 ft Roadway	
1558	1 of 6	1940	Plate Girder Swing Span-220' C-C End Wedges-24 ft Roadway-5' Sidewalk	Table of Stresses, Est. Quant. And Gen'l Notes
1558	2 of 6	1940	Plate Girder Swing Span-220' C-C End Wedges-24 ft Roadway-5' Sidewalk	General Layout
1558	3 of 6	1940	Plate Girder Swing Span-220' C-C End Wedges-24 ft Roadway-5' Sidewalk	Typical Sections Thru Roadway
1558	4 of 6	1940	Plate Girder Swing Span-220' C-C End Wedges-24 ft Roadway-5' Sidewalk	Details of Long Girder
1558	5 of 6	1940	Plate Girder Swing Span-220' C-C End Wedges-24 ft Roadway-5' Sidewalk	Details of Long Girder
1558	6 of 6	1940	Plate Girder Swing Span-220' C-C End Wedges-24 ft Roadway-5' Sidewalk	Machinery Details
1559	3 of 3	1940	Details of Span Adjoining Swing Span	
1559	1 of 3	1940	Standard 39' I-Beam Span Superstr.-24' Roadway-5'-0" Sidewalk	Salt Water Construction
1560	1 of 2	1940	Concrete Pile Bents-24' Roadway-5' Sidewalk	Salt Water Construction
1564	1 of 4	1940	208' Swing Span-24' Roadway	Table of Stresses, Member Diagram, General Notes and Est. Quantities
1564	2 of 4	1940	208' Swing Span-24' Roadway	Typical Sections Thru Roadway



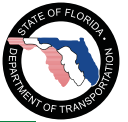
1568	1 of 1	1940	Standard Slab Superstructure-10 ft Span-24 ft Roadway	
1569	1 of 1	1940	Standard Conc. Handrail for Use on 15' Slab Spans	
1570	1 of 1	1940	Treated Timber Substructure	
1575	1 of 5	1940	Plate Girder Swing Span 170' C-C End Wedges 24 Ft. Roadway 5 Ft. Sidewalk	Table of Stresses, Est. Quant. And Genl. Notes
1575	2 of 5	1940	Plate Girder Swing Span 170' C-C End Wedges 24 Ft. Roadway 5 Ft. Sidewalk	General Layout
1575	3 of 5	1940	Plate Girder Swing Span 170' C-C End Wedges 24 Ft. Roadway 5 Ft. Sidewalk	Typical Section Thru Roadway
1575	4 of 5	1940	Plate Girder Swing Span 170' C-C End Wedges 24 Ft. Roadway 5 Ft. Sidewalk	Details of Longitudinal Girder
1575	5 of 5	1940	Plate Girder Swing Span 170' C-C End Wedges 24 Ft. Roadway 5 Ft. Sidewalk	Machinery Layout
1582	1 of 2	1940	Standard 43' Span I-Beam Superstr. 24' Roadway 5' Sidewalk	
1583	1 of 3	1940	Trunnion Type Bascule	General Layout and Estimated Quant.
1583	2 of 3	1940	Trunnion Type Bascule	Longitudinal Girder
1583	3 of 3	1940	Trunnion Type Bascule	Longitudinal Girder
1589	1 of 1	1940	Standard 15 Foot Span Slab Superstructure	
1591	1 of 1	1940	Standard Concrete Pile Bent-14" Sq. Piles, 26' Rdwy, 15 Span	(Freshwater Construction)
1631	1 of 1	1940	Standard Timber Bridge-One Lane	
1636	1 of 1	1940	Approach Slab	
1637	1 of 1	1940	Standard 40' I-Beam Superstructure-44 ft Roadway-5 ft Sidewalk	
1639	1 of 1	1940	28' Roadway Superelevated Section	Approach Slab
1645	1 of 1	1940	Standard Steel H-Pile Bent-8" @ 36# HP-26' Rdwy-15' Span	Freshwater Construction
1646	1 of 1	1940	Concrete Pile Bents-44' Roadway-5'-0" Sidewalk	
1740	2 of 2	1940	Plate Girder Swing Span-220' C.C. End Wedges-24 ft Roadway-2~4 ft Sidewalks	Typical Sections Thru Roadway
1740	1 of 2	1940	Plate Girder Swing Span-220' C.C. End Wedges-24 ft Roadway-2~4 ft Sidewalks	General Layout
1765	1 of 5	1940	Plate Girder Swing Span 220' C.C. End Wedges-24 ft Roadway-2~3'-3" Sidewalks	Table of Stresses, Estimated Quantities and General Notes
1765	2 of 5	1940	Plate Girder Swing Span 220' C.C. End Wedges-24 ft Roadway-2~3'-3" Sidewalks	General Layout
1765	3 of 5	1940	Plate Girder Swing Span 220' C.C. End Wedges-24 ft Roadway-2~3'-3" Sidewalks	Typical Sections Thru Roadway
1765	4 of 5	1940	Plate Girder Swing Span 220' C.C. End Wedges-24 ft Roadway-2~3'-3" Sidewalks	Details of Longitudinal Girder
1653	1 of 1	1941	Standard 36' I-Beam Span Superstr. 34' Roadway Two 5' Sidewalks	
1656	1 of 1	1941	Steel Pile Substructure 34' Roadway 36' Span	
1659	1 of 1	1941	Standard 15 Foot Span Slab Superstructure	Fresh Water Construction
1663	1 of 1	1941	Concrete Pile Substructure 34' Roadway ~ 36' Span	
1664	1 of 1	1941	Standard 36' I-Beam Span Superstr. 24' Roadway 4'-0" Sidewalk	
1665	1 of 1	1941	Concrete Pile Bents 24' Roadway - 4' Sidewalk	
1669	1 of 1	1941	Standard 30' I-Beam Span Superstr. 44' Roadway Two 5' Sidewalks	
1670	1 of 1	1941	Concrete Pile Bents - 44' R'W'D'Y Two 5' Sidewalks	
1671	1 of 1	1941	Concrete Pile Bent for 15 Ft. Slab Superstructure	
1672	1 of 1	1941	Standard 15 Ft. Span Slabs 2 - 5 Ft. Sidewalks	
1673	1 of 1	1941	Concrete Pile Bent for 15 Ft. Slab Superstructure	
1676	1 of 1	1941	Steel Pile Bent for 15 Ft. Slab Span Superstructure	
1680	1 of 1	1941	Standard 15 Ft. Slab Superstructure - 2 - 5 Ft. Sidewalks	
1681	1 of 1	1941	Standard Concrete Pile Bent 16" Sq. Piles, 44' RDWY., 2-5' Sidewalks	
1683	1 of 1	1941	Standard Steel Pile Bent 15' Slabs ~ 24 Ft. RDWY.	
1686	1 of 1	1941	Standard Timber Pile Bent with Concrete Cap-24' Rdwy-H:15 Loading	
1692	1 of 1	1941	28 ft Roadway-Superelevated Section with One 5 ft Sidewalk	Approach Slab
1695	1 of 1	1941	Standard 32 ft Span Concrete Deck Girder Superstructure	28 ft Roadway-H-20 Loading-Salt water Construction
1701	1 of 1	1941	Treated Timber Substructure	
1716	1 of 1	1941	Timber - Concrete - Composit Deck - 18 Ft. Span - 24 Ft. RDWY.	



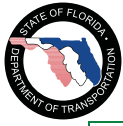
1718		1941	Standard Substructure Details for Widening Exist. Timber Bridges	
1719	1 of 1	1941	Standard Timber Truss-60 ft Span-20 ft Roadway	
1727	1 of 1	1941	Standard Timber Truss-50 ft Span-24 ft Roadway	
1738	1 of 1	1941	Standard Concr. D.G. Superstr.-30 ft Span-24 ft Rdwy-4 ft Sidewalk	
1716	1 of 1	1942	Timber Concrete Composite Deck-24 ft Roadway-18 ft Span	
1745	1 of 1	1942	Details of Concrete Pile Bents	For use with Superstructure, Index No. 1738
1759	1 of 2	1942	Standard Conc. D. G. Superstr. 30 Ft. Span 24 Ft. Roadway	
1759	2 of 2	1942	Standard Conc. Pile Bents 30 Ft. Span 24 Ft. Roadway	
1764	1 of 1	1942	Concrete Pile Bents 24' Roadway; 2'-3'-3" Sidewalk	
1765	5 of 5	1942	Plate Girder Swing Span 220' C-C End Wedges 24 Ft. Roadway 2'-3'-3" Sidewalk	
1766	1 of 2	1942	Standard 36 ft I-Beam Span Superstructure-24 ft Roadway-2~3'-3" Sidewalks	Salt Water Construction
1771	1 of 1	1942	St'n'd Timber Pile Bent with Concrete Cap	
1772	1 of 1	1942	Standard Slab Superstructure-15 ft Span: 20',22',24' &26' Rdwy Sidewalk	20' to 26' Roadway-Salt Water Construction
1774	1 of 1	1942	Standard Slab Superstructure-15 ft Span-24 ft Roadway Sidewalk	For Fresh Water Construction
1781	1 of 1	1942	Standard Slab Superstructure-15 ft Span-24 ft Roadway	H2O Salt Water Construction
1782	1 of 2	1942	Concrete Pile Bents-24' Roadway-2~3'-3" Sidewalks	End and Intermediate Bents
1782	2 of 2	1942	Concrete Pile Bents-24' Roadway-2~3'-3" Sidewalks	Details of Tower Bents
1783	1 of 3	1942	Standard Conc. D.G. Superstructure-36'-0" Span-24'-0" Roadway-2~3'-3" S. Walks	
1783	2 of 3	1942	Details of Span Adjacent Swing Span, Details of Safety Gate Brackets	
1784	1 of 1	1942	Standard Conc. D.G. Superstructure-42 ft Span-24 ft Roadway	
1797	1 of 2	1942	Standard Conc. Pile Bent Substr.-26 ft Roadway-36 ft Span	
1797	2 of 2	1942	Standard Conc. D.G. Superstructure-26 ft Roadway-36 ft Span	
1799	1 of 1	1942	Standard Treated Timber Bridge-20 ft Span-10'-8" Roadway	
1800	1 of 1	1942	Standard Treated Timber Bridge 20 Ft. Span - 18'-8" Roadway	
1801	2 of 2	1942	Standard Slab Superstructure 15 Ft. Span 30 Ft. Roadway	
1801	1 of 2	1942	Standard Timber Pile Bent 15 Ft. Span 30 Ft. Roadway	
1804	2 of 2	1942	Standard Treated Timber Bridge 24 Ft. Roadway - 15 Ft. Span	
1804	1 of 2	1942	Standard Treated Timber Bridge 24 Ft. Roadway - 15 Ft. Span	
1805	2 of 2	1942	Standard Cypress Bridge 24 Ft. Roadway - 15 Ft. Span	
1805	1 of 2	1942	Standard Cypress Bridge 24 Ft. Roadway - 15 Ft. Span	
1806	2 of 2	1942	Standard Treated Timber Bridge 20 Ft. Roadway - 15 Ft. Span	
1806	1 of 2	1942	Standard Treated Timber Bridge 20 Ft. Roadway - 15 Ft. Span	
1807	2 of 2	1942	Standard 15 Ft. Span Slab Superstructure	
1807	1 of 2	1942	Standard 15 Ft. Span Slab Superstructure	
1809	2 of 2	1942	Standar Treated Timber Bridge 26 Ft. Roadway - 15 Ft. Span	
1809	1 of 2	1942	Standard Treated Timber Bridge 26 Ft. Roadway - 15 Ft. Span	
1813	2 of 2	1942	Standard Treated Timber Bridge 30 Ft. Roadway - 15 Ft. Span	
1813	1 of 2	1942	Standard Treated Timber Bridge 30 Ft. Roadway - 15 Ft. Span	
1818	1 of 1	1942	Timber-Concrete Composite Deck-26' Roadway-14' Span	
1819	1 of 1	1942	Standard Treated Timber Bulkhead-26 ft Roadway	
1820	2 of 2	1942	Standard Treated Timber Bridge-24 ft Roadway-15 ft Span	
1820	1 of 2	1942	Standard Treated Timber Bridge-24 ft Roadway-15 ft Span	
1821	1 of 1	1942	Timber-Concrete Composite Deck-26'-0" Roadway-18'-0" Span	
1870	1 of 2	1942	Standard Treated Timber Bridge 26' Roadway 15' Span	
1870	2 of 2	1942	Standard Treated Timber Bridge 26 Ft. Roadway 15 Ft.Span	
1899	2 of 2	1942	Standard Timber Bridge 20 Ft. Roadway - 15 Ft. Span	



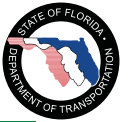
1613	E 2 of 2	1943	Standard Concrete Box Culverts	Triple 10 Ft. Span Culvert 7 Ft., 8 Ft., 9 Ft. & 10 Ft. Heights
1830	1 of 2	1943	Standard Slab Bridge-15 ft Span-30 ft Roadway	Details of Bents
1830	2 of 2	1943	Standard Slab Bridge-15 ft Span-30 ft Roadway	Details of Superstructure
1839	2 of 2	1943	Standard 25 ft I-Beam Span Superstructure -25' Rdwy-2~3 ft S.W.S.	
1850	1 of 1	1943	Standard Cypress Bridge	26' Roadway 15' Span
1853	1 of 1	1943	Std 25 ft I-Beam Span Superstr.-16" x 16" Conc. Piles-24 ft Rdwy-2~3 ft Sidewalks	
1858	1 of 1	1943	Standard I-Beam Superst.-35' and 40' Spans-26' Roadway	
1859	1 of 1	1943	Concrete Pile Bent-26 ft Roadway-15 ft Span	
1861	1 of 3	1943	Concrete Pile Bents-26 ft Roadway-30 ft Span	End and Intermediate Bents
1861	2 of 3	1943	Concrete Pile Bent-26 ft Roadway-30 ft Span	Tower Bent
1861	3 of 3	1943	Standard Conc. D.G. Superstructure-26 ft Roadway-30 ft Span	
1864	1 of 1	1943	Standard Pile Bent-15'-0" Span-30'-0" Roadway	
1868	1 of 3	1943	Standard Conc. Pile Bent Substr.-37'-6" Span-24' Rdwy-Two 3'-6" Sidewalks	Details of Intermed. And End Bents
1868	2 of 3	1943	Standard Conc. Pile Bent Substr.-37'-6" Span-26' Rdwy-Two 3'-6" S'dw'ks	Details of Tower Bent
1868	3 of 3	1943	Standard Concrete D.G. Superstr.-37'-6" Span-26' Rdwy-Two 3'-6" Sidewalks	
1871	1 of 3	1943	Standard Conc. Pile Bent Substr.-36'-0" Span-24' Rdwy-Two 3'-9" Sidewalks	End and Intermediate Bents
1871	3 of 3	1943	Standard Concrete D.G. Superstructure-36 Span-24'Rdwy-Two 3'-9" Sidewalks	
1883	1 of 2	1943	Concrete Pile Bents 26 Ft. Roadway - 35 Ft. & 40 Ft. Spans	
1883	2 of 2	1943	Concrete Pile Bents 26 Ft. R'DWAY - 35 Ft. & 40 Ft. Spans	
1860	1 of 1	1944	Standard Slab Superstructure-15 ft Span-26 ft Roadway	For Fresh Water or Salt Water Construction
1882	1 of 2	1944	Standard Conc. Pile Bent Substr.-26 ft Roadway-36 ft Span	
1882	2 of 2	1944	Standard Conc. D.G. Superstructure-26 ft Roadway-36 ft Span	
1884	1 of 1	1944	Standard Steel Pile Bent 23' & 40' Spans 26' Roadway	
1886	1 of 1	1944	Standard Steel Pile Bent 15' Slab Span 26' Roadway	
1889	1 of 2	1944	Precast Concrete Superstructure 15 Ft. Span 26 Ft. Roadway	
1889	2 of 2	1944	Concrete Pile Bent 15 Ft. Span 26 Ft. Roadway	
1899	1 of 2	1944	Standard Treated Timber Bridge 20' Roadway 15' Span	
1904	1 of 1	1944	Standard Detour Bridge	
1905	1 of 1	1944	Standard Slab Superstructure 15' Span ~ 24', 26', 28', 30' RDWY. ~ One 5' Sidewalk	
1906	2 of 3	1944	Standard Pile Bent Superstructure 31'-0" Span ~ 26' R'DW'Y ~ Two 3'-6" S'DW'KS.	Details of Tower Bent
1906	1 of 3	1944	Standard Conc. Pile Bent Substruct. 31'-0" Span - 26' RDWY - Two 3'-6" Sidewalks	Details of End and Intermediated Bents
1908	1 of 1	1944	Standard Timber Pile Bent 26 Ft. Roadway 15 Ft. Span	
1916	1 of 1	1944	Standard I-Beam Superstructure 40' Span : 26' Roadway	
1920	1 of 2	1944	Standard Concrete D.G. Superstr. 36' Span - 24' RDWY - RDWY - Two 3'-0" Sidewalks	
1693	1 of 2	1945	Standard 38' I-Beam Span Superstructure-26' Roadway	
1693	2 of 2	1945	Concrete Pile Bents-26 ft Roadway-38 ft Span	
1922	1 of 1	1945	66'-83'-66' Cantilever Suspended I-Beam Span Superstr ~ 26' RDWY	
1923	1 of 1	1945	Standard Steel Pile Bents 40' Span 26' Roadway	
1926	1 of 1	1945	70'-90'-80' Cantilever Suspended I-Beam Span Superstr ~ 26' RDWY ~ Two 3' Sidewalks	
1928	1 of 2	1945	Standard Concrete D.G. Superstr.-36'-0" Span-26' Rdwy-Two 3'-0" Sidewalks	
1928	2 of 2	1945	Standard Conc. Pile Bent Substruct.-36'-0" Span-26' Rdwy-Two 3'-0" Sidewalks	Details of Intermed. Tower and End Bents
1932		1945	Standard I-Beam Superstructure-50'-0" Span-26'-0" Roadway	
1933	1 of 1	1945	Standard Conc. D.G. Superstructure-26 ft Span-33 ft Span	
1937	1 of 2	1945	Standard Steel Pile Bent Substructure 30 Ft. Span 26 Ft. Roadway	For Salt Water Construction
1942	1 of 1	1945	Concrete Pile Bent-15 ft Span-26 ft Rdwy	
1947	1 of 1	1945	Standard Conc. D.G. Superstructure-28 ft Roadway-30 ft Span	For Salt Water and Fresh Water Construction



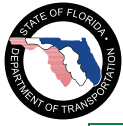
1948	1 of 1	1945	Standard Steel Pile Bent Substructure-30 ft Span-28 ft Roadway	Fresh or Salt Water Construction
1951	1 of 1	1945	Standard 15 ft Span Slab Superstructure	Fresh or Salt Water Construction
1956	1 of 2	1945	Concrete Pile Bent-25 ft Span-24 ft Rdwy	
1956	2 of 2	1945	Standard 25' I-Beam Span-24' Rdwy-Fresh Water Construction	
1964	1 of 3	1945	Standard Concrete Pile Bent Substr.-36'-0" Span-26' Rdwy-Two 3'-9" Sidewalks	End and Intermediate Bents
1964	2 of 3	1945	Standard Conc. Pile Bent Substr.-36'-0" Span-26' Rdwy-Two 3'-9" S.walks	Tower Bent
1964	3 of 3	1945	Standard Concrete D.G. Superstr.-36' Span-26' Rdwy-Two 3'-9" Sidewalks	For Fresh Water Construction
1969	1 of 1	1945	Standard Steel Pile Bent Substructure-33 ft Span-26 ft Roadway	For Fresh Water Construction
1973	1 of 1	1945	Standard I-Beam Superstructure-50'-0" Span-24'-0" Roadway	
1975	1 of 1	1945	Standard Conc. D.G. Superstructure-28 ft Roadway-33 ft Span	For Fresh or Salt Water Construction
1979	1 of 1	1945	Four Pile Concrete Bent Substruct. Intermed. And Tower Bents	28 ft Roadway-Fresh or Salt Water Construction-H15 or H20
1980	1 of 1	1945	Concrete Pile End Bent-28 ft Roadway-33 ft Span	
1985	1 of 1	1945	Standard Steel Pile Bents-15 ft Slab Span-24 ft Roadway	
1985	1 of 1	1945	Standard Steel Pile Bents-15 ft Slab Span-24 ft Roadway	
1990	3 of 3	1945	Standard Concrete D.G. Superstructure 35'-0" Span ~ 28' Roadway ~ One 3'-6" Sidewalk	
1988	1 of 1	1946	Standard Steel Pile Bent-36 ft Span-30 ft Roadway	End Bent
1989	1 of 1	1946	Standard Steel Pile Bent-33 ft Span-30 ft Roadway	End Bent
1990	2 of 3	1946	Standard Steel Pile Bent Substruct.-35'-0" Span-28'-0" Rdwy-One 3'-6" Sidewalk	Details of Intermediate Bents
1990	1 of 3	1946	Standard Steel Pile Bent Substruct.-35'-0" Span-28'-0" Rdwy-One 3'-6" Sidewalk	Details of End Bents
1996	1 of 1	1946	Standard Steel Pile Bent 33 Ft. Slab - 30 Ft. Roadway	
2004	1 of 1	1946	Standard Conc. D.G. Suprstr. 36'-0" Span 30'-0" Roadway	
2007	1 of 1	1946	Concret Pile Bent 15 Ft. Span 28 Ft. R'DW'Y.	
2009	2 of 2	1946	Standard Conr. Pile Bent 36 Ft. Span - 30 Ft. Roadway	Interm. And Tower Bents
2010	1 of 1	1946	Standard Conc. D.G. Suprstr. 36'-0 Span 30'-0" Roadway	
2011	1 of 1	1946	Standard Steel Pile Bents 15 Ft. Slab Span 28 Ft. Roadway	
2012	2 of 2	1946	Standard Steel Pile Bent 33' Span - 28' RDWY. - 2-3'-6" Walks	End Bent
2020	1 of 1	1946	Standard Concrete D.G. Superstr. 33'-0" Span, 28' RDWY., Two 3'-6" Sidewalks	
2028	1 of 1	1946	Standard 60' I-Beam Span Superstructure 30'-0" Roadway	Frech Water Construction
2036	1 of 1	1946	Standard Timber Pile Bent with Concrete Cap ~ 24'-0" RDW - 15' Span	
2041	1 of 1	1946	Standard H-Pile Abutment for 15 Ft. Slab Span ~ 28 Ft. Roadway	
2044	1 of 1	1946	Standard Steel Pile Bents 15 Ft. Slab Span ~ 26 Ft. Roadway	
2066	2 of 2	1946	Standard I-Beam Superstructure 32'-0" Span 28'-0" Roadway	
2066	1 of 2	1946	Concrete Pile Bents 24 Ft. RDWY - 32 Ft. Span	
2069	2 of 2	1946	Standard I-Beam Superstructure 32'-0" Span 28'-0" Roadway	
2069	1 of 2	1946	Concrete Pile Bents 28 Ft. RDWY - 32 Ft. Span	
2071	1A of 1	1946	Concrete Cap for Timber Piles 12' Roadway	
2071	1 of 1	1946	Standard 15 Ft. Span Slab Superstr. 12 Ft. Roadway	
2072	1 of 1	1946	Concrete Pile End Bent 28 Ft. Roadway 33 Ft. Span	
2080	1 of 1	1946	Standard Precast Concrete Pile Abutment ~ 15 Ft. Span 28 Ft. Roadway	
2083	1 of 1	1946	Widening 18 Ft. Clear Span Slab Bridge	Superstructure Details
2085	1 of 1	1946	Widening 16 Ft. Clear Span Slab Bridge	Superstructure Details
2087	2 of 2	1946	Steel Pile Bent 28 Ft. Roadway 33 Ft. Span	Intermediate and Tower Bent
2087	1 of 2	1946	Steel Pile Bent 28 Ft. Roadway 33 Ft. Span	End Bent
2093	1 of 1	1946	Standard Concrete Pile Bent 15 Ft. Span 28 Ft. Roadway	
2094	1 of 1	1946	Concrete Pile Bent 15 Ft. Span ~ 24 Ft. Roadway	
2098	1 of 1	1946	15 Ft. Span Superelevated Slab Superstructure	Special Details for 15 Ft. Slab with .03 Ft. Per Ft. Superelevation
2105	1 of 1	1946	Intermediate Bent Utilizing Existing Timber Piles	



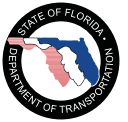
2106	1 of 1	1946	Superelevated Slab Superstructure 26 Ft. Roadway 15 Ft. Span	
2108	1 of 1	1946	Concrete Abutment 26Ft. Roadway 15 Ft. Slab Span	
2120	1 of 1	1946	Standard I-Beam Span Superstructure 62'-0" Span ~ 44' Roadway ~ 2 ~ 6' Sidewalks	
2046	2 of 3	1947	Intermediate Pile Bent 40' Span - 44' R'DW'Y. - 2-6' S'D'W'K'.	
2046	1 of 3	1947	End Pile Bent 40' Span - 44' R'DW'Y. - 2-6' S'D'W'K'.	
2046	3 of 3	1947	Standard 40' I-Beam Span Superstr. 44' Roadway Two 6'-0" Sidewalks	
2136	1 of 1	1947	Concrete Pile Bents 28 Ft. RDWY - 62 Ft. Span	End and Interm. Bents
2138	1 of 1	1947	Standard I-Beam Span Superstr. 62'-0" Span 28'-0" Roadway	
2144	1 of 1	1947	Standard Slab Superstructure-15' Span-24',26',28',30' Rdwy-Two 4' Sidewalks	
2150	1 of 1	1947	Standard Conc. D.G. Superstructure-28 ft Roadway-33 ft Span	For Fresh Water or Salt Water Construction
2150	A 1 of 1	1947	Standard Concrete D.G. Superstructure 28 Ft. Roadway 33 Ft. Span	
2156	1 of 1	1947	Concrete Pile Bent-30° Skew-15 ft Span-28 ft Roadway	
2157	1 of 1	1947	Standard I-Beam Span Superstr.-44'-0" Span-28'-0" Roadway	
2158	1 of 1	1947	Standard 15 ft Span-Slab Superstructure on 30° Skew	Fresh or Salt Water Construction
2161	1 of 1	1947	Standard 15 ft Span-Slab Superstructure	Fresh or Salt Water Construction
2168	1 of 1	1947	Standard Steel Pile Bents 15 Ft. Slab Span 28 Ft. Roadway	
2179	2 of 2	1947	Standard Concrete D.G. Superst. 36 Ft. Span Dual 26 Ft. Roadway	
2181	1 of 1	1947	Widening 8 Ft. Clear Span Slab Bridge	Superstructure Details
2183	1 of 1	1947	Standard Concrete Pile Abutment - 15 Ft. Span, 35Ft. Slab Width	Details of Intermediate Bent
2187	1 of 1	1947	Standard Concrete Pile Abutment - 15 Ft. Span, 20 Ft. RDWY.	
2191	3 of 4	1947	Single Leaf Trunnion Type Bascule	Longitudinal Girder
2191	2 of 4	1947	Single Leaf Trunnion Type Bascule	Longitudinal Girder
2191	1 of 4	1947	Single Leaf Trunnion Type Bascule	Stresses and Member Sizes
2192	1 of 1	1947	Rest Bent for Single Leaf Bascule	
2201	1 of 1	1947	Standard I-Beam Superstructure 65'-0" Span 30'-0" Roadway	
2211	1 of 1	1947	Standard Steel Pile Bents 25 Ft. Span 24 Ft. Roadway	
2218	1 of 1	1947	Superelevated Slab Superstructure-24 ft Roadway-15 ft Span	Special Details for Spans on 1° Curve
2193-A	1 of 1	1947	Details of Approach Slab for 20'-0" Roadway	
1604	E 1 of 1	1948	Single Concrete Box Culverts	4 Ft. Span - 6 Ft. Height
2184	CP40	1948	Standard Concrete Pile Bent-15 ft Span-40 ft Slab Width	Details of Intermediate Bent
2184	CP35	1948	Standard Concrete Pile Bent-15 ft Span-35 ft Slab Width	Details of Intermediate Bent
2184	SE	1948	15'-6" Span Slab Superstructure	Details of End Span
2184	SO	1948		Details of Superstructure
2223	1 of 1	1948	Details of Drainage Sump	
2224	S-S.3	1948	Standard 15 ft Span-Slab Superstructure	Special Details for Slabs-Superelevated 0.03 ft per ft
2224	CA28-2	1948	Concrete Pile Abutments-15 ft Slab Span-28' Roadway	
2224	TP24	1948	Timber Pile Bents-15 ft Span-24 ft Roadway	
2224	SE	1948	Standard 15 ft Span-Slab Superstructure	Details of Intermediate & End Spans
2224	SS428	1948	Std. 15 ft Span-28 ft Rdwy-Slab Superstructure	Special Details for Slabs to be Superelevated .04 ft per ft
2224	S	1948	Standard 15 Ft. Span Slab Superstructure	
2237	S	1948	15 ft Span Slab Superstructure	
2237	SE	1948	15 ft 6 in Span Slab Superstructure	Details of End Span
2239	S	1948	Standard 15 Ft. Span Slab Superstructure	
2239	S S E 2	1948	Standard 15 Ft. Span 28 Ft. Roadway	Special Details - Intermed. & End Spans Slab Superelevated 0.02' Per Ft.
2239	S. E.	1948	Standard 15 Ft. Span Slab Superstructure	Details of Intermediate & End Spans
2243	S. E.	1948	Standard 15 Ft. Span Slab Superstructure	Details of Intermediate & End Spans (To Be Constructed One Half at a Time)
2248	C P - 24	1948	Standard 40' I-Beam Span - 24 Ft. Roadway	Details of End Bents & Intermediate Bents
2248	S	1948	Standard 40 Ft. I-Beam Span - 24 Ft. Roadway	Superstructure Details
2251	1 of 1	1948	66'-83-66 Cantilever Suspended I-Beam Span Superstructure-24 Ft. RDWY.	
2260	1 of 1	1948	Details of Concrete Sheet Piling Bulkhead	
2270	CP24	1948	Concrete Pile Bent-25 ft Span-24 ft Roadway	



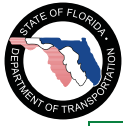
2270	S	1948	Standard 25 ft I-Beam Span-24 ft Rdwy-fresh water Construction	
2281	2 of 2	1948	Concrete D.G. Superstructure-36'-0" Span-24'-0" Roadway-2~3'-0" Sidewalks	Superelevated .03' per ft
2281	1 of 2	1948	Concrete Pile Bents-36'-0" Span-24'-0" Rdwy-2~3'-0" Sidewalks	Details of End Bents & Intermediate Bents-Superelevated .03 ft per ft
2287	CP28	1948	Standard 36 ft I-Beam Span-28 ft Roadway	Details of End Bents & Intermediate Bents
2287	S	1948	Standard 36 ft I-Beam Span-28 ft Roadway-Fresh Water	
2288	1 of 1	1948	Standard 44 ft I-Beam Span-28 ft Roadway	
2294	1 of 5	1948	Concrete D.G. Superstructure-36'-0" Span-24'-0" Roadway-2~3'-0" Sidewalks	
2297	1 of 1	1948	Standard Concrete Handrail	
2305	S	1948	Standard 50 ft I-Beam Span-28 ft Roadway-Fresh Water	
2307	TP24	1948	Timber Pile Bents-25 ft Span-24 ft Roadway	
2308	TP24	1948	Timber Pile Bents-15 ft Span-24 ft Roadway	
2308	TPA24	1948	Concrete Abutment-15 ft Span-24 ft Roadway	
2308	S	1948	Standard Slab Superstructure-15 ft Span-24 Roadway	
2321	2 of 2	1948	Standard I-Beam Superstructure-28 ft Span-28 ft Roadway-1~4 ft Sidewalk	
2321	1 of 2	1948	Concrete Pile Bents-28'-0" Span-28'-0" Rdwy-1~4'-0" S.W.	Details of End Bents and Intermediate Bents
2326	S	1948	Standard Slab Superstructure-15' Span-24 ft Roadway	
2326	TP 24	1948	Timber Pile Bents 15 Ft. Span 24 Ft. Roadway	
2797	S	1948	Standard Slab Superstructure-15' Span-24 ft Roadway	
3170	S	1948	Standard Slab Superstructure 15' Span 24 Ft. Roadway	
2184	1 of 1	1949	15 ft Span Slab Superstructure	
2224	CP24	1949	Concrete Pile Bents-15 ft Span 24 ft Roadway	
2224	CP24-5	1949	Concrete Pile Bents-15 ft Span-24 ft Roadway	Superelevated 0.05 ft per ft
2224	S-S.5	1949	Standard 15 ft Span-Slab Superstructure	Special Details for Slabs-Superelevated 0.05 ft per ft
2255	1 of 1	1949	Details of Approach Slab for 28 Ft. Roadway Superelevated	
2264	1 of 1	1949	Details of Approach Slab for 24'-0" Roadway; Superelevated	
2270	TP24	1949	Timber Pile Bents-25 ft Span-24 ft Roadway	
2304	3 of 3	1949	Concrete Deck Girder Span 36'-0" Span ~ 28'-0" RDWY. ~ 2'-3'-6" Sidewalks	Half End Elevation of 36 Ft. C.D.G. Span at Bascule Piers & at Bents Adjacent to Bascule Piers & Special Details fo Span with Safety Gate & Light Seat
2304	2 of 3	1949	Concrete Deck Gired Span 36'-0" Span ~ 28'-0" RDWY. ~ 2'-3'-6" Sidewalks	
2304	1 of 3	1949	Concrete Pile Bents 36'-0" Span ~ 28'-0" RDWY. ~ 2'-3'-6" S. W.	
2307	S	1949	Standard I-Beam Superstructure 25Ft. Span 24Ft. Roadway	
2332	CP24	1949	Concrete Pile Bent-25 ft Span-24 ft Roadway	
2334	S	1949	Standard 41 ft I-Beam Span-28 ft Roadway	
2335	CP28	1949	Standard 30 ft I-Beam Span-28 ft Roadway	Details of End and Intermediate Bents
2335	S	1949	Standard 30 ft I-Beam Span-28 ft Roadway	
2337	TP20	1949	Timber Pile Bents-15 ft Span-20 ft Roadway	
2337	S	1949	Standard Slab Superstructure-15 ft Span-20 ft Roadway	
2346	S	1949	Standard Slab Superstructure-15 ft Span-20 ft Roadway	
2346	TP20	1949	Timber Pile Bents-15 ft Span-20 ft Roadway	
2350	SP24E	1949	Steel Pile Bent-24 ft Roadway-35 ft Span	End Bent
2350	S	1949	Composite I-Beam Superstructure-35 ft Span-24 ft Roadway	
2350	CP24	1949	Concrete Pile Bents-24 ft Roadway-35 ft Span	Details of End Bents and Intermediate Bents
2350	ST24 I	1949	Steel Pile Bent-24 ft Roadway-35 ft Span	
2359	CP28	1949	Concrete Pile Bent-36 ft Span-28 ft Roadway-2~3'-6" Sidewalks	
2359	S	1949	Concrete Deck Girder Span-36'-0" Span-28'-0" Rdwy-2~3'-6" Sidewalks	
2365	1 of 1	1949	Composite I-Beam Superstucture 62 Ft. Span 24 Ft. Roadway	
2366	1 of 1	1949	Precast Units 15 Ft. Slab Spab ~ 24 Ft. Roadway	
2370	1 of 1	1949	Elementary Wiring Detail	Double Leaf Bascule
2381	2 of 2	1949	Standard I-Beam Superstructure-40'-0" Span-28'-0" Rdwy-2~3'-0" Sidewalks	
2381	1 of 2	1949	Concrete Pile Bents-28 ft Roadway-40 ft Span	Details of End Bents and Typical Intermediate Bents
2382	1 of 1	1949	Standard I-Beam Superstructure-50'-0" Span-28'-0" Rdwy-2~3'-0" Sidewalks	



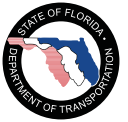
2398	S	1949	Standard Slab Superstructure-15 ft Span-31 ft Roadway	
2398	CP31	1949	Standard Concrete Pile Bent-15 ft Span-31 ft Roadway	
2401	SP28 I	1949	Steel Pile Bent-28 ft Roadway-35 ft Span	Intermediate Bent
2401	SP28E	1949	Steel Pile Bent-28 ft Roadway-35 ft Span	End Bent
2401	S	1949	Composite I-Beam Superstructure-35 ft Span-28 ft Roadway	
2405	S	1949	Concrete Deck Girder Span-36'-0" Span-28'-0" Rdwy-2~3'-6" Sidewalks	
2408	CP28	1949	Concrete Pile Bents-36'-0" Span-28'-0" Rdwy-2~3'-6" S.W.	
2409	S	1949	Composite I-Beam Superstructure-63 ft Span-28 ft Roadway	
2413	S-S-6	1949	Standard I Beam Superstructure-25 ft Span-20 ft Roadway	Special Details for Spans-Superelevated 0.06 ft per ft
2413	TP20	1949	Standard Timber Pile Bents-25 ft Span-20 ft Roadway	
2413	SP20	1949	Standard Steel Pile Bents-25 ft Span-20 ft Rdwy-Superelev. .06' per ft	
2413	S	1949	Standard I-Beam Superstructure-25 ft Span-20' Roadway	
2423	C.P. 28	1949	Concrete Pile Bents 15 Ft. Span 28 Ft. Roadway	
2433	S	1949	Composite I-Beam Superstructure-50 ft Span-28 ft Roadway	
2433	C.P. 28	1949	Concrete Pile Bents 28 Ft. Roadway 50 Ft. Span	
2931	TP20	1949	Timber Pile Bents-15 ft Span-20 ft Roadway	
2931	S	1949	Standard Slab Superstructure-15 ft Span-20 ft Roadway	
3159	CP28	1949	Concrete Pile Bents-36'-0"-28'-0" Rdwy-2~3'-6" S.W.	
2307	S-1	1950	Standard I-Beam Superstructure 24' Roadway 25' Span	Special Details for Spans on a 1°00' Curve
2337	S-4	1950	Standard Slab Superstructure-15 ft Span-20 ft Roadway	Special Details for Slabs to be Superelevated .04 ft per ft
2423	TP24	1950	Timber Pile Bents-15 ft Span-24 ft Roadway	
2423	C.P. 24	1950	Concrete Pile Bent 15 Ft. Span 24 Ft. Roadway	
2423	S-S-4	1950	15 Ft. Span Slab Superstructure 24 Ft. Roadway	
2431	S	1950	Standard I-Beam Superstructure 25 Ft. Span 20 Ft. Roadway	
2431	T.P. 20	1950	Standard Timber Pile Bents 25 Ft. Span 20 Ft. Roadway	
2433	SP 28 E	1950	Steel Pile Bent 28 Ft. Roadway - 50 Ft. Span	
2433	S.P. 28 I	1950	Steel Pile Bent 50 Ft. Span - 28 Ft. Roadway	
2446	CP28	1950	Concrete Pile Bents-36'-0" Span-28'-0" Rdwy-2~5'-0" S.W.	
2446	S	1950	Concrete Deck Girder Span-36 ft Span-28 ft Rdwy-2~5 ft Sidewalks	
2453	S	1950	Composite I-Beam Superstructure-56 ft Span-28 ft Roadway	
2454	2 of 2	1950	Steel Pile End Bent 28 Ft. Roadway 56 Ft. Span	
2454	1 of 2	1950	Steel Pile Bent 28 Ft. Roadway 56 Ft. Span	
2455	2 of 2	1950	Steel Pile End Bent 28 Ft. Roadway 35 Ft. Span	
2455	1 of 2	1950	Steel Pile Bent 28 Ft. Roadway 35 Ft. Span	
2456	1 of 1	1950	Steel Pile Bent 28 Ft. Roadway 35 Ft. & 56 Ft. Span	
2466	S	1950	Standard Slab Superstructure-15 ft Span-24 ft Roadway	
2466	CP - 24I	1950	Standard Concrete Pile Bent 15 Ft. Span ~ 24 Ft. Roadway	
2471	1 of 2	1950	Details of 65-65-65 Continuous I-Beam Spans for 20 ft Roadway	Details of 65-65-65 Continuous I-Beam Spans for 20 ft Roadway
2471	2 of 2	1950	Details of 65 - 65 - 65 Continuous I-Beam Spans for 20 Ft. Roadway	
2474	1 of 1	1950	Precast Slab Suprstructure 15 Ft. Span 28 Ft. Roadway	
2478	2 of 2	1950	Standard 50'-50'-50' Continuous I Beam Superstructure ~ 20' RDWY	
2478	1 of 2	1950	Standard 50'-50'-50' Continuous I Beam Superstructure ~ 20' RDWY	
2479	1 of 1	1950	20 Ft. Span I-Beam Bridge	
2484	1 of 1	1950	Conversion of Standard Four-Pile Timber Bent	For use with 24 ft Roadway
2504	2 of 2	1950	Standard I-Beam Superstructure 25 Ft. Span - 28' Roadway - 1 ~ 4 Ft. Sidewalk	
2522	1 of 1	1950	Precast Concrete Deck Slabs for 15 ft Span Timber Bridges	
2541	CP24 E	1950	Concrete Pile End Bent-50 ft Span-24 ft Roadway	
2541	CP24 I	1950	Concrete Pile Intermediate Bents and Tower Bent-50 ft Span-24 ft Roadway	
2541	S	1950	Composite I-Beam Superstructure 50 Ft. Span 24 Ft. Roadway	Details ~ 50' Span
2547	TP20	1950	Timber Pile Bents-15 ft Span-20 ft Roadway	
2547	S	1950	Standard Slab Superstructure 15 Ft. Span ~ 20 Ft. Roadway	
2556	CP28	1950	Concrete Pile Bents-15 ft Span-28 ft Rdwy-5'-0" SW	
2556	S	1950	Standard 15 Ft. Span Slab Superstructure with 5' Ft. Walk	
2561	CP28	1950	Standard Concrete Pile Bents-18"sq Piling-28' Roadway-35' Span	End and Intermediate Bents
2569	CP28	1950	Concrete Pile Bents-15 ft Span-28 ft Rdwy-2~1'-6" Sdwks	
2569	S	1950	Precast Slab Superstructure-15 ft Span-28 ft Roadway	



2570	S	1950	Standard 15' Span Slab Superstructure on 30° Skew	
2574	CP24	1950	Concrete Pile Bents-15 ft Span-24 ft Roadway-2~3 ft SW	
2574	S	1950	15 ft Span Superstructure-24 & 28 ft Roadway-2~3 ft SW	
2575	S	1950	Slab Superstructure 15' Span - 28' Roadway	
2588	2 of 2	1950	Composite I-Beam Superstructure-40 ft Span-28 ft Rdwy-2~4'-0" SW	Special Details of 40' Span on 1° Curve
2588	1 of 2	1950	Composite I-Beam Superstructure 40 Ft. Span 28 Ft. Roadway 2 ~ 4 Ft. S. Walks	
2588	C.P. 28	1950	Concrete Pile Bents 40'-0" Span ~ 28'-0" RDWY ~ 2-4'-0" S.W.	
2592	S	1950	Composite I-Beam Superstructure-40 ft Span-28 ft Rdwy-2~3'-6" Sidewalks	
2592	CP - 28-I	1950	Concrete Pile Bents 28 Ft. Roadway 40 Ft. Span	
2592	C.P. 28-E	1950	Concrete Pile Bent 40'-0" Span~28'-0" RDWY.~2~3'-6" Sidewalks	
2594	S	1950	Precast Slab Superstructure-15 ft Span-20 ft Roadway	
2595	S	1950	Composite I-Beam Superstructure 60 Ft. Span 28 Ft. RDWY 2 ~ 3'-6" Sidewalks	
2608	1 of 2	1950	Composite I-Beam Superstructure 60 Ft. Span 28 Ft. RDWY 2 ~ 4'-0" Sidewalks	
2608	2 of 2	1950	Composite I-Beam Superstructure 60 Ft. Span 28 Ft. RDWY 2 ~ 4'-0" S.W.	Special Details of 60' Span on 1° Curve
2610	CP28	1950	Standard Concrete Pile Bents-40 ft Span-28 ft Rdwy	
2610	S	1950	Composite I-Beam Superstructure 40 Ft. Span 28 Ft. Roadway	
2615	S	1950	Slab Superstructure-15' Span-28' Roadway-2~3' Sidewalks	
2615	CP28	1950	Concrete Pile Bents-15' Span-28' Roadway-2~3' Sidewalks	
2620	SS 5	1950	Details of 40 Ft. Span Composite I-Beam Superstructure	
2620	C.P. - 28 - S5	1950	Concrete Pile Bents 40' Span ~ 28' RDWY ~ .05' Superelevation	
2625	S	1950	Precast Slab Superstructure 15 Ft. Span 24 Ft. Roadway	
2627	TP24	1950	Timber Pile Bents-15 ft Span-24 ft Roadway	
2635	CP28	1950	Concrete Pile Bents-15 ft Span-28 ft Roadway-2~1'-6" Sidewalks	
2635	S	1950	Precast Slab Superstructure-15 ft Span-28 ft Roadway	
2639	SP28-I	1950	Steel Pile Bent-28 ft Roadway-35 ft Span	Intermediate Bent
2639	SP-28-E	1950	Standard Steel Pile Bents-10 HP 42 Piles-28' Roadway-35' Span	End Bent
2639	S	1950	Composite I-Beam Superstructure 35 Ft. Span 28 Ft. Roadway	
2642	S	1950	Precast Slab Superstructure-15 ft Span-24 ft Rdwy-2~2'-6"SW	
2644	CP28	1950	Concrete Pile Bents-15' Span-28' Rdwy-2~3 ft Sdwks	
2651	CP28	1950	Concrete Pile Bent-15 ft Span-28 ft Roadway-2~1'-6" Sdwks	
2651	S	1950	Precast Slab Superstructure 15 Ft. Span 28 Ft. Roadway	
2658	TP20	1950	Timber Pile Bents-15 ft Span-20 ft Roadway	
2658	S	1950	Standard Slab Supstructure 15 Ft. Span 30° Skew 20' Roadway	
2679	S 1 of 2	1950	25' Span ~ 24' RDWY ~ Precast Girders ~ Cast In Place Slab	
2869	S	1950	Composite I-Beam Superstructure-40 ft Span-28 ft Rdwy-2~3'-3" SW	
2877	CP28	1950	Concrete Pile Bents-33 ft Span-28 ft Roadway	Bents Nos. 3,4,5,& 6
2326	A T.P. 24	1951	Timber Pile Bents 15 Ft. Span 24 Ft. Roadway	
2437	1 of 1	1951	Standard Concrete Box Culvert	Triple 8 Ft. Span Culverts 7 Ft. 8 Ft. Heights
2615	BH28	1951	Concrete Bulkheads-15' Span-28' Roadway-2~3'-1" Sidewalks	
2670	CP 42 E	1951	Composite Pile End Bent-60 ft Span-Four Lane Roadway	
2670	S	1951	Composite I-Beam Superstructure 60 Ft. Span ~ Four Lane Roadway	
2670	C.P. 42 E	1951	Composite Pile End Bent 60 Ft. Span ~ Four Lane Roadway	
2678	1 of 1	1951	Details of 14' & 20" Octagonal Piles	
2679	CP24	1951	Concrete Pile Bents-25' Span-24' Roadway	
2681	1 of 1	1951	Slab Superstructure-15 ft Span-28 ft Roadway	
2695	T.P. 20	1951	Timber Pile Bents 25 Ft. Span ~ 20 Ft. Roadway	Superseded by Index 2698
2695	S	1951	Precast Girders ~ Cast In Place Slab 25 Ft. Span 20 Ft. Roadway	
2703	S	1951	Slab Superstructure 15 Ft. Span 52 Ft. Roadway	
2703	C.P.	1951	Concrete Pile Bents 15 Ft. Span 52 Ft. Roadway	
2710	C.P. 28	1951	Concrete Pile Bent 25 Ft. Span ~ 28 Ft. Roadway	



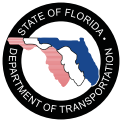
2710	S	1951	Precast Girders ~ Cast In Place Slab 25 Ft. Span 28 Ft. Roadway	
2711	S	1951	Slab Superstructure-15 ft Span-24 ft Roadway	
2715	TP24	1951	Timber Pile Bents-25 ft Span-24 ft Roadway	
2715	S	1951	Precast Girders-Cast in Place Slab-25 ft Span-24 ft Roadway	
2715	CPA	1951	Concrete Pile Abutment-25 ft Span-24 ft Roadway	
2715	CP24	1951	Concrete Pile Bents-25 ft Span-24 ft Roadway	
2721	SP28	1951	Steel Pile Bents-25' Span-28' Roadway	
2721	S	1951	Precast Girders~Cast in Place Slab-25 ft Span-28 ft Roadway	
2723	CPA	1951	Concrete Pile Abutment-25 ft Span-28 ft Roadway	
2733	CP28	1951	Concrete Pile Bents-36 ft Span-28 ft Rdwy-2~3'-6" SW	
2733	S	1951	Concrete Deck Girder Span-36 ft Span-28 ft Roadway-2~3'-6" Sidewalks	
2750	S	1951	Precast Slab Superstructure-15 ft Span-24 ft Roadway	
2752	CP28	1951	Concrete Pile End Bent-60 ft Span-28 ft Roadway	
2752	S	1951	Composite I-Beam Superstructure-60 ft Span-28 ft Roadway	
2767	1 of 1	1951	Precast Concrete Deck Slabs for 15 ft Span Timber Bridges	
2770	S	1951	Concrete Deck Girder Superstructure 40'-0" Span ~ 28'-0" RDWY ~ 2 ~ 3'-0" Sidewalk	
2771	S	1951	Precast Slab Superstructure-15 ft Span-28 ft Roadway	
2771	CP28	1951	Concrete Pile Bents-15 ft Span-28 ft Roadway	
2777	CP28	1951	Concrete Pile Bent-42 ft Span-28 ft Roadway	
2777	S	1951	Composite I-Beam Superstructure-42 ft Span-28 ft Roadway	
2778	S	1951	Composite I-Beam Superstructure-55 ft Span-28 ft Roadway	
2786	S	1951	Precast Slab Superstructure 15 Ft. Span - 28 Ft. RDWY -2-3'-1" Ft. S.W.	
2797	T.P. 24	1951	Timber Pile Bents 15 Ft. Span 24 Ft. Roadway	
2803	1 of 1	1951	Details of Approach Slab for 24 Ft. Roadway ~ 30° Skew	
2808	T.P. 24	1951	Timber Pile Bents 18 Ft. Span 24 Ft. Roadway	
2825	S	1951	Precast Slab Superstructure 15 Ft. Span 20 Ft. Roadway	
2839	1 of 1	1951	Precast Concrete Deck Slabs for 15 ft Span Timber Bridges	
2840	S	1951	Precast Girders-Cast in Place Slab-25 ft Span-28 ft Roadway	
2840	C.P. 28	1951	Concrete Pile Bents 25 Ft. Span Ft. Roadway	
2844	S	1951	Composite I-Beam Superstructure-53 ft Span-28 ft Rdwy-2~3'-0" Sidewalks	
2866	3 of 3	1951	60'-60' Continuous Composite I-Beam Superstructure-2~26' Rdwy-2~5' S.W.	
2867	1 of 3	1951	60'-90'-60' Continuous Composite I-Beam Superstructure-2~26' Rdwy-2~5' S.W.	
2867	3 of 3	1951	60'-90'-60' Continuous Composite I-Beam Superstructure-2~26' Rdwy-2~5' S.W.	
2893	5 of 5	1951	Standard Continuous 84'-126'-84' Plate Girder Superstructure	
2893	4 of 5	1951	Standard Continuous 84'-126'-84' Plate Girder Superstructure	
2893	2 of 5	1951	Standard Continuous 84'-126'-84' Plate Girder Superstructure	
2897	1 of 1	1951	Precast Concrete Deck Slabs for 15 Ft. Span Timber Bridge	
2903	S	1951	Precast Girders-Cast in Place Slab-25 ft Span-24 ft Roadway	
2903	C.P. 24	1951	Concrete Pile Bents 25' Span 24' Roadway	
2936	S	1951	Composite I-Beam Superstructure-42 ft Span-28 ft Roadway	
2937	S	1951	Composite I-Beam Superstructure-55 ft Span-28 ft Roadway	
4241	1 of 1	1951	Standard Timber Bridge	
2294	5 of 5	1952	Concrete Pile Bents-36'-0" Span-24'-0" Rdwy-2~3'-0" Sidewalks	Details of End Bents & Intermediate Bents
2844	S.P. 28 E	1952	Steel Pile End Bent 28'-0" RDWY 3'-0" Sidewalk ~ 53'-0" Span	
2854	S	1952	Standard I-Beam Superstructure-25 ft Span-28 ft Roadway	
2854	C.P. 28	1952	Concrete Pile Bents 25 Ft. Span 28 Ft. Roadway	Details of End Bents and Intermediate Bents Nos. 2 and 5
2861	TP24	1952	Timber Pile Bent-15 ft Span-24 ft Roadway	
2861	C.P. 24	1952	Concrete Pile Bent 15 Ft. Span 24 Ft. Roadway	
2861	S	1952	Slab Superstructure 15 Ft. ~ 24, 26, 28 & 30 Ft. Roadway	
2861	S-S-3_28	1952	Std. 15 Ft. Span ~ 28 Ft. RDWY Slab Suprstructure	
2866	2 of 3	1952	60'-60' Continuous Composite I-Beam Superstructure-2~26' Rdwy-2~5' S.W.	



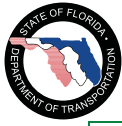
2866	1 of 3	1952	60'-60' Continuous Composite I-Beam Superstructure ~ 2-26' RDWY ~ 2-5' S.W.	
2867	2 of 3	1952	60'-90'-60' Continuous Composite I-Beam Superstructure ~ 2-26' RDWY ~ 2-5' S.W.	
2869	S.P. 28-E	1952	Steel Pile End Bent 40'-0" Span ~ 28'-0" RDWY ~ 2~3'-3" Sidewalks	
2874	CP28	1952	Concrete Pile Bents-25 ft Span-28 ft Roadway-2~3 ft Sdwks	
2874	S	1952	Precast Girders-Cast in Place Slab-25 ft Span-28 ft Rdwy-2~3'-0" Sdwks	
2877	S	1952	Concrete Deck Girder Span 33 Ft. 28 Ft. Roadway	
2878	S	1952	Concrete Deck Girder Span 25 Ft. 28 Ft. Roadway	
2879	1 of 1	1952	Approach Slab for 28 Ft. RDWY with Flared Curb and 6" Slab	
2893	3 of 5	1952	Standard Continuous 84'-126'-84' Plate Girder Superstructure	
2893	1 of 5	1952	Standard Continuous 84'-126'-84' Plate Girder Superstructure	
2922	2 of 2	1952	Concrete Slab Superstructure-20'-0" Rdwy-15'-0" Span-30° Skew	
2922	1 of 2	1952	Timber Pile Bents-20'-0" Rdwy-15'-0" Span-30° Skew	
2930	S	1952	Precast Girders-Cast in Place Slab-25' Span-28' Roadway-2° Curve-Superel. .05' per ft	
2930	S.P. 28 E	1952	Steel Pile Bents 28 Ft. Roadway ~ 25 Ft. Span ~ Superel. .05'Per Ft.	
2930	S.P. 28 I	1952	Steel Pile Bents 28 Ft. Roadway ~ 25 Ft. Span ~ Superel. .05'Per Ft.	Intermediate Bents
2939	2 of 5	1952	Movable Span-33'-0" Span-28'-0" Rdwy-1~3'-6" S.W.	Superstructure Details
2939	3 of 5	1952	Movable Span 33'-0" Span ~ 28'-0" RDWY ~ 2 - 3'-6" S.W.	
2939	1 of 5	1952	Concrete Pile Bents 33'-0" Span ~ 28'-0" RDWY ~ 1 - 3'-6" S.W.	
2940	1 of 2	1952	Concrete Pile Bents-28 ft Span-28 ft Roadway-1~4 ft Sidewalk	
2940	2 of 2	1952	Standard I-Beam Superstructure-28 ft Span-28 ft Roadway-1~4 ft Sidewalk	
2960	1 of 2	1952	Concrete Pile Bents 25' Span ~ 28' RDWY ~ 2-3'0" SDWKS ~ 2.78° Curve	
2960	2 of 2	1952	Precast Girders ~ Cast In Place Slab 25' Span ~ 28' RDWY ~ 2-3'0" SDWKS ~ 2.78° Curve	
2963	2 of 2	1952	Precast Slab Superstructure-15 ft Span-24 ft Roadway	
2976	CP28	1952	Concrete Pile Bents-32'-0" Span-28'-0" Roadway	
2991	S	1952	Precast Slab Superstructure 15 Ft. Span 28 Ft. Roadway	
2997	1 of 1	1952	Treated Timber Bulkhead Maximum Height 14'-0"	
3096	T.P. 24 ~ 0.0072	1952	Timber Pile Bents 15 Ft. Span 24 Ft. RDWY	
3297	S	1952	Concrete Pile Bents 25 Ft. Span 28 Ft. RDWY 2-3 Ft. SDWKS	
3297	S	1952	Precast Girders ~ Cast In Place Slab 25 Ft. Span 28 Ft. RDWY 2-3'-0" Ft. SDWKS	
3759	C.P. 28	1952	Concrete Pile Bents 25 Ft. Span, 28 Ft. RDWY., 2 ~ 3 Ft. S.W.	
3759	S	1952	Precast Girders ~ Cast In Place Slab 25 Ft. Span ~ 28 Ft. RDWY. ~ 2-3'-0" SDWKS.	
2546	SS-5-24	1953	Standard C.D.G. Superstructure-33 ft Span-28' Rdwy-Two 3' Sdwks	
2546	CP28	1953	Concrete Pile Bents-33 ft Span-28' Rdwy-Two 3' Sdwks	
2594	TP20	1953	Timber Pile Bents-15 ft Span-20 ft Roadway	
2642	CP28	1953	Concrete Pile Bents-15' Span-24' Rdwy-2~2'-6" Sdwks	
2644	S	1953	Precast Slab Superstructure-15 ft Span-28 ft Roadway-2~3 ft Sdwks	
2698	S	1953	Precast Girders~Cast in Place Slab-25 ft Span-20 ft Roadway	
2698	TP20	1953	Timber Pile Bents-25' Span-20' Roadway	
2788	S	1953	Standard I-Beam Superstructure 25' Span 28' RDWY 2 ~ 4' SDWKS	
2788	C.P. 28	1953	Concrete Pile Bents 25 Ft. Span, 28 Ft. RDWY., 2 ~ 4 Ft. S.W.	
2813	T.P. 24	1953	Timber Pile Bents 15 Ft. 24 Ft. RDW'Y.	
2813	S	1953	Precast Slab Superstructure 15' Span 24' Roadway	
2825	T.P. 20	1953	Timber Pile Bents 15 Ft. Span 20 Ft. Roadway	
2846	1 of 5	1953	Concrete Pile Bents 33' Span 28' Roadway 2 ~ 4'-0" S.W.	Bent at Hinged End and Rest Bent for Movable Span



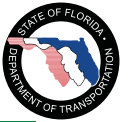
2861	CP-046-28	1953	Concrete Pile Bents-15 ft Span-28 ft Roadway	Superelevated .046 ft per ft
2861	TP5-24	1953	Timber Pile Bent-15 ft Span-24 ft Roadway	
2861	SS.046-28	1953	Concrete Slab Superstructure-15' Span-28 ft Roadway	Special Details for Slabs to be Superelevated .046 per foot
2861	SS-5-24	1953	Concrete Slab Superstructure-15' Span-24 ft Roadway	Special Details for Slabs to be Superelevated .045 ft per ft
2861	S-S-3/16-28	1953	Concrete Slab Superstructure 15 Ft. Span ~ 28 Ft. Roadway	Special Details for Slabs to be Superelevated 3/16" Per Ft.
2861	C.P. 28	1953	Concrete Pile Bent 15 Ft. Span 28 Ft. RDWY	
2903	T.P. 24	1953	Timber Pile Bents 25' Span 24' Roadway	
2915	CP24	1953	Concrete Pile Bents-25 ft Span-24 ft Roadway	
2915	S	1953	Concrete D.G. Superstructure-25 ft Span-24 ft Rdwy	
2944	S	1953	Concrete D.G. Superstructure 25' Span ~ 28' RDWY. ~ 2-3'-0" SDWKS.	
2944	C.P. 28	1953	Concrete Pile Bents 25 Ft. Span - 28 Ft. RDWY - 2 ~ 3 Ft. SDWKS	
2976	S	1953	Concrete Deck Girder Span 32 Ft. Span 28 Ft. Roadway	
2991	C.P. 28	1953	Concrete Pile Bents 15 Ft. Span 28 Ft. Roadway	
3000	S	1953	Standard Concrete D. G. Superstr. 33 Ft. Span 28' RDWY Two 3' SDWKS	
3000	T.P. 28	1953	Concrete Pile Bent 33 Ft. Span 28' RDWY 2~3' SDWKS	
3003	T.P. 20	1953	Timber Pile Bents 15 Ft. Span ~ 20 Ft. RDWY. ~ 2-3 Ft. S.W.	
3003	S	1953	Precast Slab Superstructure 15 Ft. Span , 20 Ft. RDWY. , 2~3 Ft. S.W.	
3004	S	1953	Precast Slab Superstructure 15 Ft. Span ~ 20 Ft. RDWY. ~ 2-3 Ft. S.W.	
3007	1 of 1	1953	14" X 14" Precast Concrete Pile Fresh Water Construction	
3012	S	1953	Concrete Slab Superstructure 15' Span 28' Roadway 30° Skew	
3012	C.P. 28	1953	Concrete Pile Bents 15' Span 28' Roadway 30° Skew	
3031	CP28	1953	Concrete Pile Bents-36 ft Span-28 ft Rdwy-2~3 ft S.W.	
3031	S	1953	Precast Girders-Cast in Place Slab-36 ft Span-28 ft Rdwy-2~3'-0" S.W.	
3043	1 of 3	1953	Composite Pile Bent-30 ft Span-Two Traffic Lanes	End Bent
3043	3 of 3	1953	Concrete D.G. Superstructure-30'-0" Span-4 Traffic Lanes	
3043	2 of 3	1953	Composite Pile Bent 30 Ft. Span - Two Traffic Lanes	
3044	1 of 1	1953	Concrete Decking for 20' RDWY - 15" Span - Timber Bridge	
3047	1 of 1	1953	Concrete Decking for 20' Rdwy-15' Span-Timber Bridge	15 ft Timber Span (Concrete Decking Details)
3050	CP28	1953	Concrete Pile Bents-25 ft Span-42° Skew-28 ft Roadway	
3050	S	1953	Concrete Deck Girder Span-25 ft Span-48° Skew-28 ft Roadway	
3055	C.P. 24	1953	Concrete Pile Bents 15'-0" Span ~ 24' RDWY ~ 1-5'-0" Sidewalk	
3055	S	1953	Slab Superstructure 15 Ft. Span ~ 24 Ft. Roadway ~ 1-5'-0" Sidewalk	
3062	1 of 1	1953	Concrete Decking for 24' Rdwy-15' Span-Timber Bridge	Details of Concrete Decking
3068	CP28	1953	Concrete Pile Bents-33'-0" Span-28'-0" Roadway	
3068	S	1953	Concrete Deck Girder Superstr.-33 ft Span-28' Roadway	
3088	CP28	1953	Concrete Pile Bents-20' Span-28' Rdwy-1:5' S.W.-.0208 Superelev.	
3089	1 of 1	1953	Composite Concrete & Steel Piling (14" Sq.)	
3096	S.S. 24 ~ 0.0072	1953	Concrete Slab Superstructure 15 Ft. Span 24 Ft. RDWY Superelev. 0.072'	
3100	S	1953	Precast Slab Superstructure 15 Ft. Span 20 Ft. Roadway	
3100	T.P. 20	1953	Timber Pile Bents 15 Ft. Span ~ 20 Ft. Roadway	
3102	T.P. 20-0.06	1953	Timber Pile Bents 15 Ft. Span ~ 20 Ft. Roadway	
3137	S	1953	Precast Slab Superstructure-15 ft Span-28 ft Roadway	
3142	CP28-E	1953	Concrete Pile Bents-45' Span-28' Rdwy-2~4' Sdwks	
3142	S	1953	Composite I-Beam Superstructure-45 ft Span- 28 ft Rdwy-2~4 ft Sidewalks	
3142	CP - 28-I	1953	Concrete Pile Intermediate Bent 45 Ft. Span - 28 Ft. R'DW'Y - ~ 4 Ft. S.Walks	
3160	C.P. 28	1953	Concrete Pile Bents 25 Ft. Span - 28 Ft. Roadway	
3160	S	1953	Concrete Deck Girder Supstr. 25 Ft. Span - 28 Ft. Roadway	
3201	S	1953	Concrete Deck Girder Super. 36 Ft. Span ~ 24 Ft. Roadway	



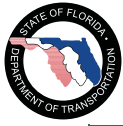
3201	CP 24	1953	Concrete Pile Bents 36'-0" Span ~ 24'-0" Roadway ~ 2-3'-0" Sidewalks	
3493	C.P. 24	1953	Concrete Pile Bents 25 Ft. Span 24 Ft. Roadway	
3493	S	1953	Precast Girders ~ Cast In Place Slab 25 Ft. Span 24 Ft. Roadway	
3567	C.P. 24	1953	Concrete Pile Bents 25 Ft. Span 24 Ft. RDW'Y.	
3567	S	1953	Concrete D. G. Superstructure 25 Ft. Span 24 Ft. RDW'Y	
3580	C.P. 24	1953	Concrete Pile Bents 25 Ft. Span 24 Ft. RDW'Y	
3580	S	1953	Concrete D. G. Superstructure 25 Ft. Span 24 Ft. RDW'Y	
2123	1 of 1	1954	Precast Concrete Piles	Details of Piles for Salt Water Construction
2228	1 of 1	1954	12"x 12" Precast Concrete Pile-Fresh Water Construction	
2469	1 of 1	1954	14" X 14" Precast Concrete Pile - Salt Water Construction	
2721	CP - 28	1954	Concrete Pile Bents 25' Span 28' Roadway	
2723	CP28	1954	Concrete Pile Bents-25' Span-28' Roadway	
2723	S	1954	Precast Girders~Cast in Place Slab-25 ft Span-28 ft Roadway	
2915	C.P.A.	1954	Concrete Pile Abutment 25 ft Span-24 ft Roadway	
3082	CP24	1954	Composite Concrete & Steel Pile Bent-24 ft Roadway-25 ft Span	
3102	S	1954	Standard Slab Superstructure 15 Ft. Span ~ 20 Ft. Roadway	
3102	C.P. 20	1954	Timber Pile Bents 15 Ft. Span ~ 20 Ft. Roadway	
3102	T.P. 20	1954	Timber Pile Bents 15 Ft. Span ~ 20 Ft. Roadway	
3159	S	1954	Concrete Deck Girder Span 36'-0" Span ~ 28'-0" RDWY ~ 2-3'-6" S.W.	
3170	T.P. 24	1954	Timber Pile Bents 15 Ft. Span 24 Ft. Roadway	
3182	CP28	1954	Concrete Pile Bents-36'-0"-28'-0" Rdwy	
3182	S	1954	Concrete Deck Girder Span-36 ft Span-28 ft Roadway	
3194	S	1954	Concrete Slab Superstructure 20 Ft. Span 28 Ft. Roadway	
3196	S	1954	Concrete Deck Girder Superstructure-36 ft Span-24 ft Rdwy-2~3'-0" Sdwks	
3196	CP24	1954	Intermediate Concrete Pile Bent-36 ft Span-24 ft Roadway	
3197	1 of 1	1954	Composite Concret and Steel Piling 20' Sq.	
3223	S	1954	Concrete Deck Girder Superstr.-25 ft Span-28 ft Roadway-2~5'-0" Sidewalks	
3223	CP28	1954	Concrete Pile Bents-25 ft Span-28 ft Roadway-2~5 ft Sidewalks	
3264	S	1954	Standard I-Beam Superstructure-36 ft Span-28 ft Roadway-2~3'-6" SW	
3264	CP28	1954	Concrete Pile Bent-36 ft Span-28 ft Roadway-2~3'-6" Sidewalks	End Bent No. 1
3276	1 of 3	1954	Concrete Pile Bent-76' Span-28' Roadway	
3276	2 of 3	1954	Superstructure - 76 Ft. Span	
3281	CP28	1954	Concrete Pile Bents-20 ft Span-28 ft Roadway	
3281	S	1954	Concrete Slab Superstructure-20 ft Span-2~3'-6" SW-28 ft Rdwy	
3294	1 of 1	1954	18"x 18" & 20"x 20" Prestressed Concrete Piles	
3320	S	1954	Concrete Deck Girder Span-36 ft Span-28 ft Roadway-2~3'-6" Sidewalks	
3320	CP28	1954	Concrete Pile Bents-36'-0"-28'-0" Rdwy-2~3'-6" S.W.	
3347	S	1954	Composite I-Beam Supersructure 60 Ft. Span 28 Ft. Roadway	
3352	CP28	1954	Concrete Pile Bents-36 ft Span-28'-0" Roadway	
3352	S	1954	Concrete Deck Girder Span 36 Ft. Span 28 Ft. Roadway	
3355	S	1954	Concrete Deck Girder Span 36 Ft. Span 28 Ft. RDWY 2~5 Ft. Sidewalks	
3355	C.P. 28	1954	Concrete Pile Bents 36'-0" Span ~ 28'-0" RDWY ~ 2 ~ 5'-0" S.W.	
3379	S	1954	Concrete Slab Superstruct.-20 ft Span-28 ft Rdwy-30° S.K.	
3379	C.P. 24	1954	Concrete Pile Bents 20' Span ~ 24'RDWY ~ 30° SK.	
3389	S	1954	Concrete Slab Superstructure 20 Ft. Span ~ 24 Ft. R'DW'y ~ 30° Skew	
3389	C.P. 24	1954	Concrete Pile Bents 20' Span ~ 24' RDWY ~ 30° SK. Lt.	
3399	1 of 2	1954	Composite I-Beam Superstructure-63 ft Span-2~23 ft Rdwys-2~5 ft Swks	
3486	2 of 3	1954	Superstructure-76 ft Span	
3010	1 of 2	1955	Composite I-Beam Superstructure-50 ft Span-Four Lane Roadway	50 ft I-Beam Span



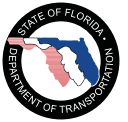
3010	2 of 2	1955	Composite I-Beam Superstructure-50 ft Span-Four Lane Roadway	
3011	2 of 2	1955	Composite I-Beam Superstructure-45 ft Span-Four Lane Roadway	
3011	1 of 2	1955	Composite I-Beam Superstructure-45 ft Span-Four Lane Roadway	
3108	C.P. 28	1955	Concrete Pile Bents 20 Ft. Span - 28 Ft. Roadway	
3108	S	1955	Concrete Slab Superstructure 20' Span 28' Roadway	
3185	S	1955	Precast Slab Superstructure 15 Ft. Slab 28 Ft. Roadway	
3194	C.P. 28	1955	Concrete Pile Bents 20 Ft. Span 28 Ft. Roadway	
3296	S	1955	Precast Slab Superstructure-15 ft Span-24 ft Roadway	
3320	EB-SP-28	1955	Steel Pile End Bent-36'-0" Span-28'-0" Rdwy-2~3'-6" SW	
3320	IB-SP28	1955	Steel Pile Intermediate Bent-36'-0" Span-28'-0" Roadway-2~3'-6"SW	
3323	1 of 1	1955	Prestressed Concrete Beams	
3399	2 of 2	1955	Composite I-Beam Supersructure 63 Ft. Span ~ 2 ~ 23 Ft. RDWYS ~ 2 ~ 5 Ft. SWKS.	
3438	1 of 1	1955	Prestressed C. D. G. Superstructure 36 Ft. Span 4 Lane Roadway	
3440	1 of 3	1955	Concrete Pile Bents 36 Ft. Span 4 Lane Roadway	
3440	3 of 3	1955	Concrete Deck Girder 36 Ft. Span 4 Lane Roadway	
3441	1 of 1	1955	Concrete Deck Girder 45 Ft. Span 4 Lane Roadway	
3444	1 of 1	1955	Prestressed Superstructure 24 Ft. Roadway	
3486	1 of 3	1955	Steel Pile Bent 76 Ft. Span - 28 Ft. R'DW'Y	
3486	3 of 3	1955	Superstructure 76 Ft. Span	Details of Expansion Jt. Assembly & Details of Shoes for 76 Ft. Span
3516	T.P. 24	1955	Timber Pile Bents 20 Ft. Span 24 Ft. Roadway	
3516	S	1955	Standard SlabSuperstructure 20 Ft. Span 24 Ft. Roadway	
3518	C.P. 24	1955	Concrete Pile Bents 20 Ft. Span 2 ~ 3'-0" S.W. 24 Ft. RDWY	
3518	S	1955	Concrete Slab Superstructure 20 Ft. Span 2 ~ 3'-0" S.W. 24 Ft. RDWY	
3526	1 of 1	1955	Prestessed Superstructure 48 Ft. Span 24 Ft. - 28 Ft. Roadway	
3532	2 of 3	1955	Composite I-Beam Superstructure-76 ft Span-2~26 ft Roadways	
3532	1 of 3	1955	Concrete Pile Abutment-76 ft Span-2'26'-0" Roadways-2~2'-0" Curbs	
3532	3 of 3	1955	Composite I-Beam Superstructure 76 Ft. Span 2 ~ 26 Ft. Roadways	
3539	S	1955	Composite I-Beam Superstructure 40 Ft. Span 28 Ft. Roadway	
3539	C.P. - 28	1955	Concrete Pile Bent 40 Ft. Span 28 Ft. RDWY	
3540	1 of 1	1955	Composite I-Beam Superstructure 55 Ft. Span 28 Ft. Roadway	
3547	TP-7-24	1955	Timber Pile Bents 20 Ft. Span 24 Ft. Roadway	
3547	SS-7-24	1955	Concrete Slab Superstructure 20 Ft. Span 24 Ft. Roadway	
3555	SP - 28	1955	Steel Pile Bents 20 Ft. Span 28 Ft. Roadway	
3603	2 of 2	1955	Composite I-Beam Superstructure 86 Ft. Span Four Lane Roadway	
3603	1 of 2	1955	Composite I-Beam Superstructure 86 Ft. Span Four Lane Roadway	
3606	3 of 4	1955	48 Ft. Prestressed Superstructure 24 Ft. and 28 Ft. Roadways	
3606	4 of 4	1955	48 Ft. Prestressed Superstructure 24 Ft. and 28 Ft. Roadways	
3606	2 of 4	1955	48 Ft. Prestressed Superstructure 24 Ft. and 28 Ft. Roadways	
3606	1 of 4	1955	48 Ft. Prestressed Superstructure 24 Ft. and 28 Ft. Roadways	
3612	1 of 4	1955	48 Ft. Prestressed Superstructure 2-21 Ft. Roadways 2 ~ 5 Ft. Walks	
3612	2 of 4	1955	48 Ft. Prestressed Superstructure 2-21 Ft. Roadways 5 Ft. SDWLKS.	
3612	3 of 4	1955	48 Ft. Prestressed Span 2-21 Ft. Roadways, 5 Ft. Sidewalks	
3612	4 of 4	1955	48 Ft. Prestressed Span 2-21 Ft. Roadways, 5 Ft. SDWLKS.	



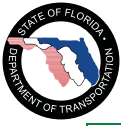
3619	1 of 1	1955	Typical Details of 18" Square and 20" Square Prestressed Piles	
3643	1 of 3	1955	Concret Pile End Bent 50 Ft. Span ~ 28 Ft. RD WY	
3643	2 of 3	1955	Concret Pile Intermediate Bent 50 Ft. Span ~ 28 Ft. RD WY	
3643	3 of 3	1955	Prestressed Concrete Span 50 Ft. Span ~ 28 Ft. RD WY	
3667	1 of 1	1955	66 Ft. Prestressed Superstructure	
4768	S	1955	Standard Slab Superstructure 20 Ft. Span 24 Ft. Roadway	
3108	S-C.P. 28	1956	Concrete Pile Bents 20 Ft. 28 Ft. RDWY.	
3108	SS-.035-28	1956	Concrete Slab Superstructure 20' Span 28' Roadway	Special Details for Slabs to be Super
3457	1 of 1	1956	Prestressed Slab-15 ft Span-28 ft Roadway	
3458	1 of 1	1956	Prestressed Slab 20 Ft. Span 24 Ft. Roadway	
3461	1 of 1	1956	Prestressed Slab 20 Ft. Span 28 Ft. Roadway	
3464	1 of 1	1956	Prestressed Slab-15 ft Span-24 ft Roadway	
3596	C.P.-28	1956	Concrete Pile Bents 33 Ft. Span ~ 28 Ft. Roadway	
3596	S	1956	Concrete Deck Girder Span 33 Ft. Span 28 Ft. Roadway	
3632	1 of 1	1956	40 Ft. Prestressed Superstructure 2-26 Ft. Roadways 6'-6" Median	
3638	4 of 4	1956	63 Ft. Prestressed Concrete Span 2 ~ 23 Ft. Roadways 2 ~ 5 Ft. Sidewalks	
3638	3 of 4	1956	63 Ft. Prestressed Concrete Span 2 ~ 23 Ft. Roadways 2 ~ 5 Ft. Sidewalks	
3644	SP 28	1956	Steel Pile Bents 28 Ft. Roadway ~ 36 Ft. Prestressed Span	
3644	CP 28	1956	Concrete Pile Bents 28 Ft. RDWY 36 Ft. Span	
3644	S	1956	36 Ft. Prestressed Concrete Span 28 Ft. Roadway	
3649	1 of 3	1956	End Bents 66 Ft. Span 4 Lane Roadway	
3649	2 of 3	1956	Intermediate Bents & Tower Bents 66Ft. Prestressed Span ~ 2 - 26' Roadways	
3659	1 of 1	1956	24'Sq. Prestressed Concrete Piles	
3660	1 of 2	1956	Prestressed Superstructure 48 Ft. Span 28 Ft. Roadway	
3660	2 of 2	1956	Concrete Pile Superstructure 48 Ft. Span 28 Ft. Roadway	
3666	1 of 1	1956	54" Prestressed Concrete Cylinder Pile	
3684	1 of 2	1956	Concrete Pile Bents 30 Ft. Span 4 Lane Roadway	
3684	2 of 2	1956	Prestressed Slab Superstructure 30 Ft. Span 4 Lane Roadway	
3690	C.P. 28	1956	Concrete Pile Bents 40 Ft. Span ~ 28 Ft. Roadway ~ 2 : 3'-6" Sidewalks	
3690	S	1956	40 Ft. Prestressed Beam Span 28'-0" Roadway 2 ~ 3'-6" Sidewalks	
3706	1 of 2	1956	Concrete Pile Substructure 37 Ft. Span ~ 26 Ft. Roadway ~ One 5 Ft. Sideway	
3706	2 of 2	1956	37 Ft. Prestressed Concrete Span 26 Ft. Roadway ~ One 5 Ft. Sideway	
3712	S	1956	Concrete Slab Superstructure 30'-0" Span 28'-0" Roadway	
3712	C.P. 28	1956	Concrete Pile Bent 28 Ft. Roadway ~ 30 Ft. Slab Span	
3746	S	1956	Concrete Slab Superstructure 33 Ft. Span 2 ~ 3'-0" S.W. 24 Ft. RDWY	
3746	C.P. 24	1956	Concrete Pile Bents 33 Ft. Span 2 ~ 3'-0" S.W. 24 Ft. RDWY	
3772	S	1956	Prestressed Concrete Superstructure 60 Ft. Span ~ 28 Ft. Roadway ~ 2-2Ft. Curbs	
3772	CP -28-I	1956	Concrete Pile Superstructure 60 Ft. Span 28 Ft. Roadway	
3792	S	1956	Concrete Slab Superstructure-20 ft Span-28 ft Rdwy-2-3 ft Sidewalks-30° Skew	
3792	CP28	1956	Concrete Pile Bents-20 ft Span-28 ft Roadway-30° Skew	
3798	1 of 3	1956	Concrete Pile Bents-33 ft Span-Dual 26 ft Roadways	End Bent
3798	2 of 3	1956	Concrete Pile Bents-33 ft Span-Dual 26 ft Roadways	Intermediate Bents
3798	3 of 3	1956	Concrete Slab Superstructure-33 ft Span-Dual 26 ft Roadways	
3800	1 of 3	1956	98 ft Prestressed Superstructure	
3800	2 of 3	1956	98 ft Prestressed Superstructure	
3800	3 of 3	1956	98 ft Prestressed Superstructure	
3802	CP28	1956	Concrete Pile Bents-28 ft Roadway-30 ft Span-30° Skew	
3802	S	1956	Concrete Slab Superstructure-30 ft Span-28 ft Roadway-30° Skew	
3804	S	1956	Concrete Slab Superstructure-30 ft Span-28 ft Roadway-15° Skew	



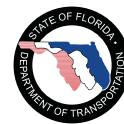
3804	CP28	1956	Concrete Pile Bents-30 ft Span-28 ft Roadway-15° Skew	
3809	1 of 3	1956	98 ft Prestressed Superstructure	
3811	CP76	1956	Concrete Pile End Bent-65 ft Span-2~38 ft Roadways	
3811	1 of 3	1956	Prestressed Concrete Superstructure-65' Span-Two 38 ft Roadways	
3827	CP28	1956	Concrete Pile Bents-20 ft Span-28 ft Roadway-15° Skew	
3827	S	1956	Concrete Slab Superstructure-20 ft Span-28 ft Rdwy-15° Skew	
3829	1 of 2	1956	68 ft Prestressed Superstructure	
3829	2 of 2	1956	68 ft Prestressed Superstructure	
3832	TP24	1956	Timber Pile Bents-30 ft Span-15° Skew-24 ft Roadway	
3832	S	1956	Concrete Slab Superstructure-30 ft Span- 15° Skew-24 ft Roadway	
3835	1 of 1	1956	47 ft Prestressed Superstructure	
3840	S	1956	Concrete Slab Superstructure-15 ft Span-28 ft Roadway	
3849	1 of 2	1956	Concrete Pile Bents-30 ft Span-52 ft Roadway	Substructure
3849	2 of 2	1956	Prestressed Slab Superstructure-32 ft Span-52 ft Roadway	
3857	1 of 3	1956	Concrete Pile Bents-38 ft Span-28 ft Roadway	End Bents
3857	2 of 3	1956	Concrete Pile Bents-38 ft Span-28 ft Roadway	
3858	2 of 3	1956	Concrete Pile Bents-38 ft Span-28 ft Roadway	
3434	S	1957	Prestressed Beam Superstructure 36 Ft. Span 28 Ft. Roadway	
3516	C.P. 24	1957	Concrete Pile Bents 20 Ft. Span 24 Ft. Roadway	
3888	CP28	1957	Concrete Pile Bents-43' Span-28' Roadway-2 ft Curb-4 ft Sidewalk	
3888	S	1957	Prestressed Concrete Superstructure-43' Span-28' Roadway-2 ft Curb-4 ft Sidewalk	
3892	T.P. 24	1957	Timber Pile Bents 30 Ft. Span 24 Ft. RDWY.	
3892	S	1957	Concrete Slab Superstructure 30 Ft. Span 24 Ft. Roadway	
3895	T.P. - 24	1957	Timber Pile Bents 26 Ft. Span ~ 24 Ft. RDWY.	
3895	S	1957	Concrete Slab Superstructure	
3900	2 of 2	1957	Prestressed Concrete Superstructure 62 Ft. Span ~ 28 Ft. Roadway ~ 2-3'-6" Sidewalks	Details of Prestressed Beams (Type C-18-2)
3900	1 of 2	1957	Prestressed Concrete Superstructure 62 Ft. Span ~ 28 Ft. Roadway ~ 2-3'-6" Sidewalks	
3908	1 of 1	1957	Slab Superstructure	
3913	S	1957	Prestressed Beam Superstructure	
3913	CP - 24I	1957	Concrete Pile Bents 26 Ft. Span 24 Ft. Roadway	
3919	C.P. 24	1957	Concrete Pile Bents Ft. Span 24 Ft. Roadway	
3923	C.P. 28	1957	Concrete Pile Bents 40 Ft. Span 2~28 Ft. RDWYS 2 Ft. Curbs & 5 Ft. SWKS	
3923	S	1957	Prestressed Beam Superstructure 40 Ft. Span 2~28 Ft. RDWYS 2 Ft. Curbs & 5 Ft. SWKS	
3927	1 of 1	1957	Prestressed Concrete Beam Type IV	
3928	1 of 3	1957	Prestressed Concrete Superstructure 98 Ft. Two 38 Ft. Roadway	
3934	C.P. - 28	1957	Concrete Pile Bents 36 Ft. Span 28 Ft. Roadway	
3935	S	1957	Prestressed Beam Superstructure 44 F. Span 28 Ft. Roadway	
3940	CP28	1957	Concrete Pile Bents-Continuous 30'-30'-30'-Spans-28 ft Roadway	
3940	S	1957	Continuous Span Concr. Slab Superstructure 30'-30'-30' Spans ~ 28 Ft. Roadway	
3969	S	1957	Concrete Slab Superstructure-20 ft Span-2~4 ft SW-24 ft Roadway	
3969	WCP24	1957	Concrete Pile Bents-20 ft Spans-2~4 ft SW-24 ft Roadway	
3969	CP24	1957	Concrete Pile Bents-20 ft Span-2~4 ft SW-24 ft Roadway	
3973	1 of 3	1957	Prestressed Concrete Superstructure-66 ft Span-2~26 ft Roadways	
3984	1 of 3	1957	Prestressed Beam Superstructure-46 ft Span-2~21 ft Roadways-2~5 ft Sidewalks	
3984	3 of 3	1957	Concrete Pile Bents-46 ft Span-2~21 ft Roadways-2~ 5 ft Swks	
3985	1 of 2	1957	Prestressed Beam Superstructure	
3985	1 of 2	1957	Prestressed Beam Superstructure-43 ft Span-2~21 ft Roadways-2~5 ft Sidewalks	



3991	S	1957	Concrete Slab Superstructure-20 ft Span-2~4'-0" SW-28 ft Roadway	
3991	CP28	1957	Concrete Pile Bents-20 ft Span-2~4'-0" SW-28 ft Roadway	
3998	1 of 1	1957	Concrete Pile Bent-43 ft Span-2~ 21 ft Rdwys-2~5' Swks~2' Median	Bents 2 & 3
4006	1 of 1	1957	Details of Approach Slab-28 ft Roadway-30° Skew-Two 3' SW Flared	
4007	1 of 2	1957	Concrete Slab Superstructure-23 ft Span-28 ft Roadway	
4008	1 of 3	1957	Concrete Slab Superstructure-21 ft Span-28 ft Roadway	
4008	2 of 3	1957	Concrete Slab Superstructure-16 ft Span-28 ft Roadway	
4008	3 of 3	1957	Concrete Pile Bents-21 ft Span-28 ft Roadway-2 ft Curbs	
4031	1 of 4	1957	Prestressed Beam Superstructure-36 ft Span-28 ft Roadway	
4033	1 of 2	1957	Prestressed Beam Superstructure-40 ft Span-2~26 ft Rdwys-2~5 ft Swks-4 ft Med	
4033	2 of 2	1957	Concrete Pile Bents-40 ft Span-2~26 ft Rdwys-2~5 ft Swks-4 ft Med	
4039	1 of 2	1957	Prestressed Beam Superstructure-60 ft Span-28 ft Roadway	
4049	1 of 4	1957	Concrete Pile End Bent-40 ft Span-28 ft Roadway	
4049	2 of 4	1957	Concrete Pile End Bent-40 ft Span-28 ft Roadway	
4049	3 of 4	1957	Prestressed Beam Superstructure-40 ft Span-28 ft Roadway	
4055	1 of 1	1957	Prestressed Beam Superstructure 48 Ft. Span 2~26 Ft. Rdwys 2~5 Ft. Swks 4 Ft. Med.	
4197	1 of 5	1957	Concrete Pile End Bent 40 Ft. Span ~ 28 Ft. RDWY. ~ 3 Ft. SDWK.	
4197	4 of 5	1957	40 Ft. Span Superstructure 28 Ft. RDWY. ~ 3'-6" SDWK.	
4197	5 of 5	1957	Prestressed Beam Type II 26-0 ~ 40 Ft. Span	
		1957	Concrete Pile End Bent Ft. Span Ft. Roadway	Wingwall Details Type III Beams
4098	S	1958	Concrete Slab Superstructure 15 Ft. Span 24 Ft. Roadway	
4098	C.P.-24	1958	Concrete Pile Bent 15 Ft. Span 24 Ft. Roadway	
4141	1 of 2	1958	Concrete Pile Bents-26' Span-28' Roadway	
4141	2 of 2	1958	Concrete Slab Superstructure-26 ft Span-28 ft Roadway	
4174	C.P.-28	1958	Concrete Pile Bents 20' Span 28' Roadway 2' Curbs 3/16" Super. Elev.	
4174	S	1958	Concrete Slab Superstructure 20 Ft. Span 28 Ft. Roadway 3/16" / Ft. Super. Elev.	
4193	3 of 5	1958	Concrete Pile Bent 40' Span 24' Roadway	
4193	4 of 5	1958	40 Ft. Span Superstructure 24 Ft. Roadway 3'-6" Sidewalks	
4193	5 of 5	1958	Prestressed Concrete Beam (Type II, 22-0) 40 Ft. Span Superstructure	
4193	1 of 5	1958	Concrete Pile End Bent 40 Ft. Span 24 Ft. Roadway 3'-6" Sidewalks	
4197	3 of 5	1958	Concrete Pile Bent 40 Ft. Span 28 Ft. Roadway	
4212	1 of 1	1958	Prestressed Beam Superstructure 70 Ft. Span 28 Ft. Roadway	
4237	C.P. 24	1958	Concrete Pile Bents 20 Ft. Span 24 Ft. Roadway	
4249	S	1958	Prestressed Slab 30 Ft. Span 24 Ft. Roadway	Proposed 30 Ft. Superstructure
4249	CP - 24I	1958	Concrete Pile Bents 30 Ft. Span 24 Ft. Roadway	
4249	CP - 24E	1958	Concrete Pile Bents 30 Ft. Span 24 Ft. Roadway	
4460	CP28	1959	End Bent and Intermediate Bent 25 Ft. Span 28 Ft. Roadway	
4460	S	1959	Concrete Slab Superstructure 25 Ft. Span 28 Ft. Roadway	
4474	1 of 1	1959	Approach Slab Details 28' Roadway ~ Superelevate 3/16" Per Ft. ~ 2' Curb & 4' S.W.	
4494	CP28	1959	Concrete Pile Bents 20 Ft. Span 28 Ft. Roadway	
4494	S	1959	Concrete Slab Superstructure 20 Ft. Span 28 Ft. Roadway	
4579	5 of 6	1959	41 Ft. Span Superstructure	
4699	C.P.28	1959	Concrete Pile Bents 20' Span ~ 28' RDWY ~ 35° Skew	
7347	1 of 2	1959	Prestressed Slab Superstructure 30 Ft. Span ~ 24 Ft. Roadway	
4749	1 of 1	1960	Concrete Pile Bent 40 Ft. Span 28 Ft. Roadway	
4827	SP-24	1960	Standard Substructure 24' Roadway; 26' Span; 30° Skew Left	
4827	S-24	1960	Standard Superstructure 26' Span; 24' Roadway; 30° Skew Left	
4859	2 of 2	1960	Substructures	
4859	1 of 2	1960	25 Ft. Span Superstructure	
4911	S	1960	28 ft Span Slab Superstructure-24 ft Roadway-9" Curbs	



7020	1 of 1	1960	Steel Pile Bents-41 ft Span-24 ft Roadway	
		1960	Prestressed Beams (Type II -	
7347	2 of 2	1962	Prestressed Slab Superstructure 30 Ft. Span ~ 24 Ft. Roadway	Slab Unit Details
7432	CP24	1962	Concrete Pile Bents-20 ft Span-24 ft Roadway	
7432	S	1962	Standard Slab Superstructure-20 ft Span-24 ft Roadway	
7473	CP24	1962	Concrete Pile Bents-20 ft Span-24 ft Roadway	
7697	1 of 2	1963	Prestressed Slabs & Beams	
7697	2 of 2	1963	Prestressed Slabs & Beams	
7786	1 of 5	1963	Concrete Slab Superstructure-25 ft Span-28 ft Roadway	
7786	5 of 5	1963	Intermediate Bents-25 ft Span-28 ft Roadway	
7786	4 of 5	1963	Intermediate Bents-25 ft Span-28 ft Roadway	
7786	2 of 5	1963	End Bents-25 ft Span-28 ft Roadway	
8381	1 of 1	1964	Intermediate Bents	
8502	1 of 1	1964	Intermediate Bents	
8750	CP	1964	Concrete Pile Bents-30 ft Span-30 ft Roadway	
		1966	Prestressed Slab Unit (15" x 36")	
9663	1 of 1	1967	Bridge Typical Sections	
10289	S 1 of 1	1969	20", 24" and 30" Prestressed Concrete Piles	
12670	2 of 3	1978	Prestressed Slab Units	
12670	1 of 3	1978	Prestressed Slab Units	
1	4		28'-0" Clear Span Concrete Deck Girder	
1866	1 of 1		Standard Conc. D.G. Superstructure 26'-0" Roadway ~ 22'-6" Span	
4007			Concrete Pile Bents-23 ft Span-28 ft Rdwy-2 ft Curbs- Superelevated 3/16" per ft	



Appendix C

The following items are included in Appendix C:

- Standard Bearing Capacity Curves

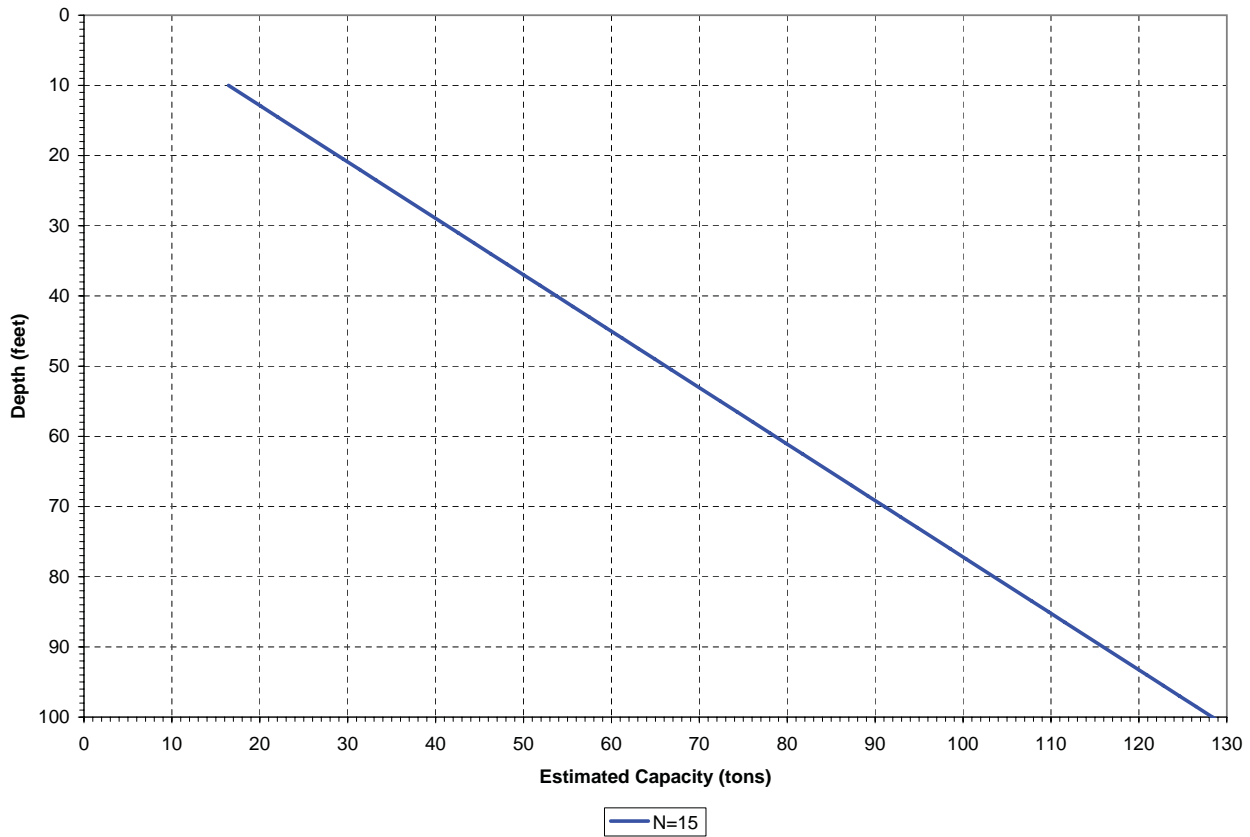
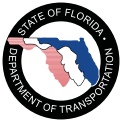


Figure 1: 12 inch Piles - “Standardized Curve”

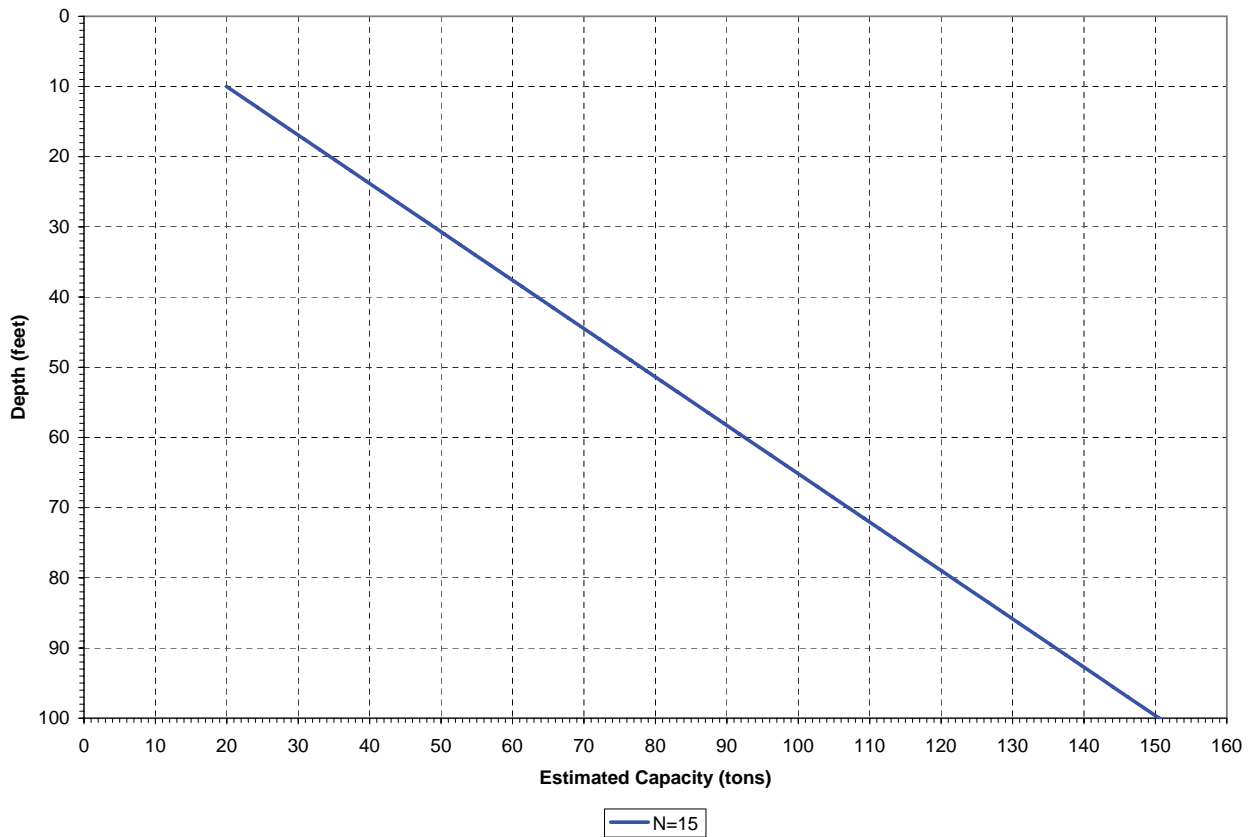


Figure 2: 14 inch Piles - “Standardized Curve”

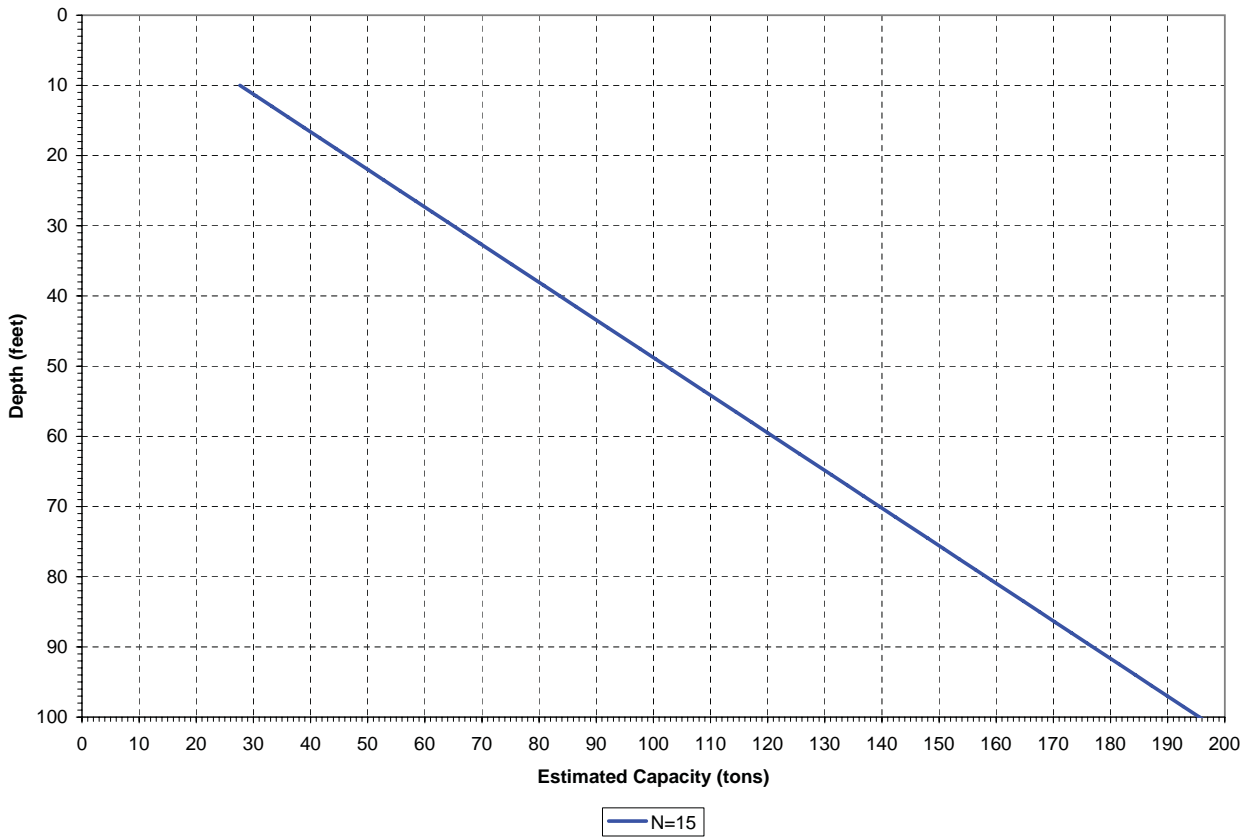
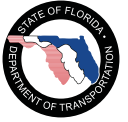


Figure 3: 18 inch Piles - "Standardized Curve"

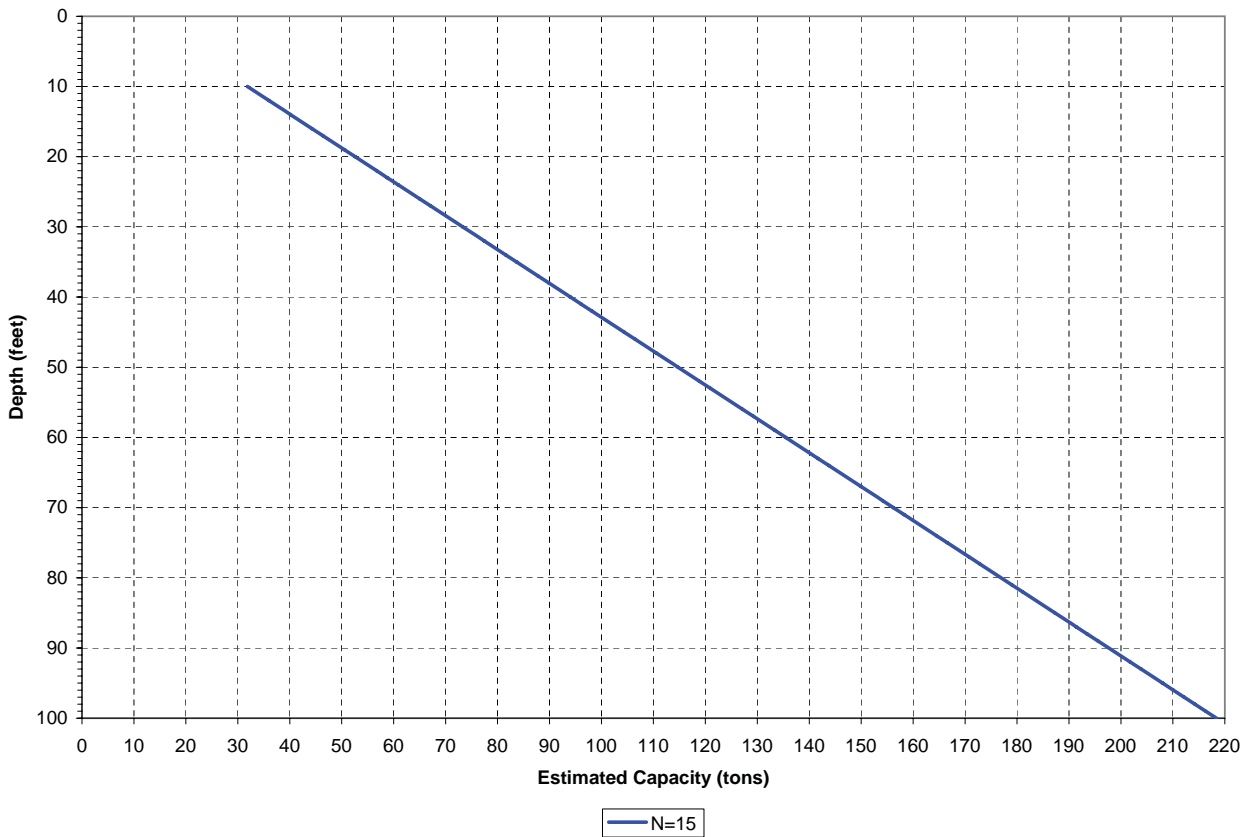


Figure 4: 20 inch Piles - "Standardized Curve"

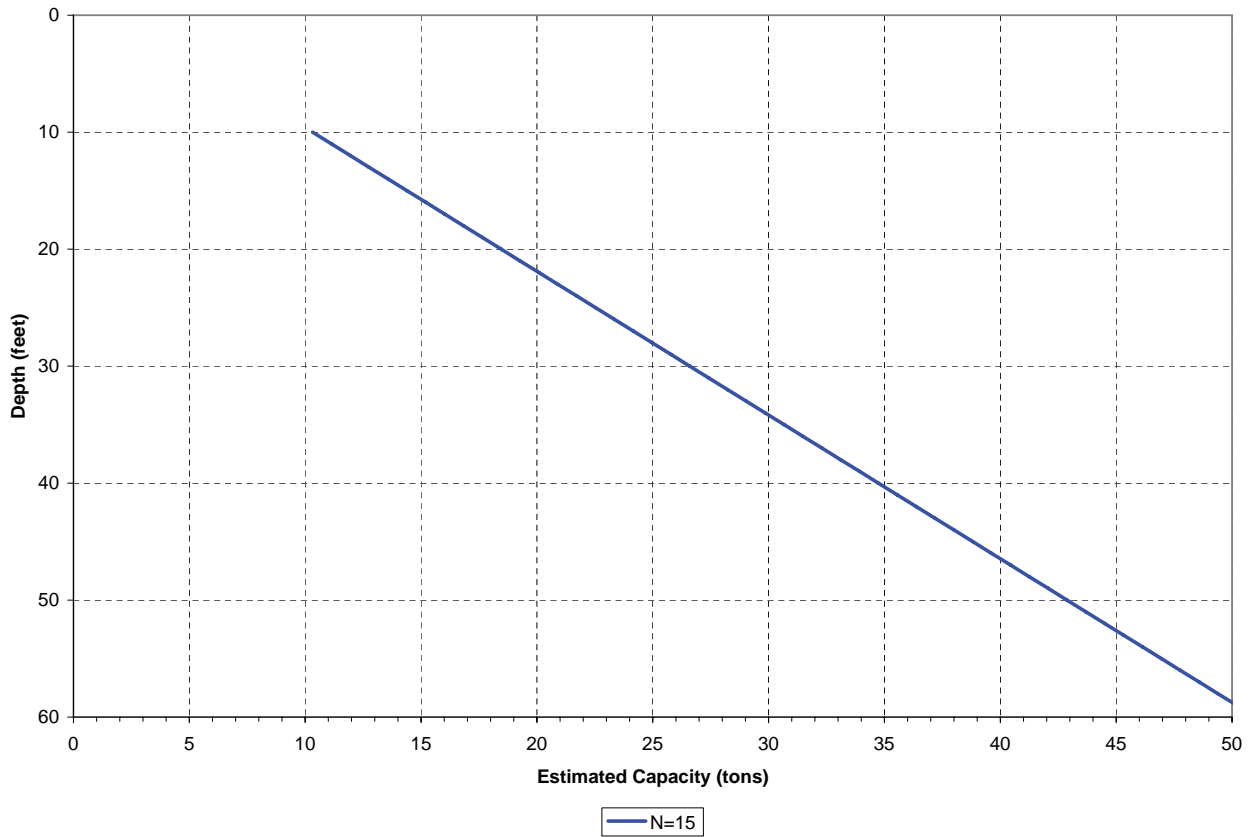
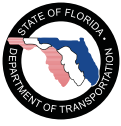


Figure 5: Timber Piles - “Standardized Curve”

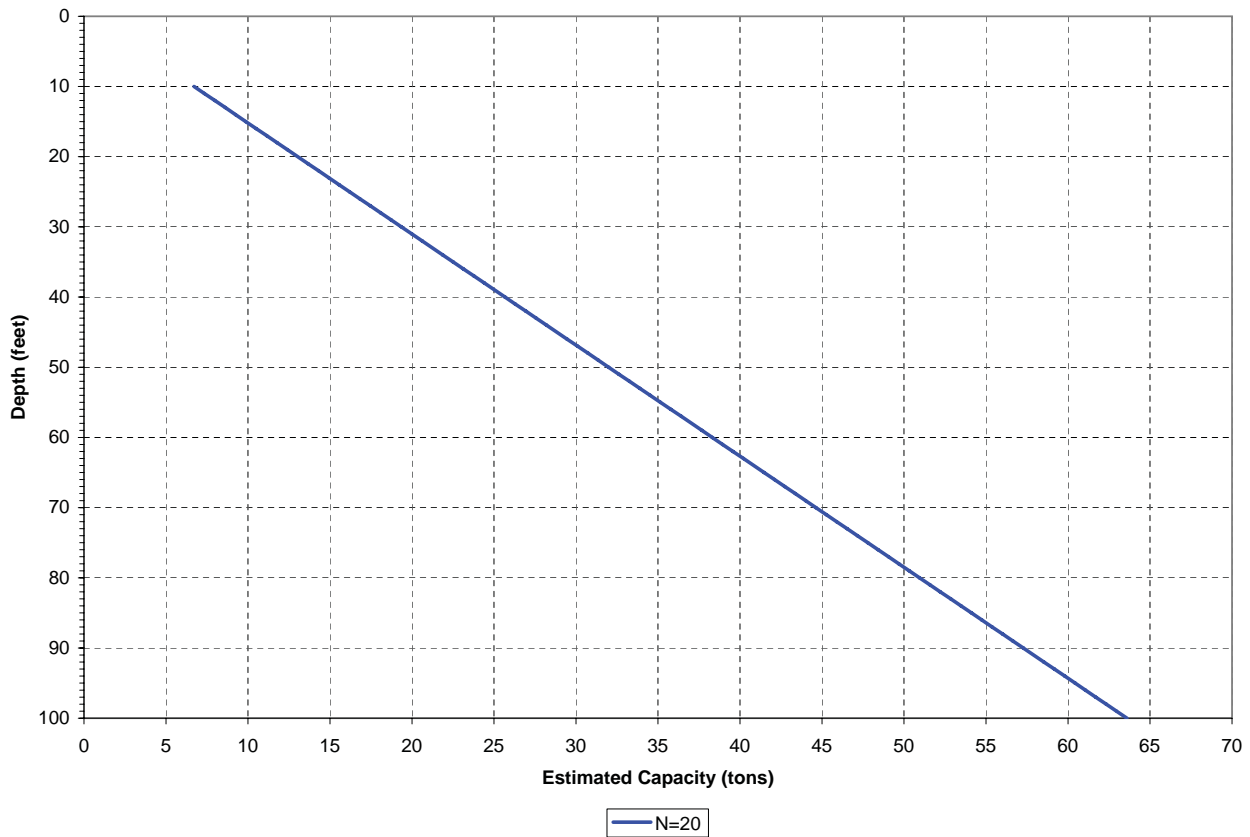


Figure 6: 8 HP 36 Pile - “Standardized Curve”

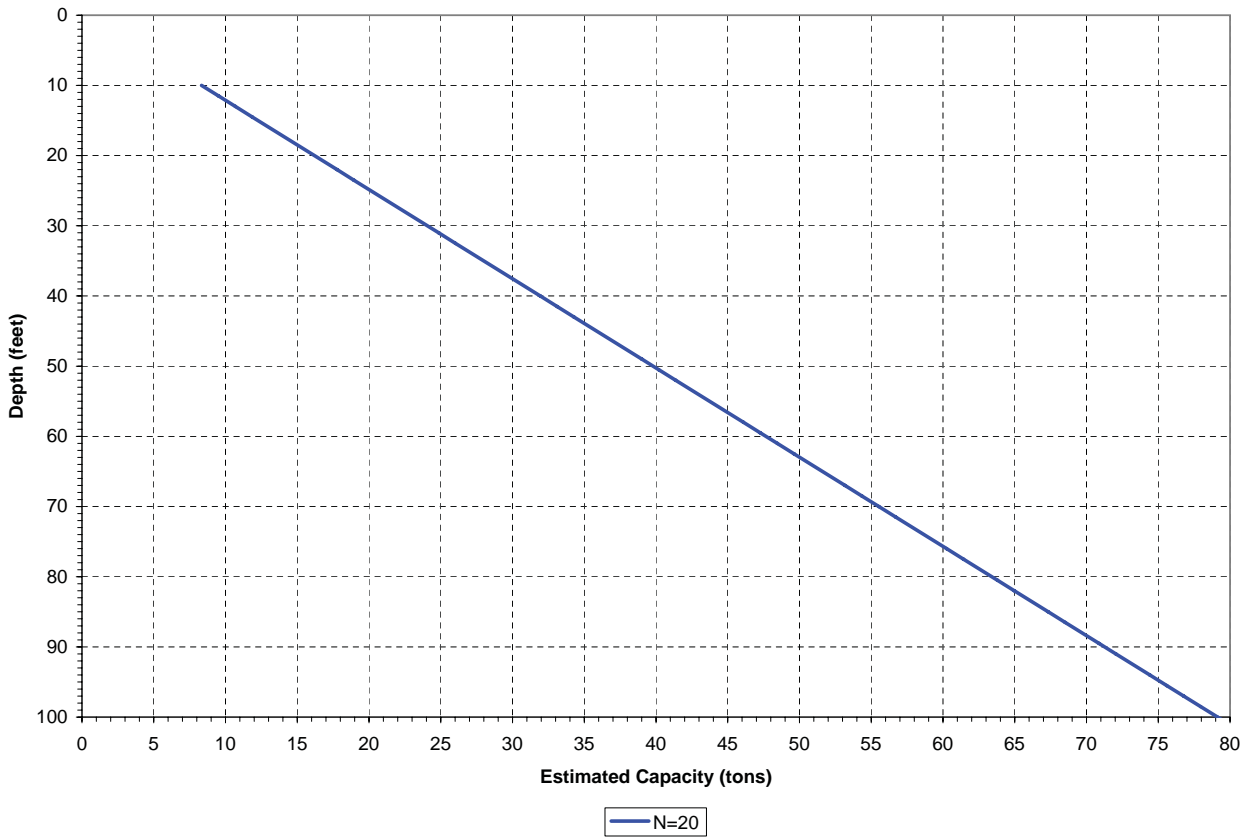
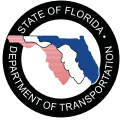


Figure 7: 10 HP 42 Piles - "Standardized Curve"

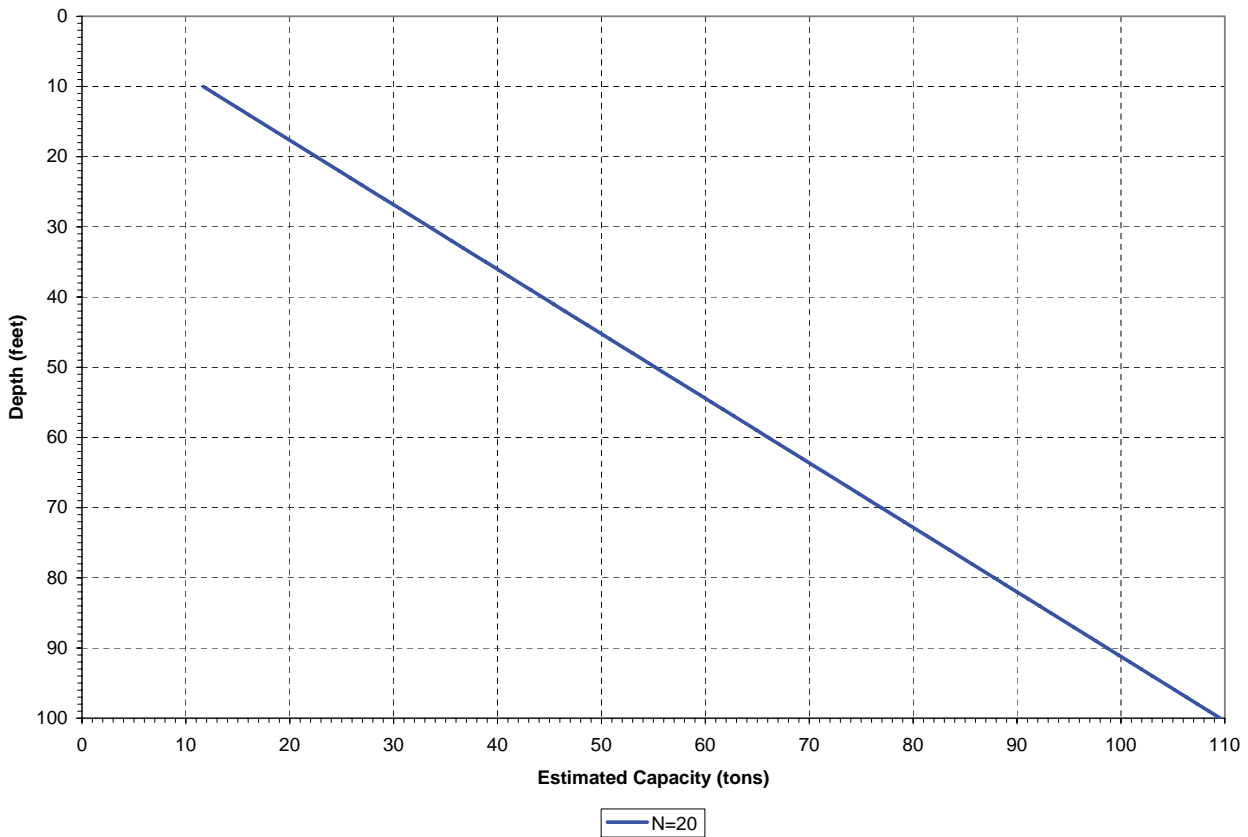


Figure 8: 14 HP 73 Piles - "Standardized Curve"

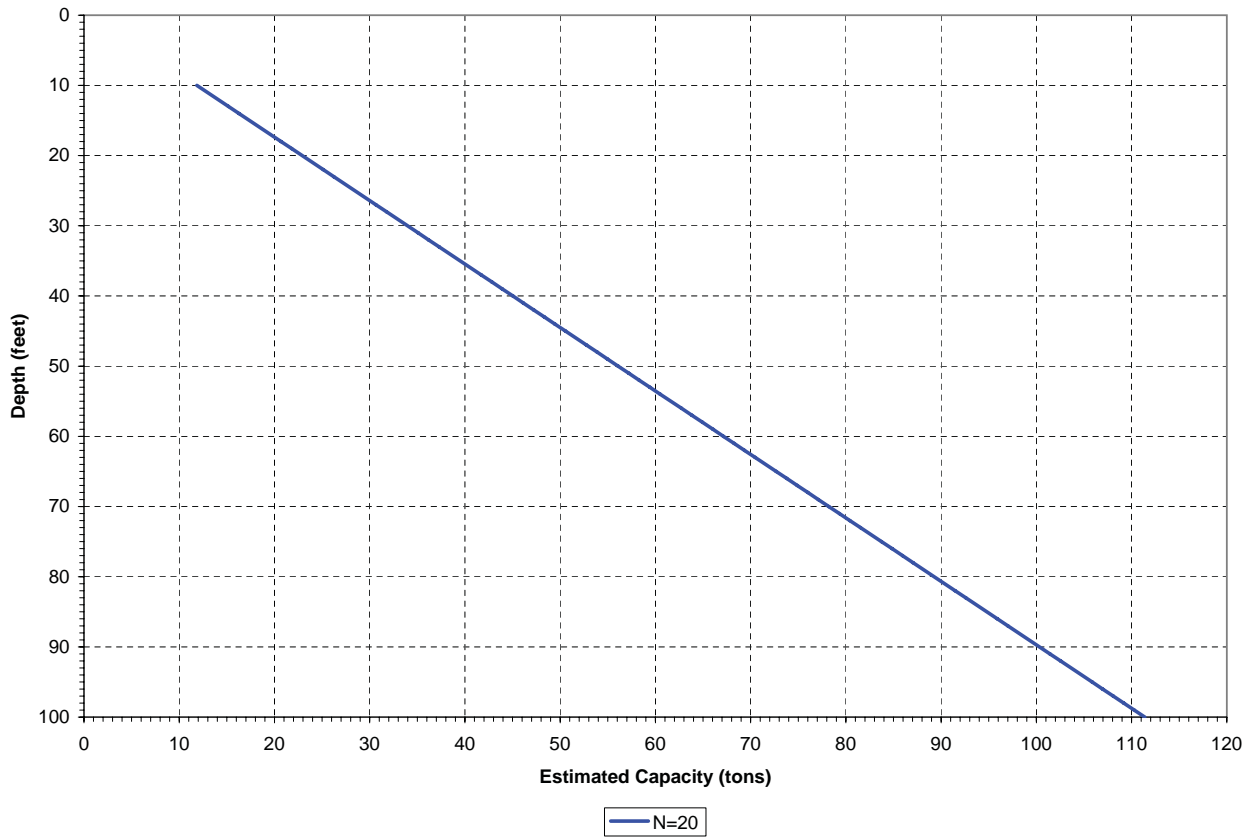
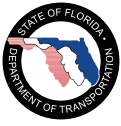


Figure 9: 14 HP 89 Pile - "Standardized Curve"



Appendix D

The following items are included in Appendix D:

- Rapid Scour Estimation Graphs



Rapid Scour Estimation Graphs

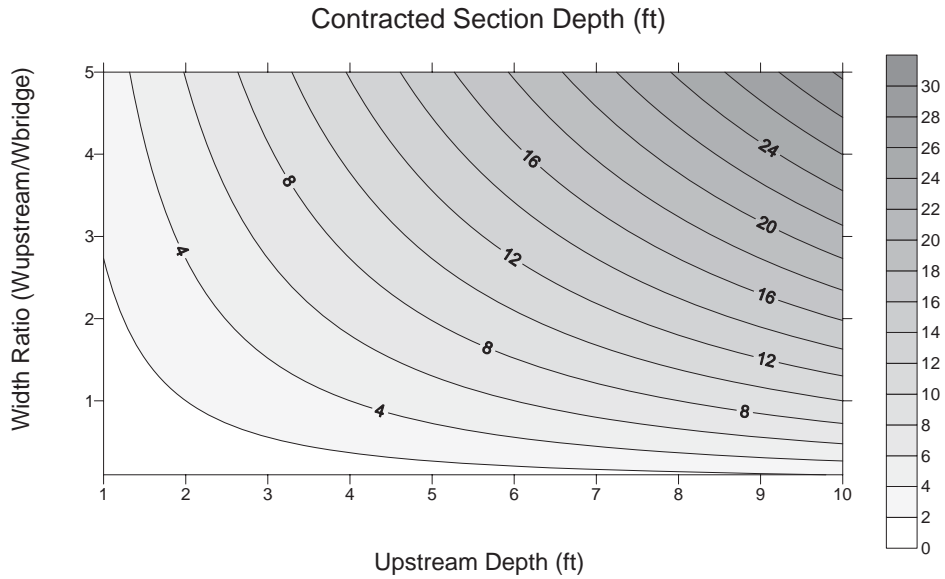


Figure 1 Contracted Section Depth as a Function of Upstream Depth and Width Ratio

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

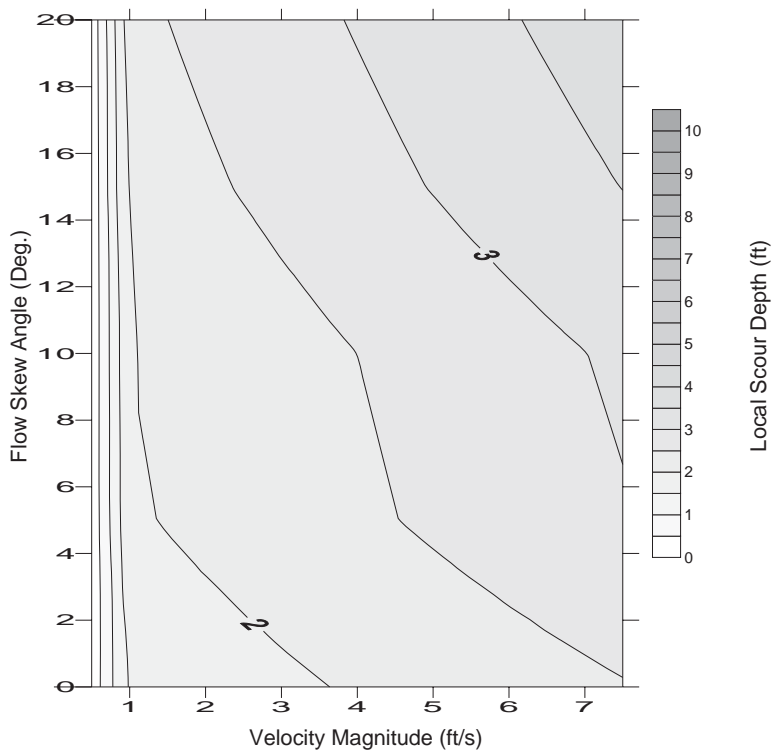
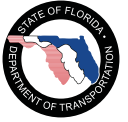


Figure 2 Local Scour Plot for a Group of Four 12" Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

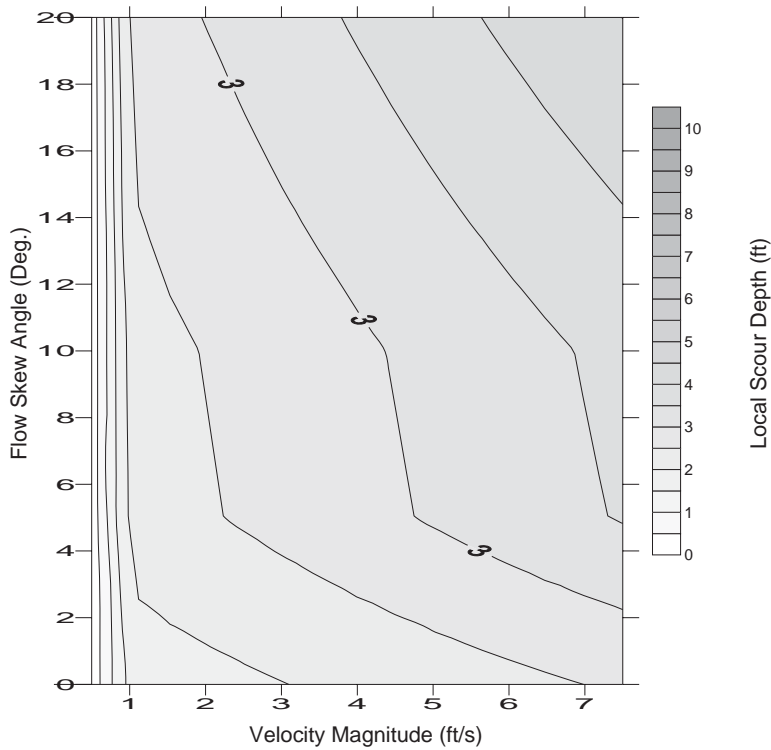


Figure 3 Local Scour Plot for a Group of Six 12'' Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

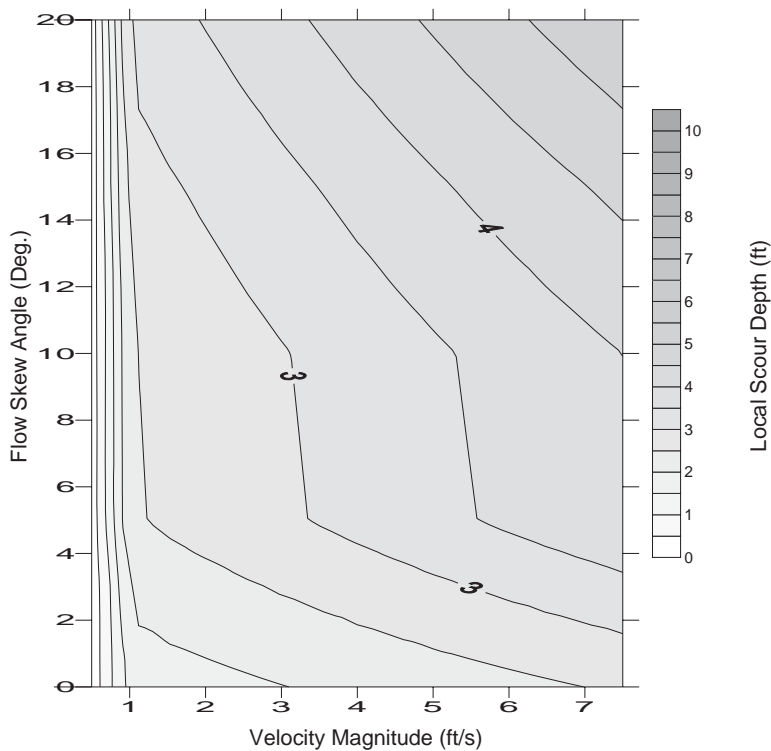
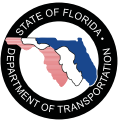


Figure 4 Local Scour Plot for a Group of Eight 12'' Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

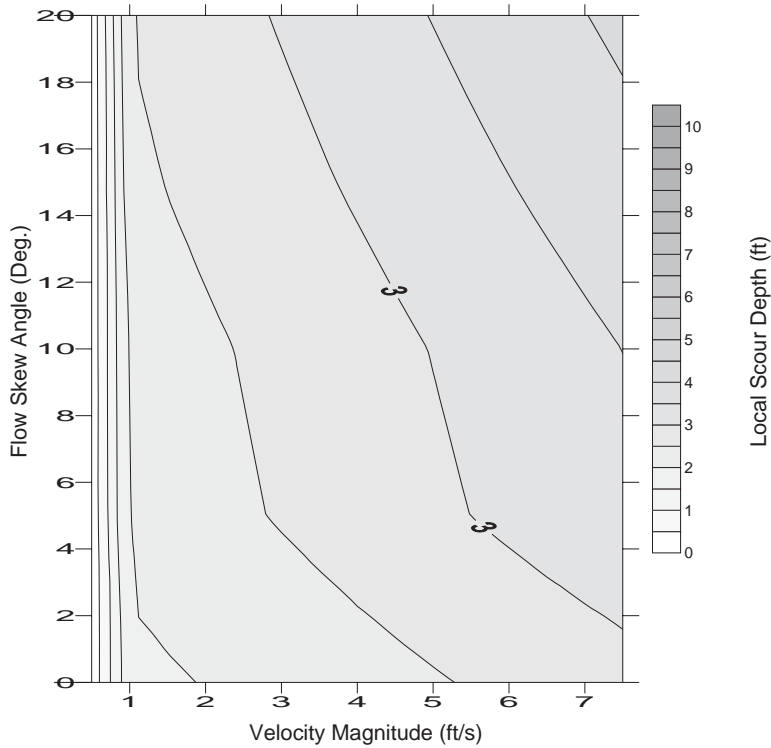


Figure 5 Local Scour Plot for a Group of Four 14' Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

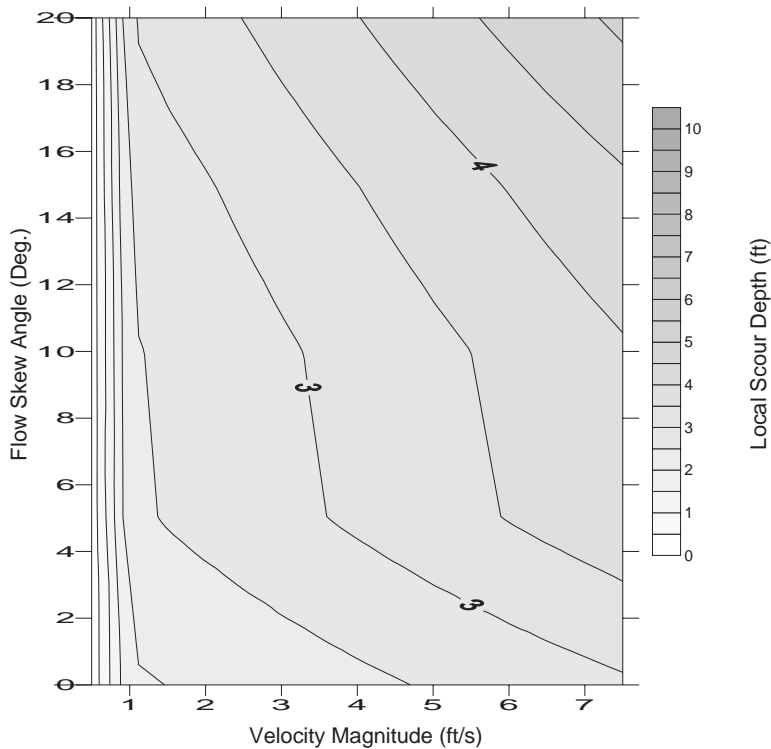
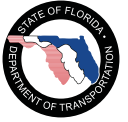


Figure 6 Local Scour Plot for a Group of Six 14' Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

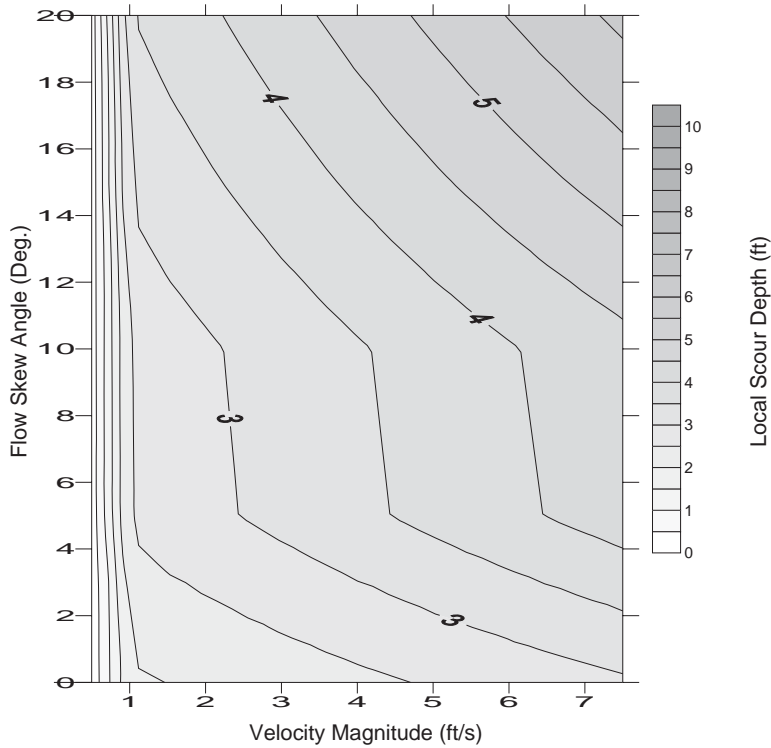


Figure 7 Local Scour Plot for a Group of Eight 14' Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

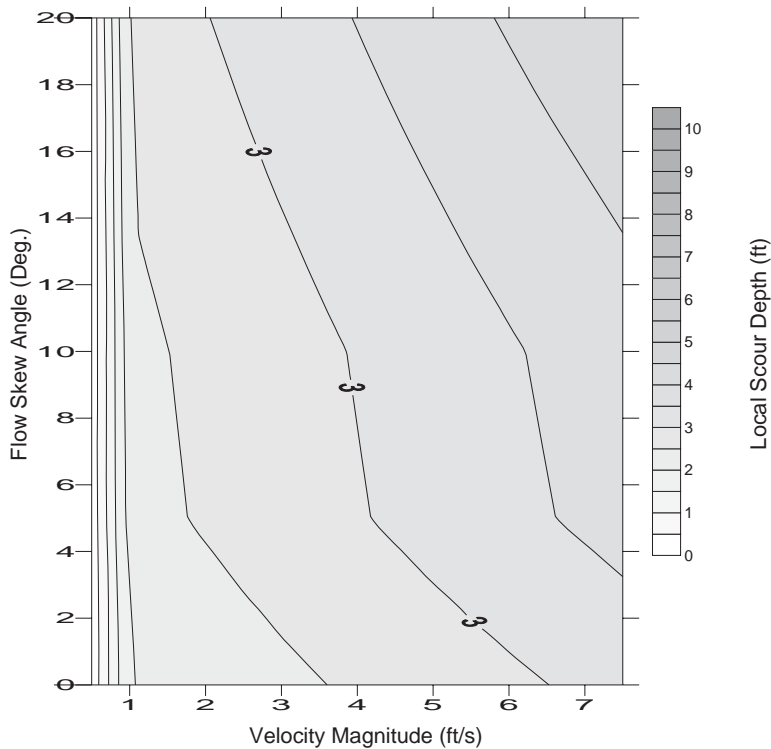
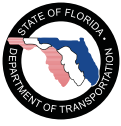


Figure 8 Local Scour Plot for a Group of Four 16' Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

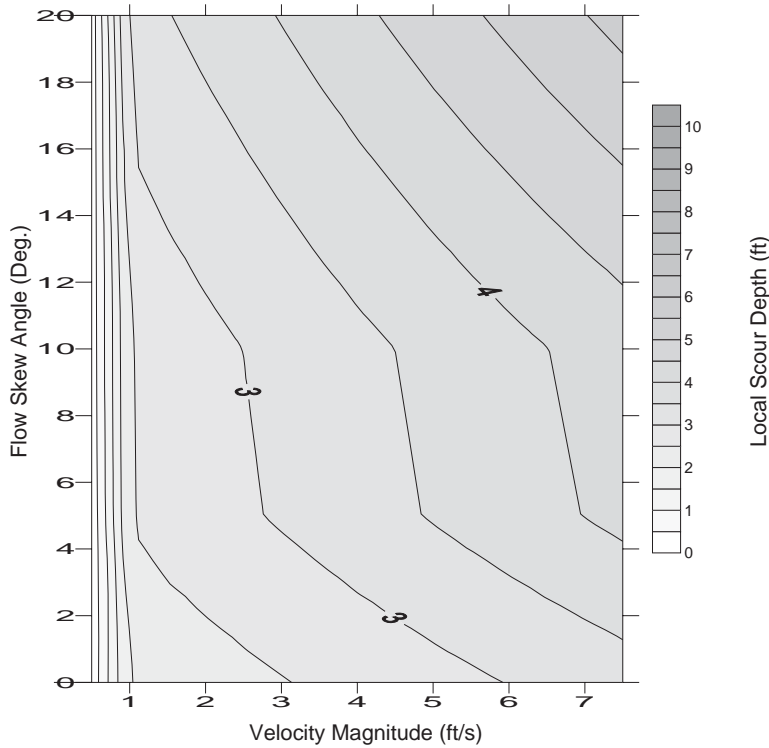


Figure 9 Local Scour Plot for a Group of Six 16' Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

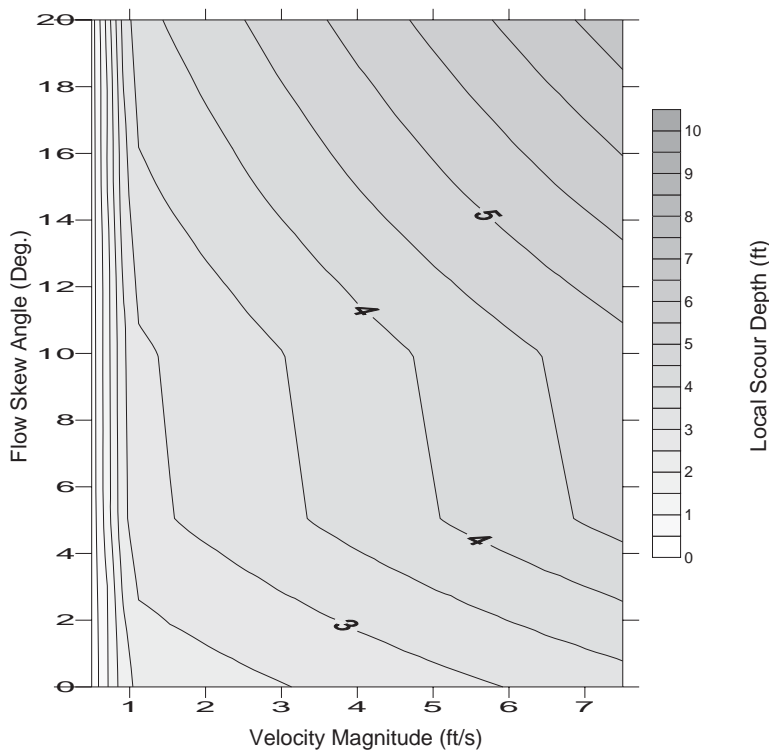
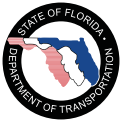


Figure 10 Local Scour Plot for a Group of Eight 16' Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

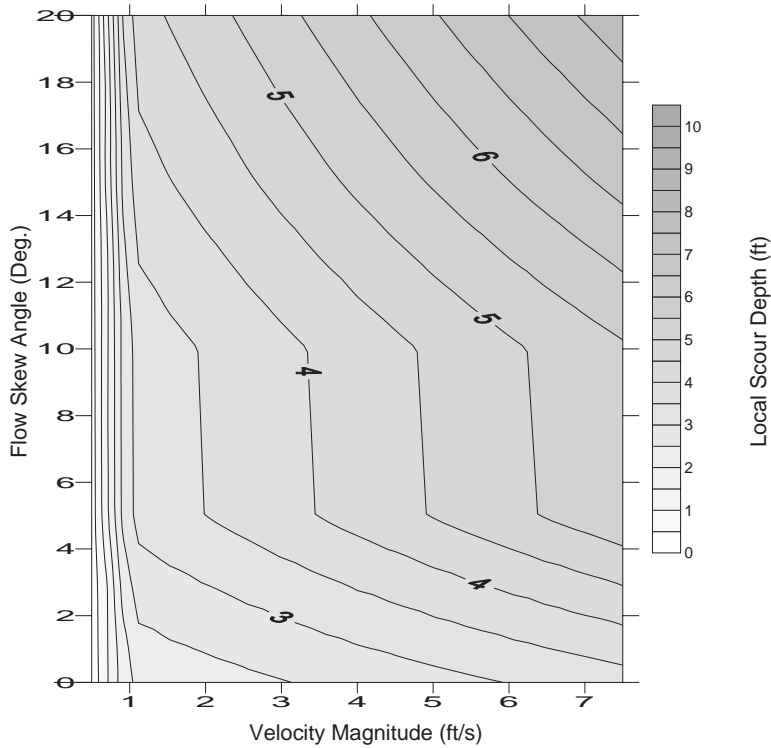


Figure 11 Local Scour Plot for a Group of Ten 16" Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

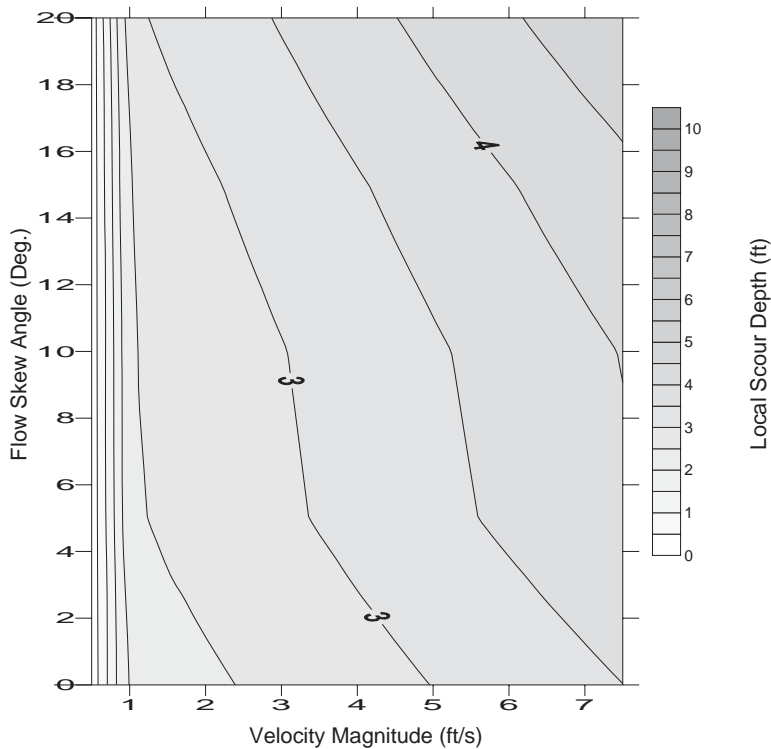
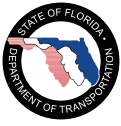


Figure 12 Local Scour Plot for a Group of Four 18" Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

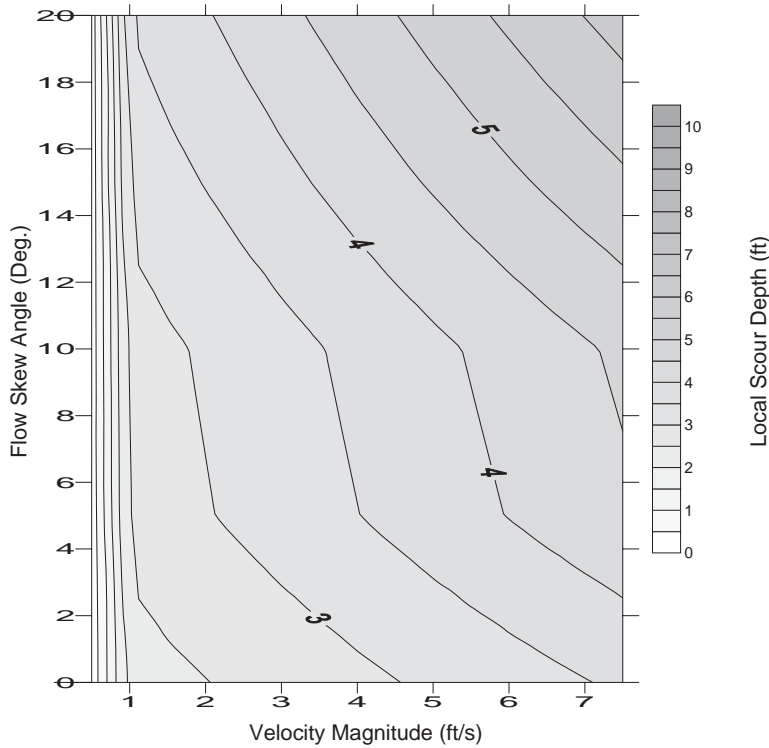


Figure 13 Local Scour Plot for a Group of Six 18" Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

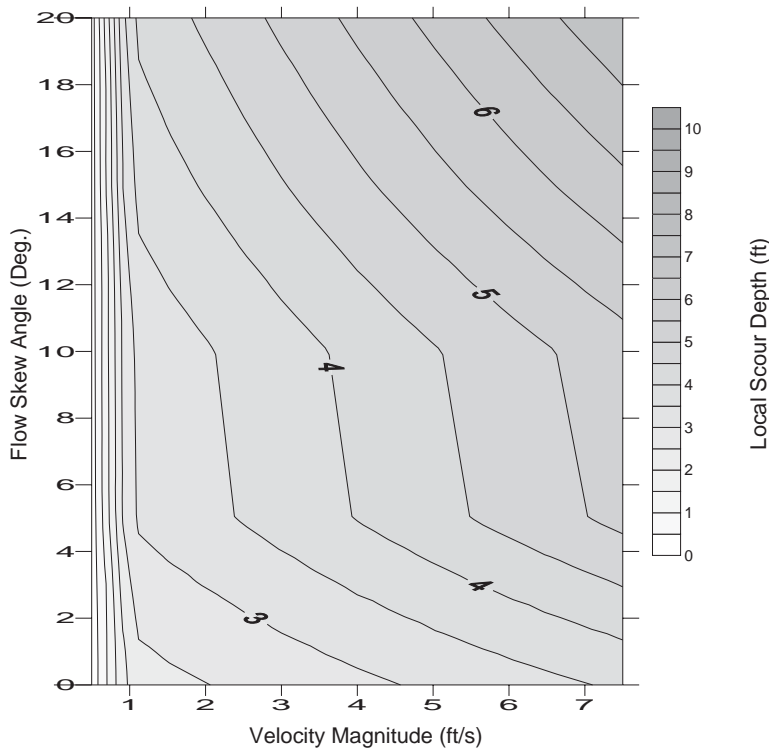
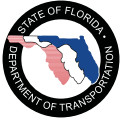


Figure 14 Local Scour Plot for a Group of Eight 18" Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

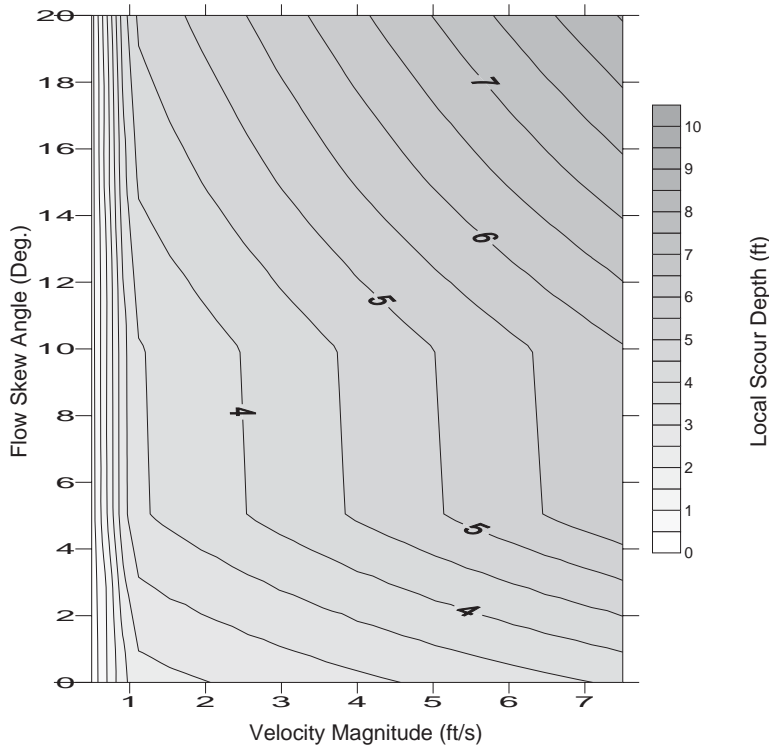


Figure 15 Local Scour Plot for a Group of Ten 18" Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

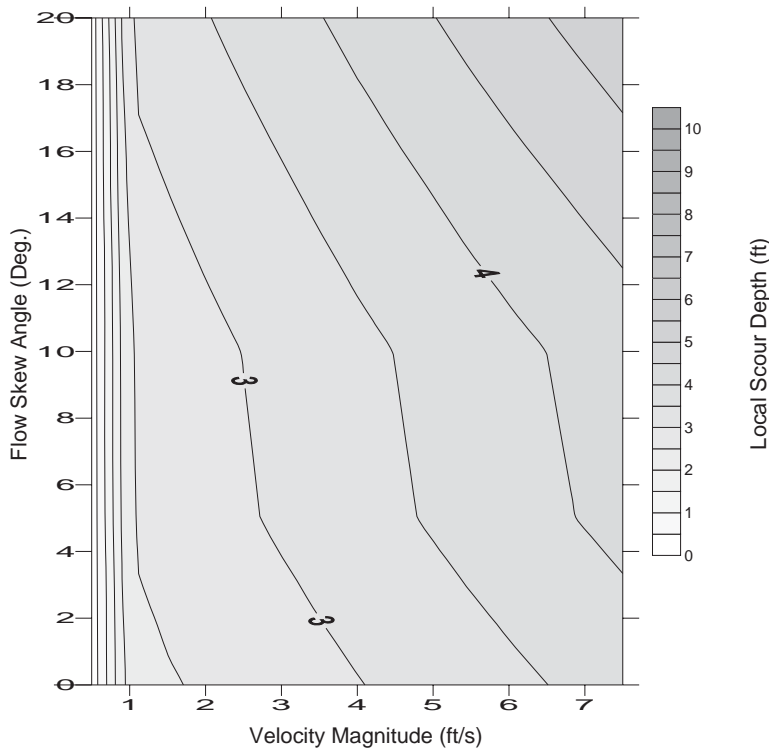
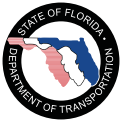


Figure 16 Local Scour Plot for a Group of Four 20" Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

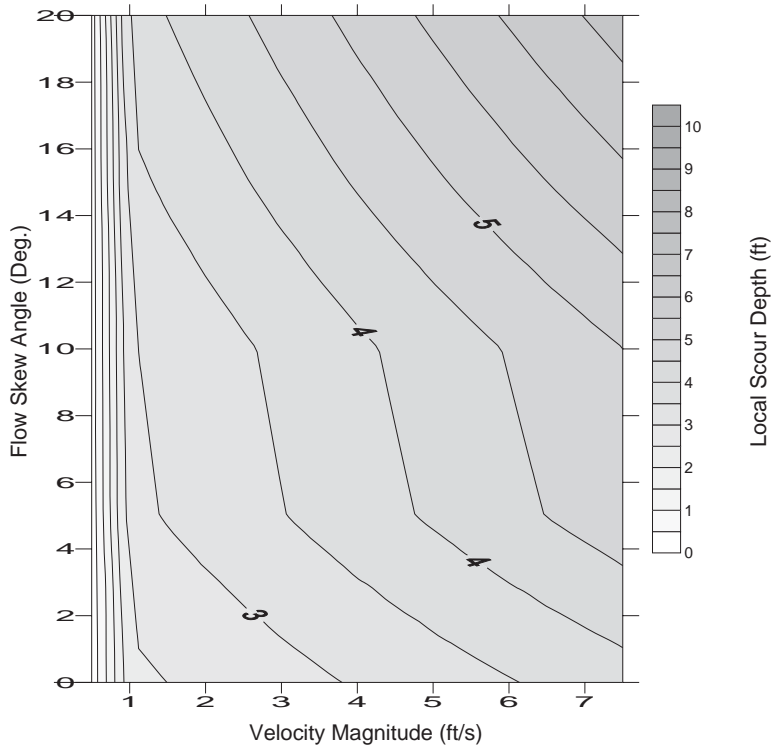


Figure 17 Local Scour Plot for a Group of Six 20" Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

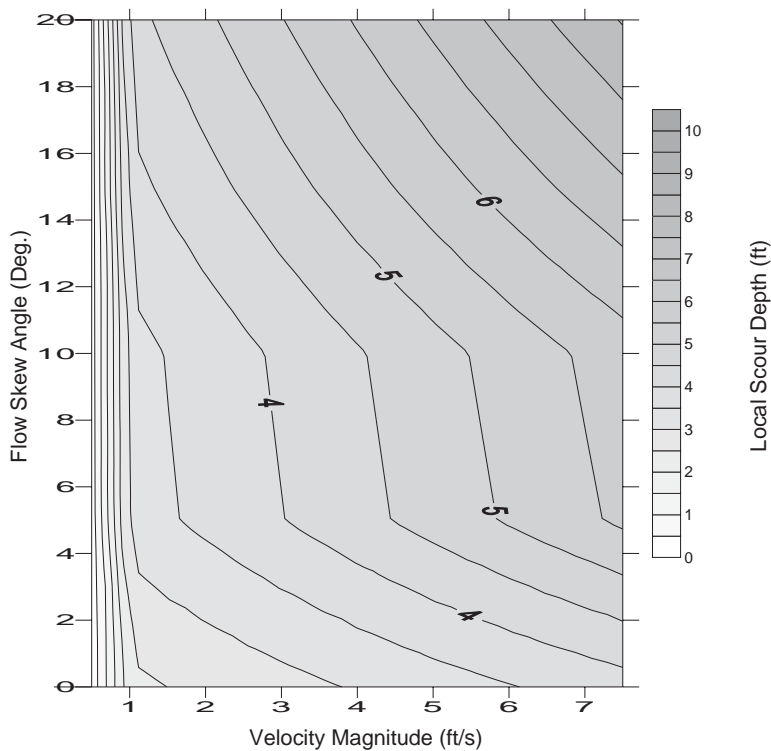
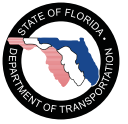


Figure 18 Local Scour Plot for a Group of Eight 20" Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

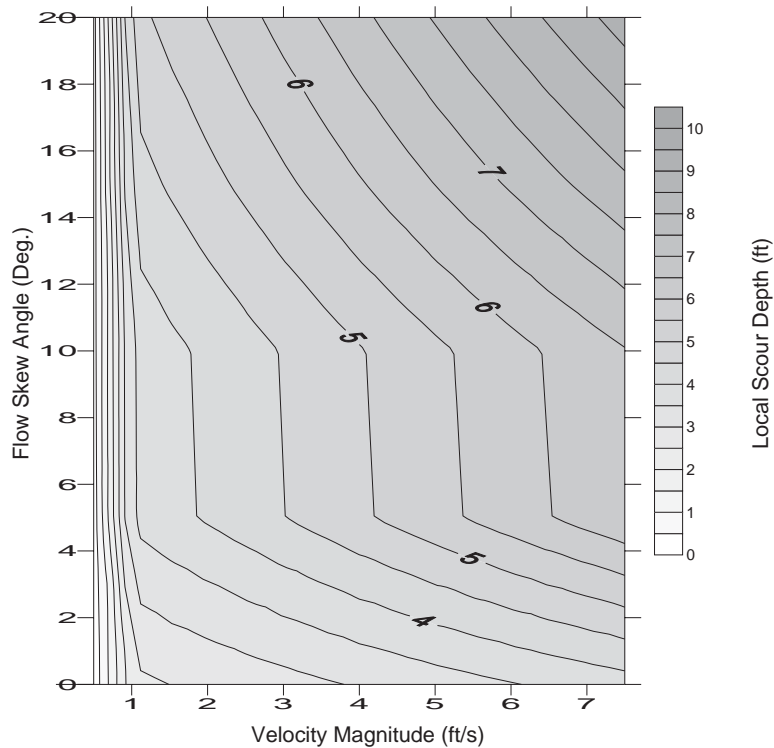


Figure 19 Local Scour Plot for a Group of Ten 20'' Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

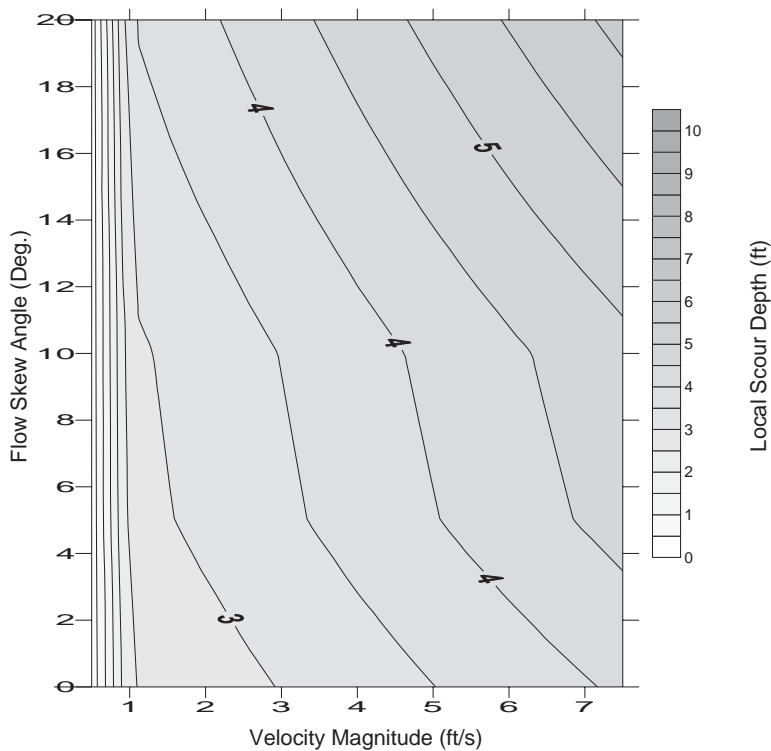
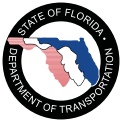


Figure 20 Local Scour Plot for a Group of Four 24'' Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

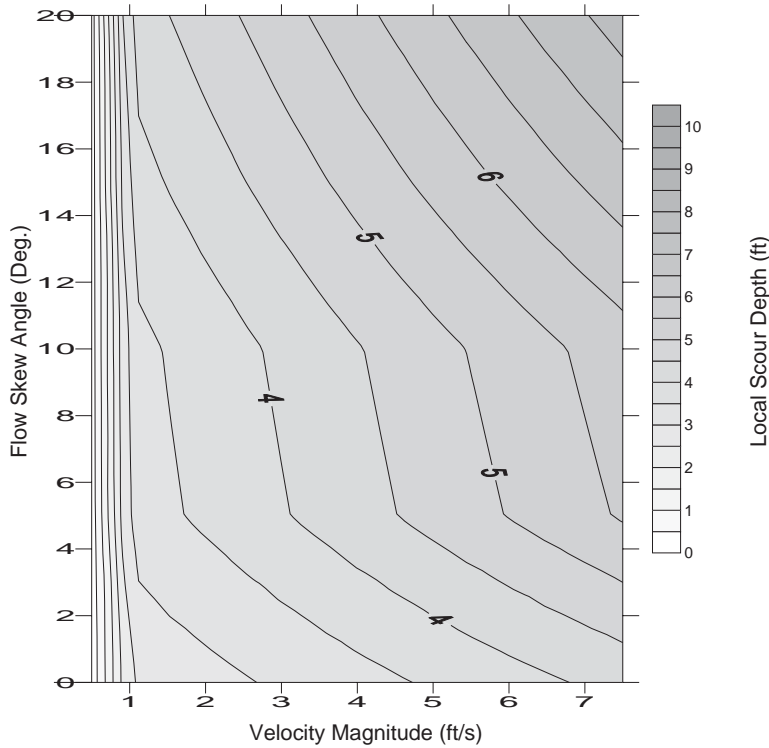


Figure 21 Local Scour Plot for a Group of Six 24' Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

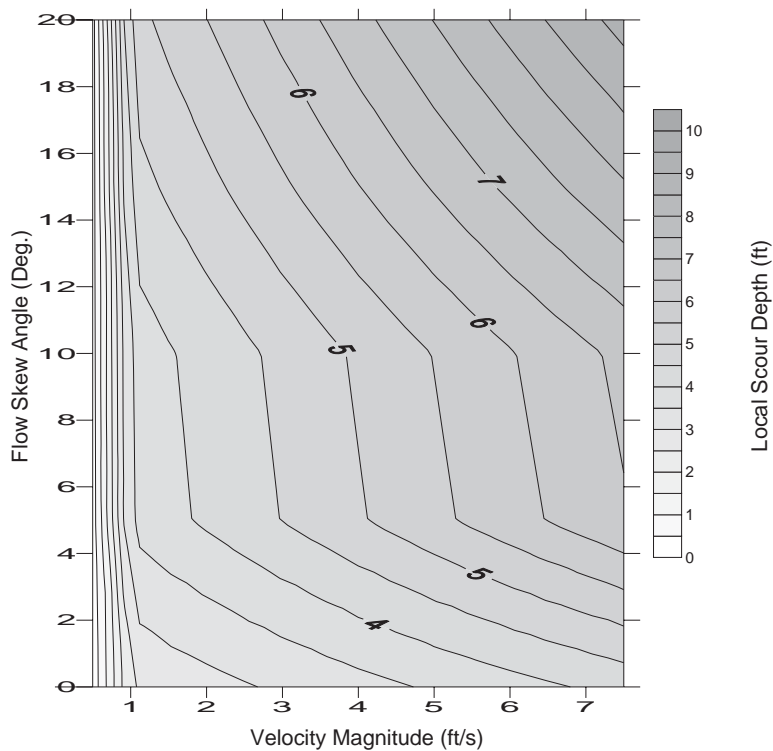
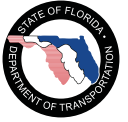


Figure 22 Local Scour Plot for a Group of Eight 24' Piles ($D_{50} = 0.15$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

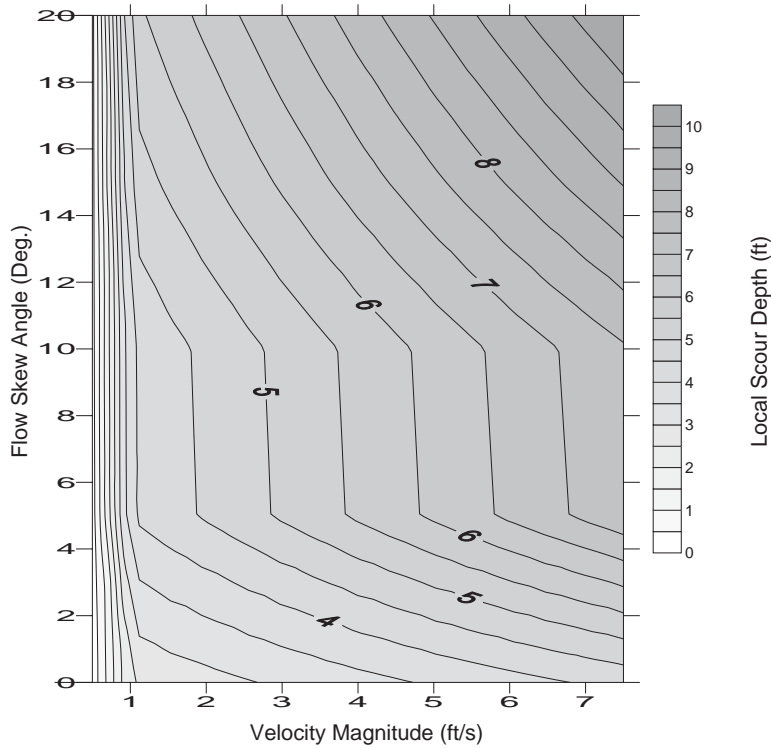


Figure 23 Local Scour Plot for a Group of Ten 24" Piles ($D_{50} = 0.15$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

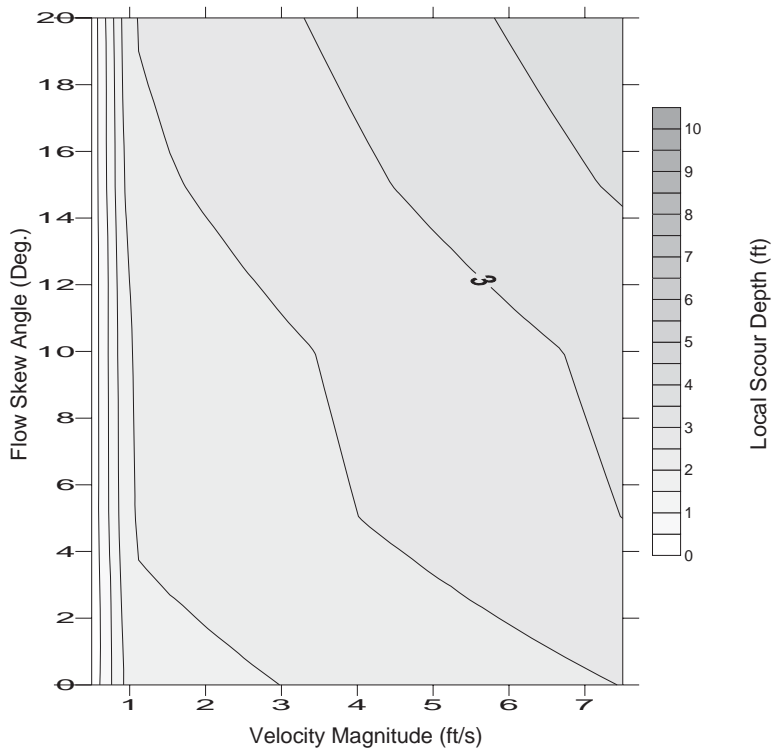
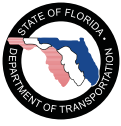


Figure 24 Local Scour Plot for a Group of Four 12" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

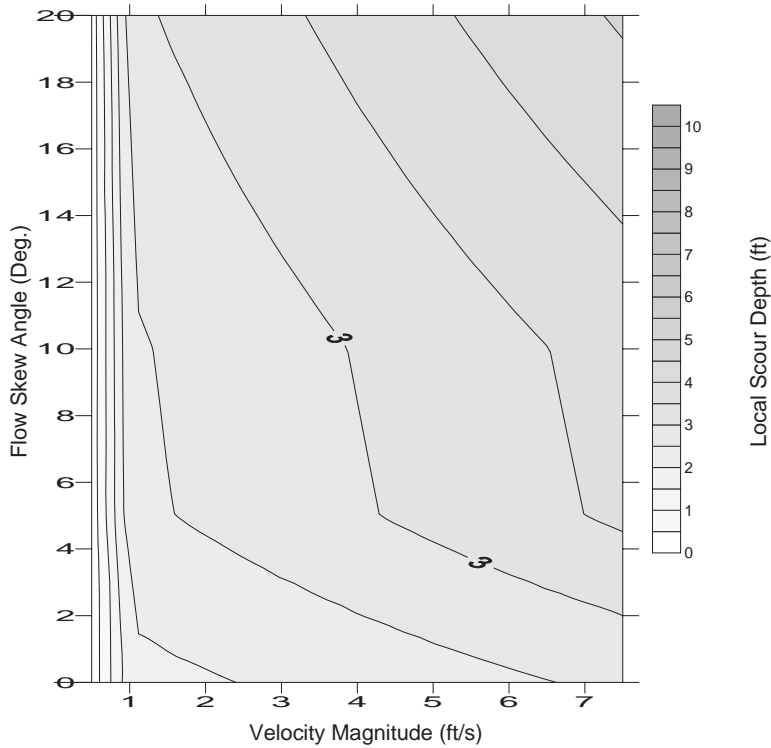


Figure 25 Local Scour Plot for a Group of Six 12" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

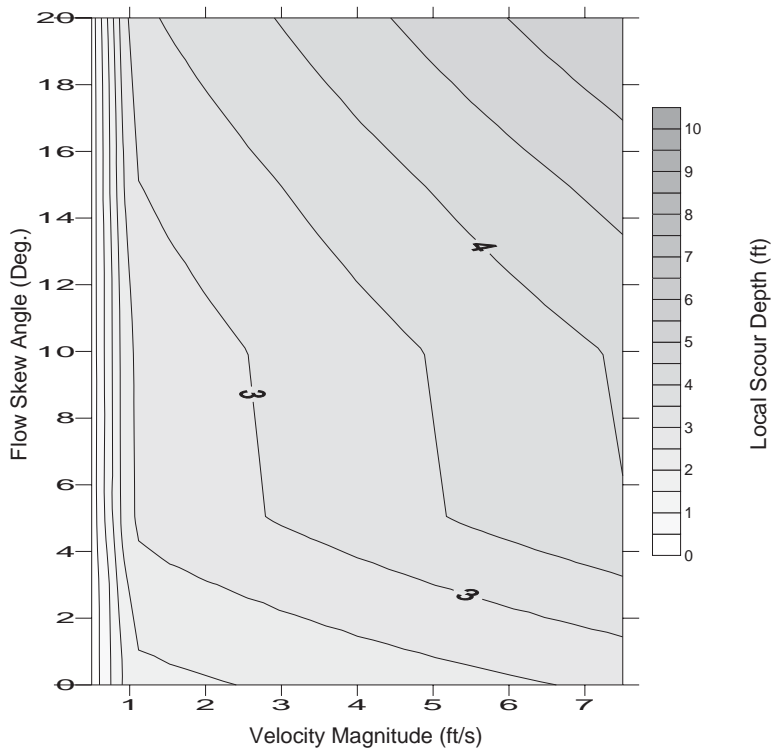
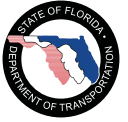


Figure 26 Local Scour Plot for a Group of Eight 12" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

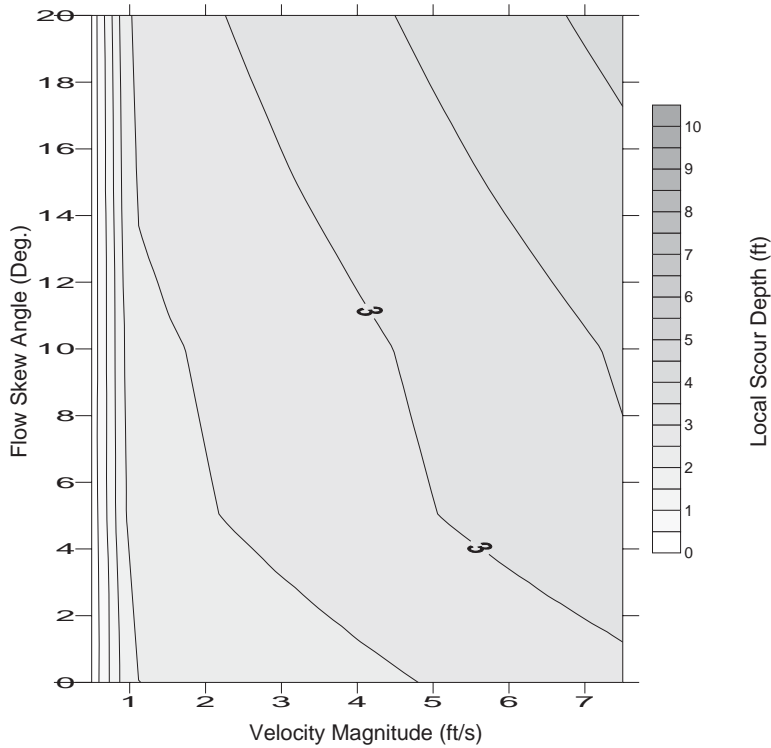


Figure 27 Local Scour Plot for a Group of Four 14' Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

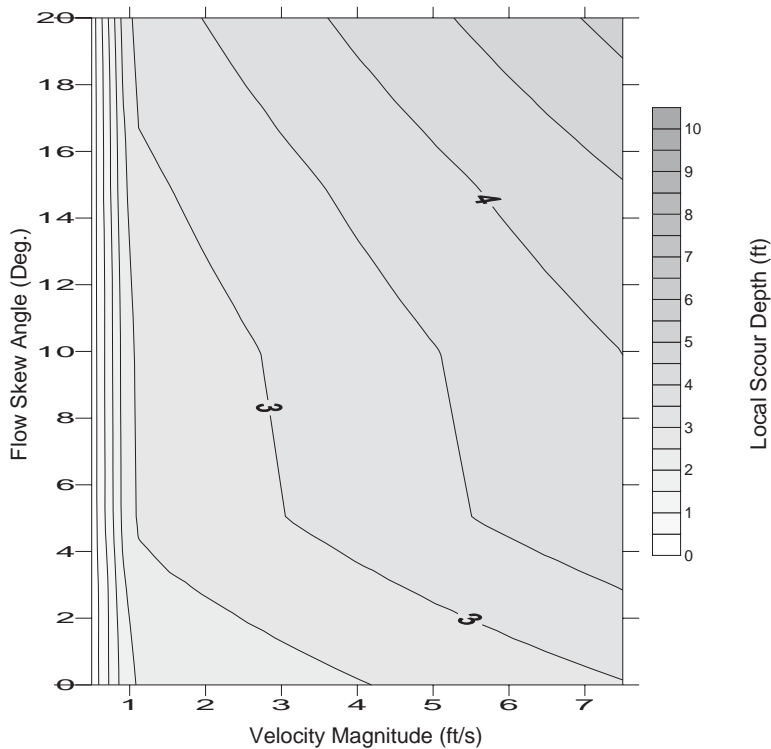
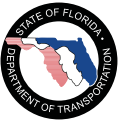


Figure 28 Local Scour Plot for a Group of Six 14' Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

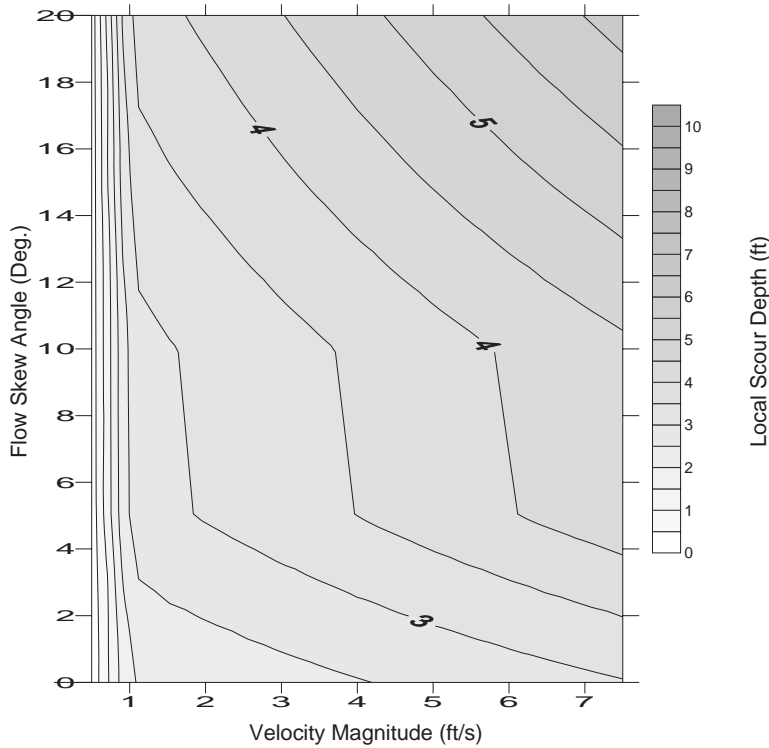


Figure 29 Local Scour Plot for a Group of Eight 14' Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

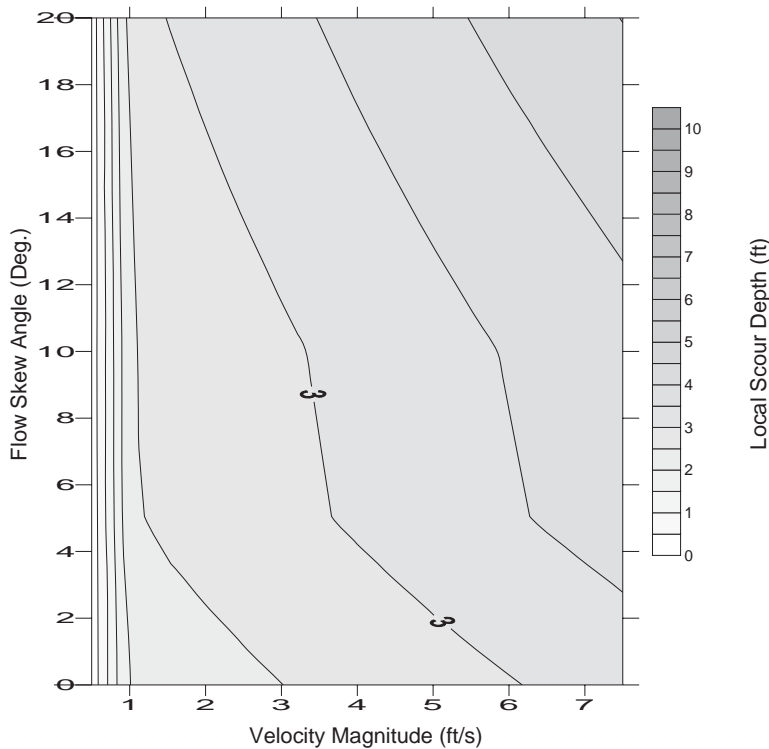
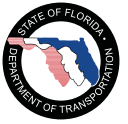


Figure 30 Local Scour Plot for a Group of Four 16' Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

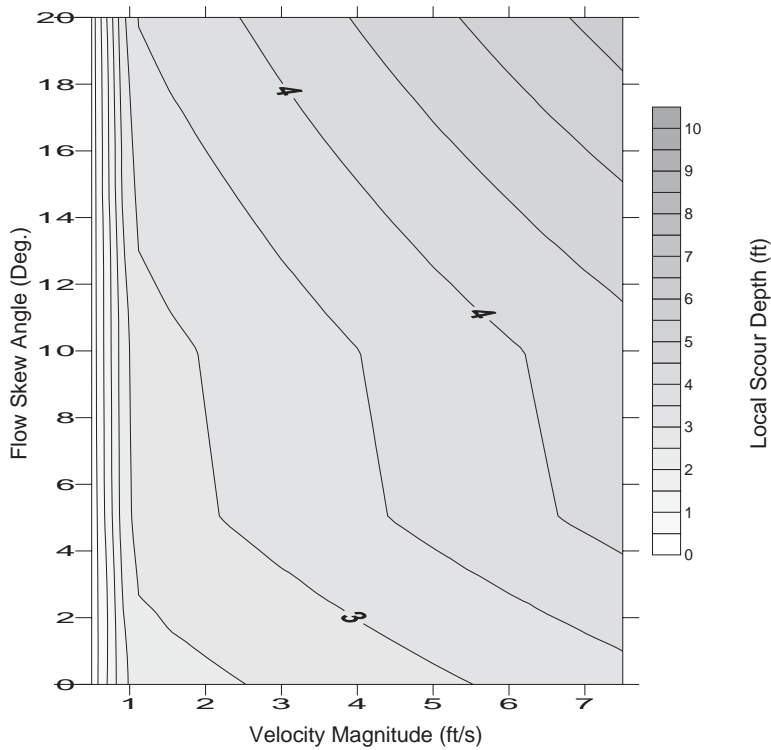


Figure 31 Local Scour Plot for a Group of Six 16' Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

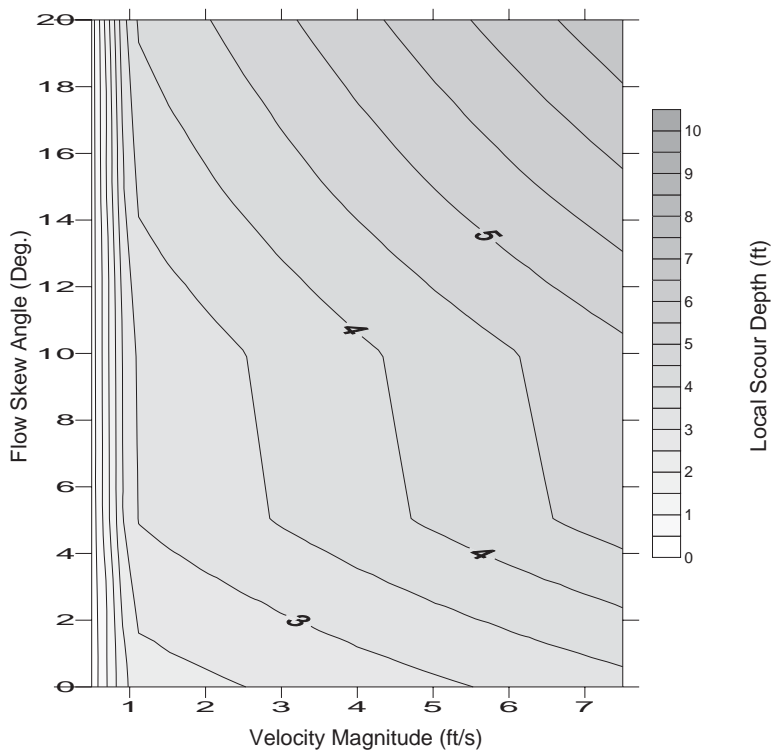
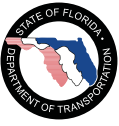


Figure 32 Local Scour Plot for a Group of Eight 16' Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

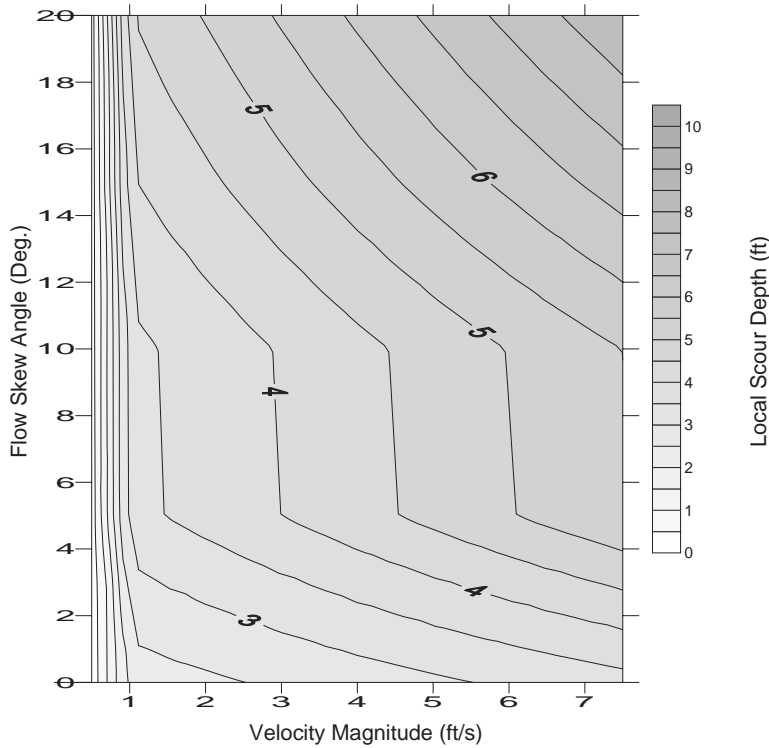


Figure 33 Local Scour Plot for a Group of Ten 16" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

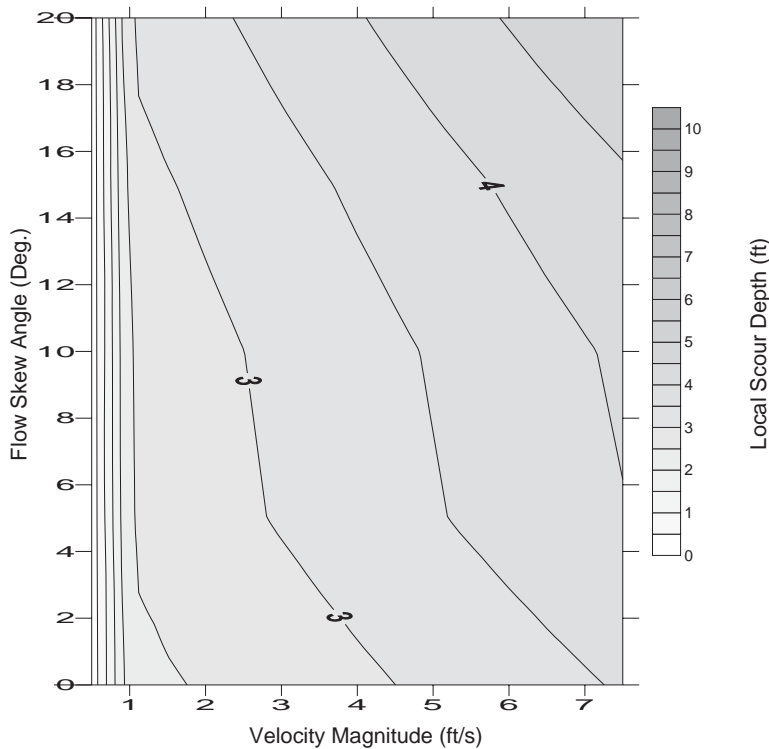
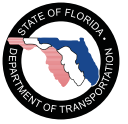


Figure 34 Local Scour Plot for a Group of Four 18" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

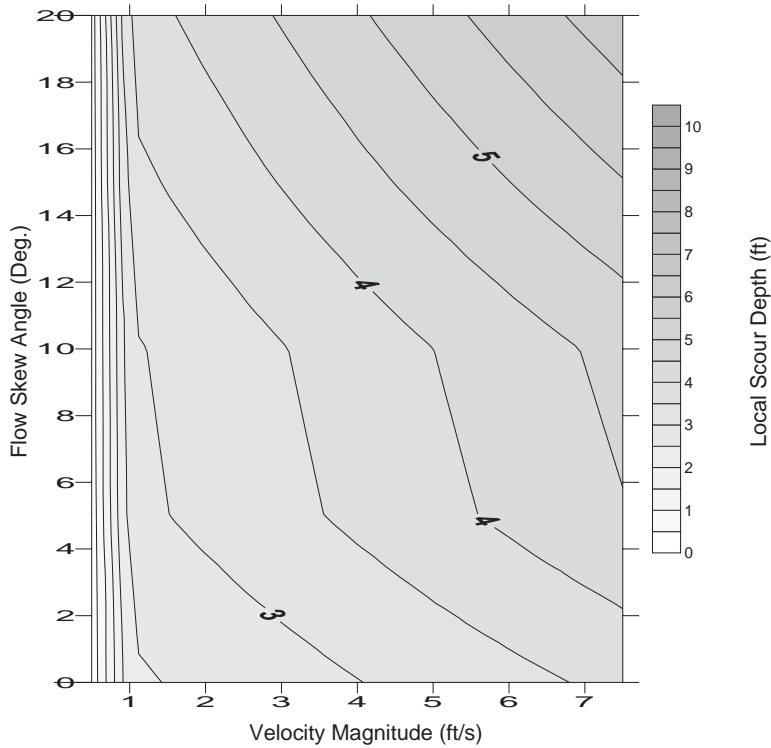


Figure 35 Local Scour Plot for a Group of Six 18" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

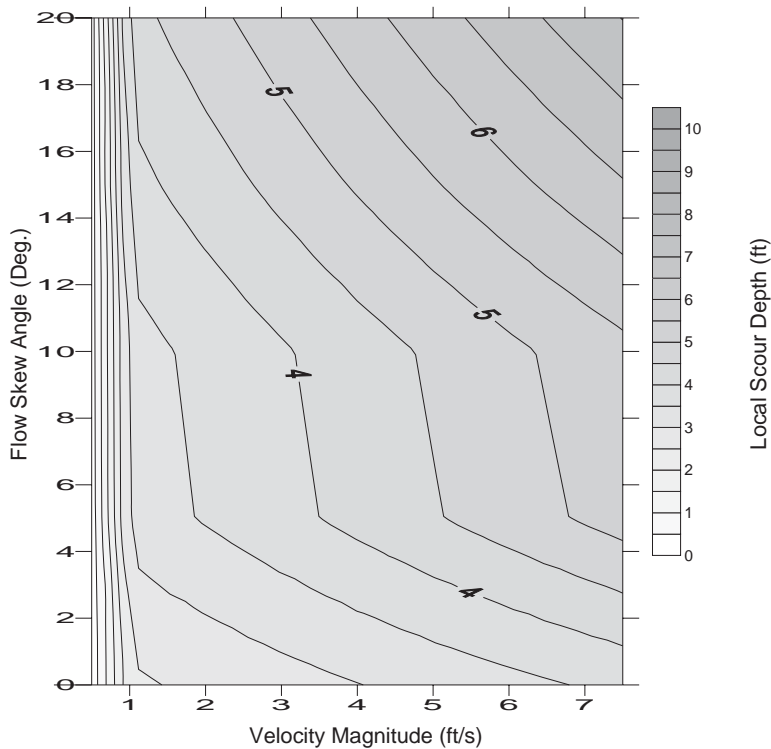
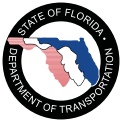


Figure 36 Local Scour Plot for a Group of Eight 18" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

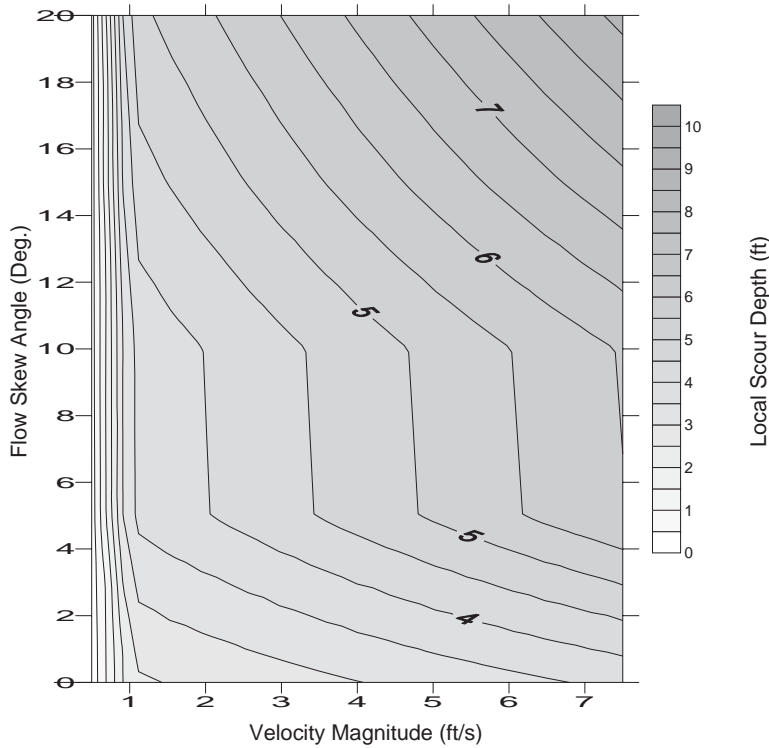


Figure 37 Local Scour Plot for a Group of Ten 18" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

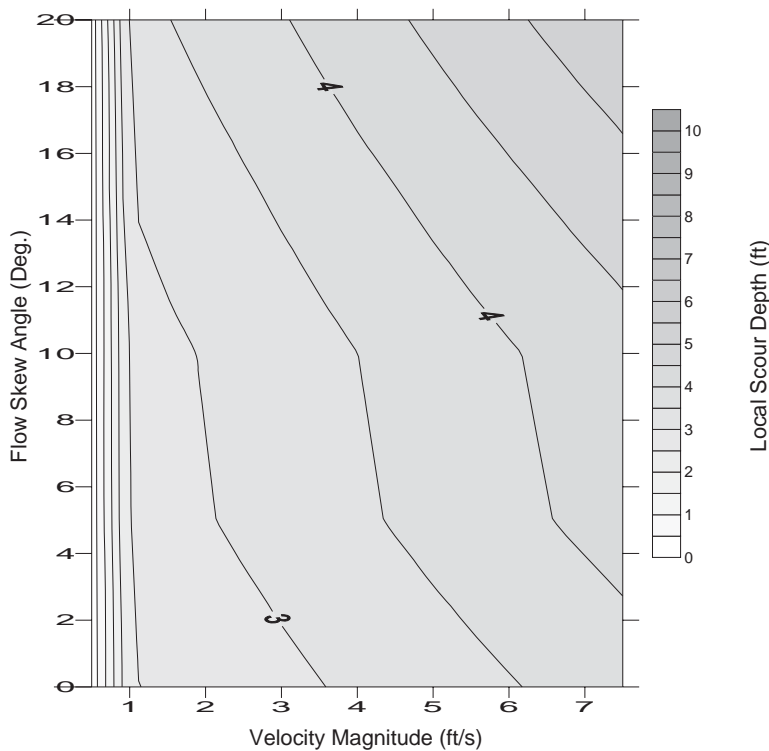
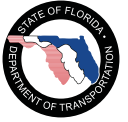


Figure 38 Local Scour Plot for a Group of Four 20" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

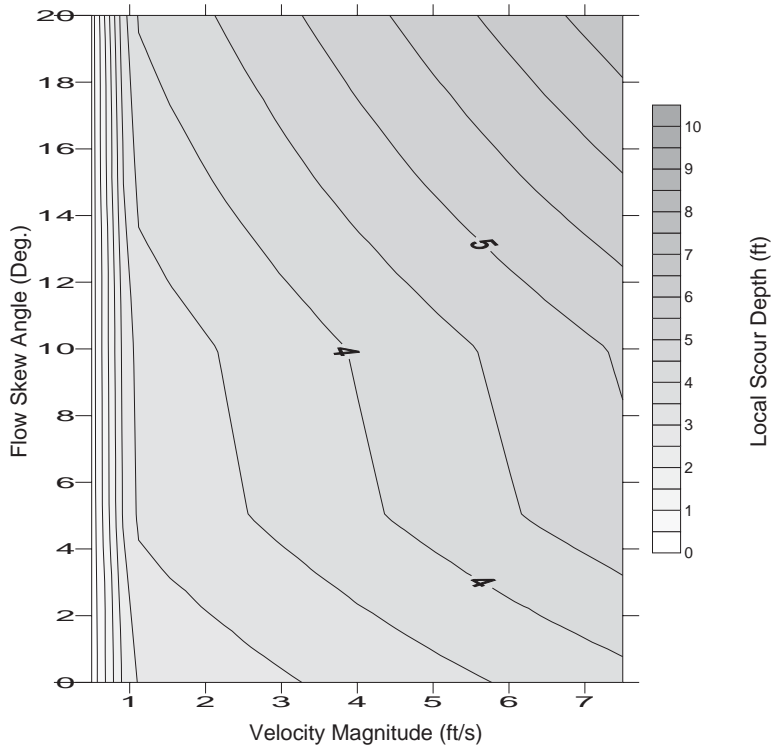


Figure 39 Local Scour Plot for a Group of Six 20" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

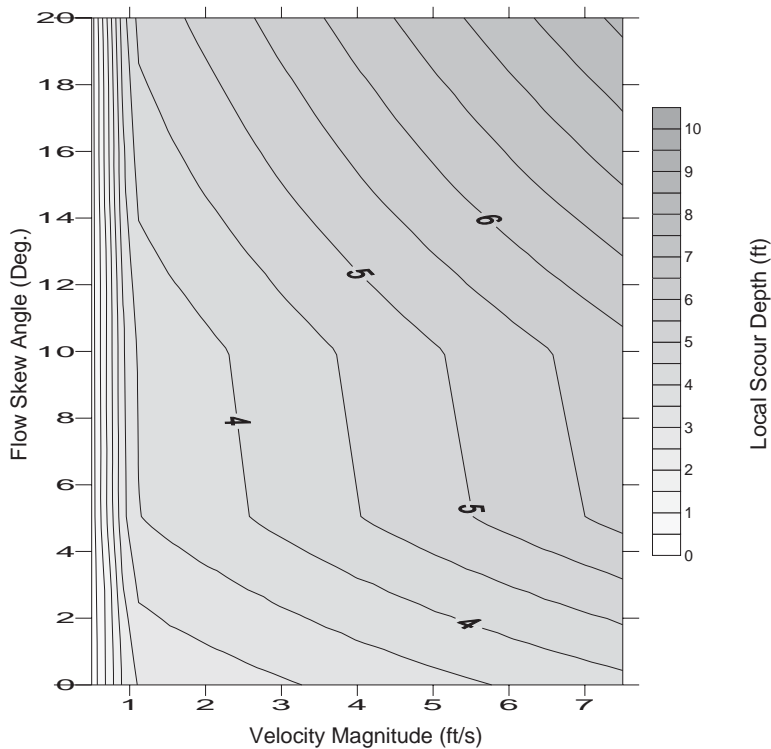
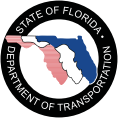


Figure 40 Local Scour Plot for a Group of Eight 20" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

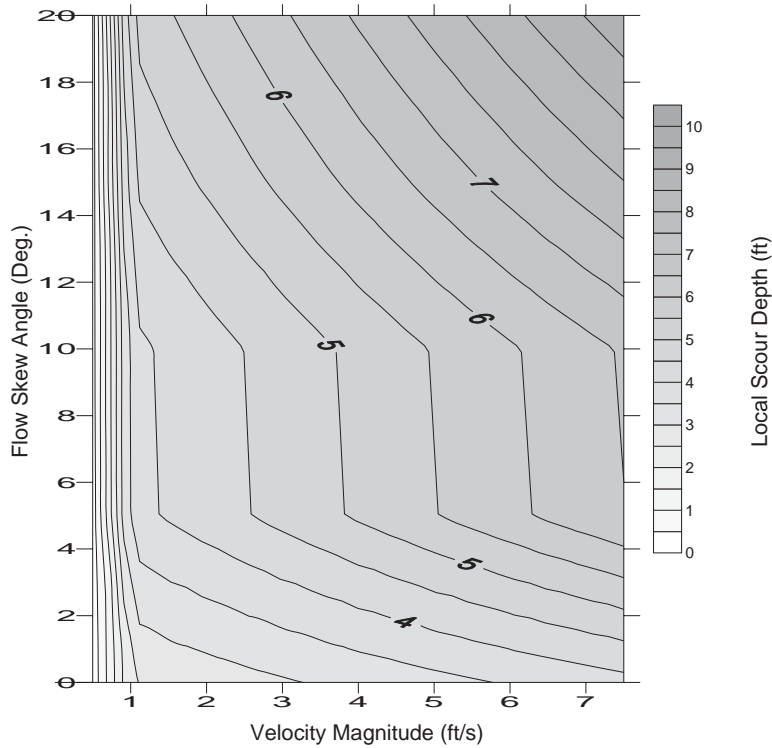


Figure 41 Local Scour Plot for a Group of Ten 20" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

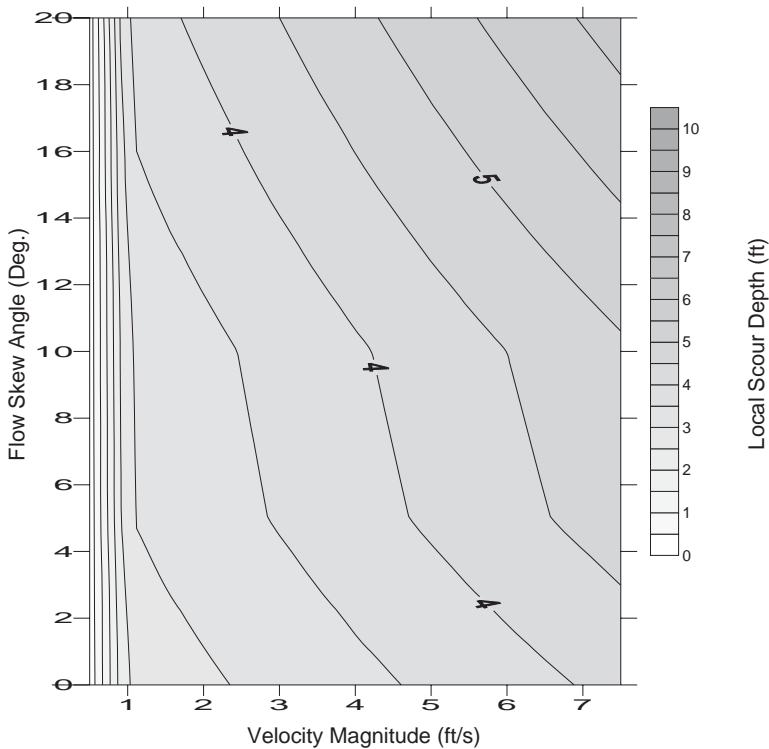
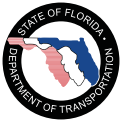


Figure 42 Local Scour Plot for a Group of Four 24" Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

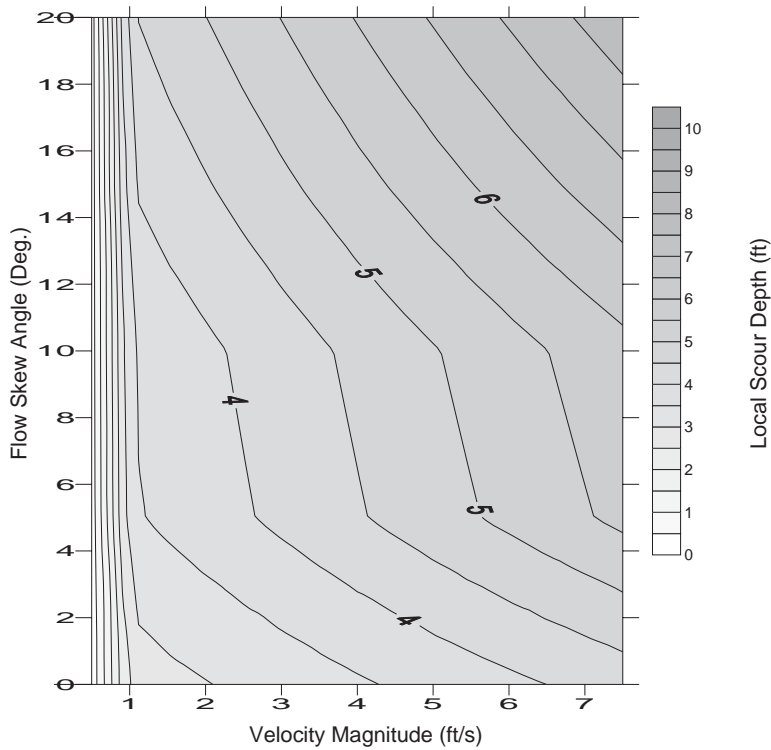


Figure 43 Local Scour Plot for a Group of Six 24' Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

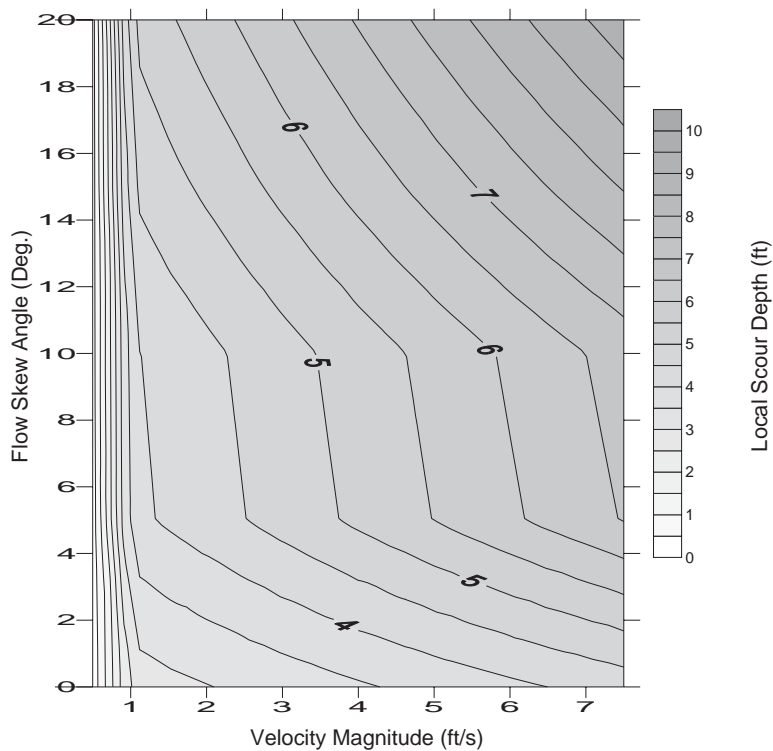
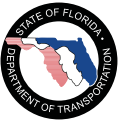


Figure 44 Local Scour Plot for a Group of Eight 24' Piles ($D_{50} = 0.20$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

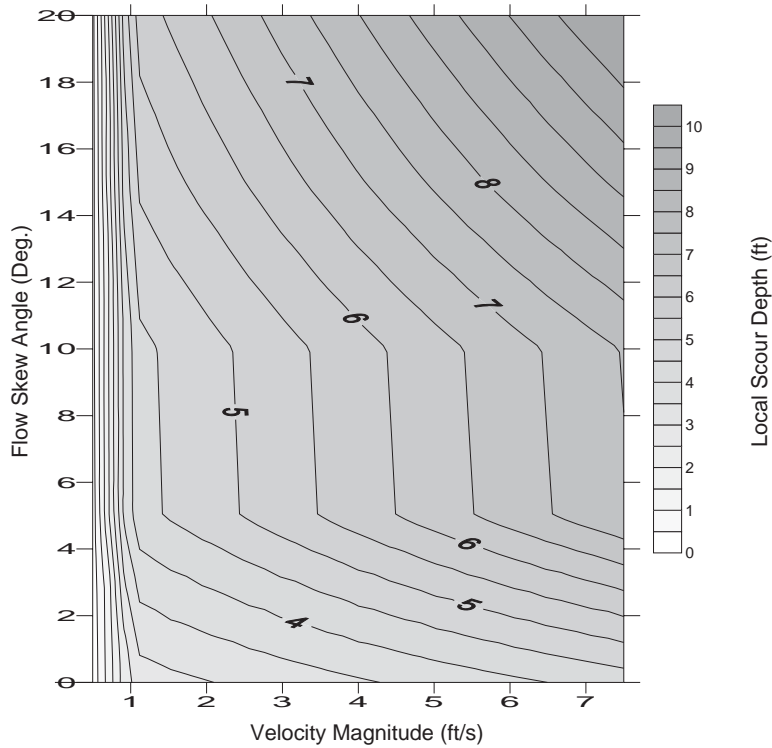


Figure 45 Local Scour Plot for a Group of Ten 24" Piles ($D_{50} = 0.20$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

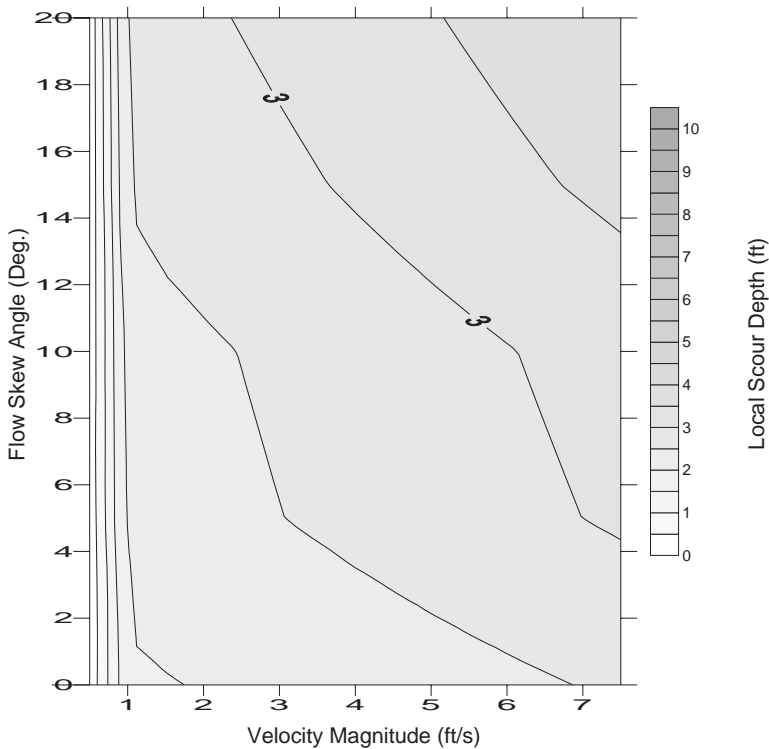
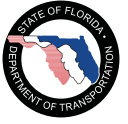


Figure 46 Local Scour Plot for a Group of Four 12" Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

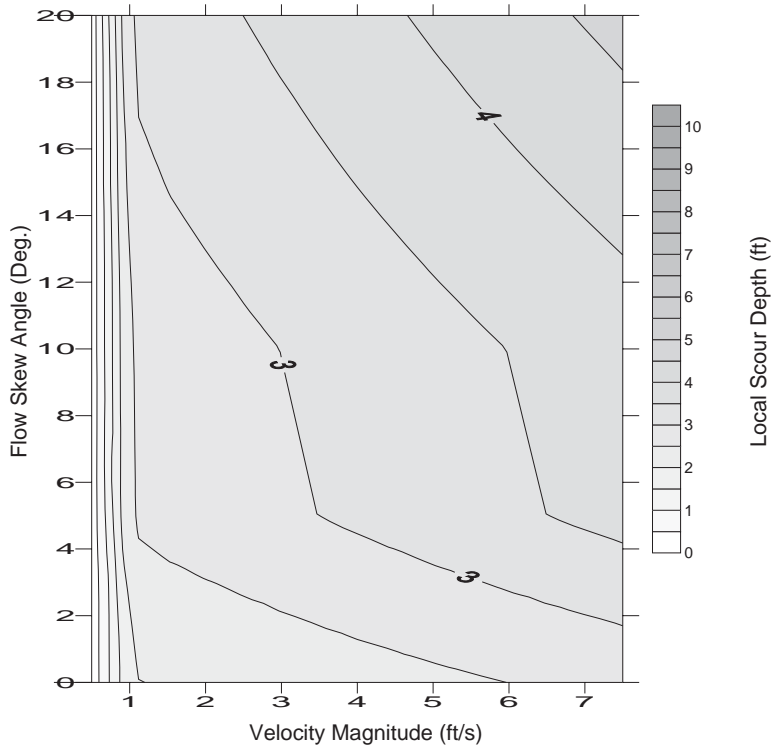


Figure 47 Local Scour Plot for a Group of Six 12" Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

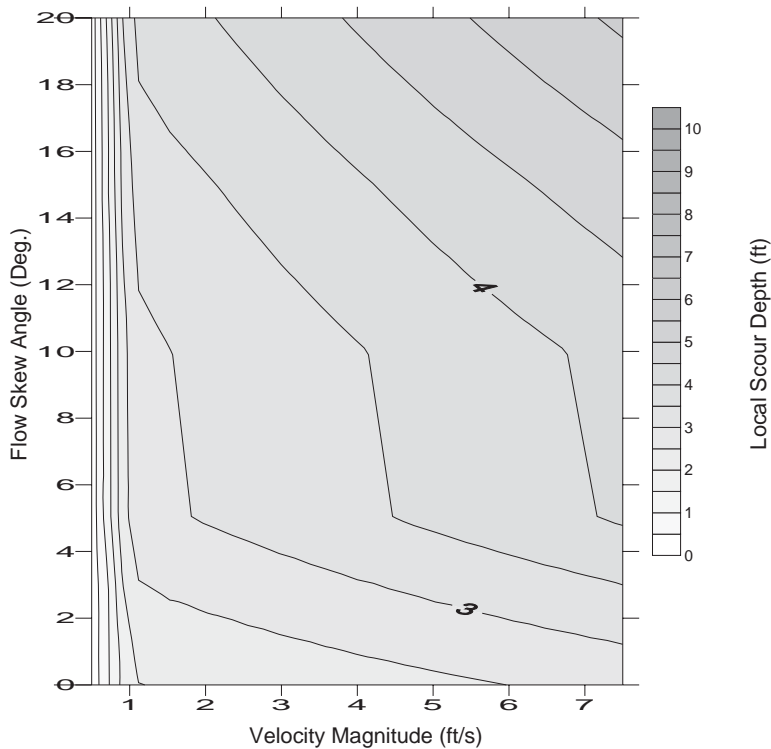
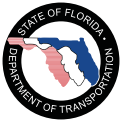


Figure 48 Local Scour Plot for a Group of Eight 12" Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

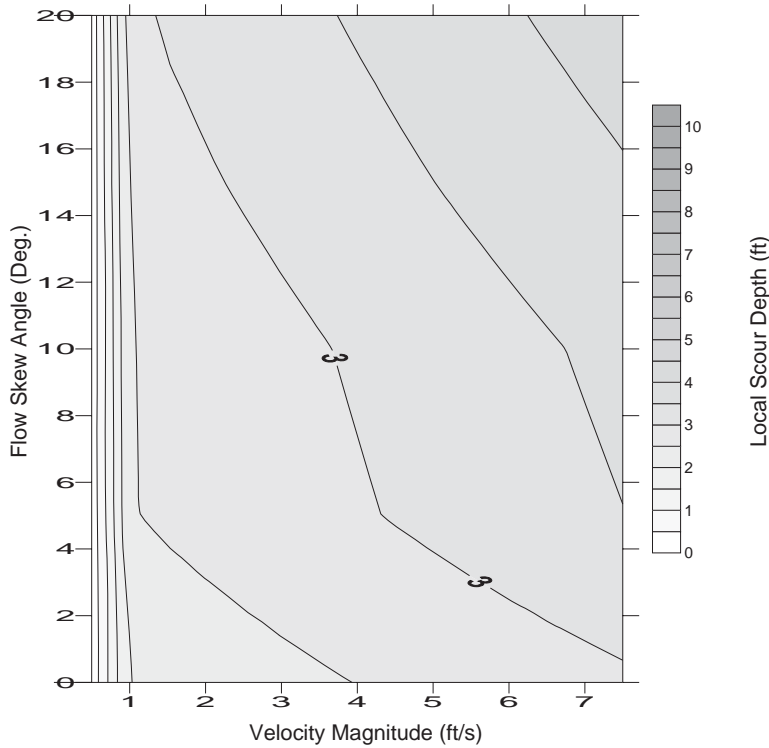


Figure 49 Local Scour Plot for a Group of Four 14' Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

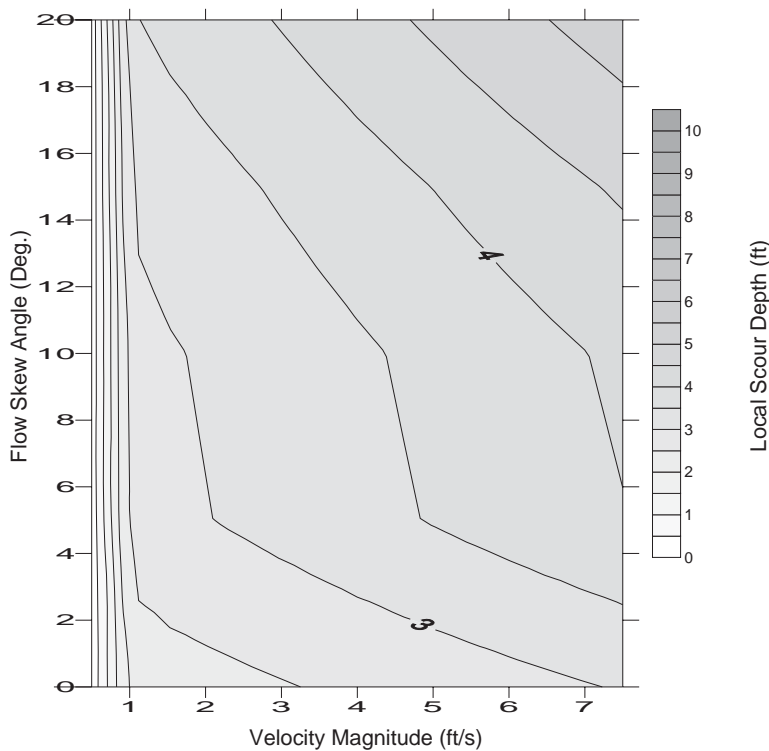
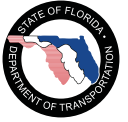


Figure 50 Local Scour Plot for a Group of Six 14' Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

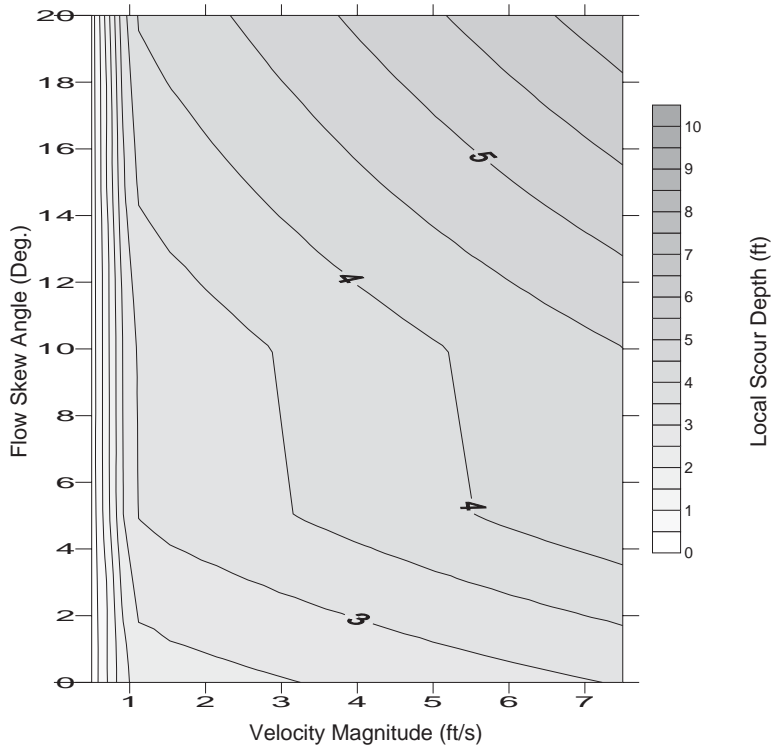


Figure 51 Local Scour Plot for a Group of Eight 14' Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

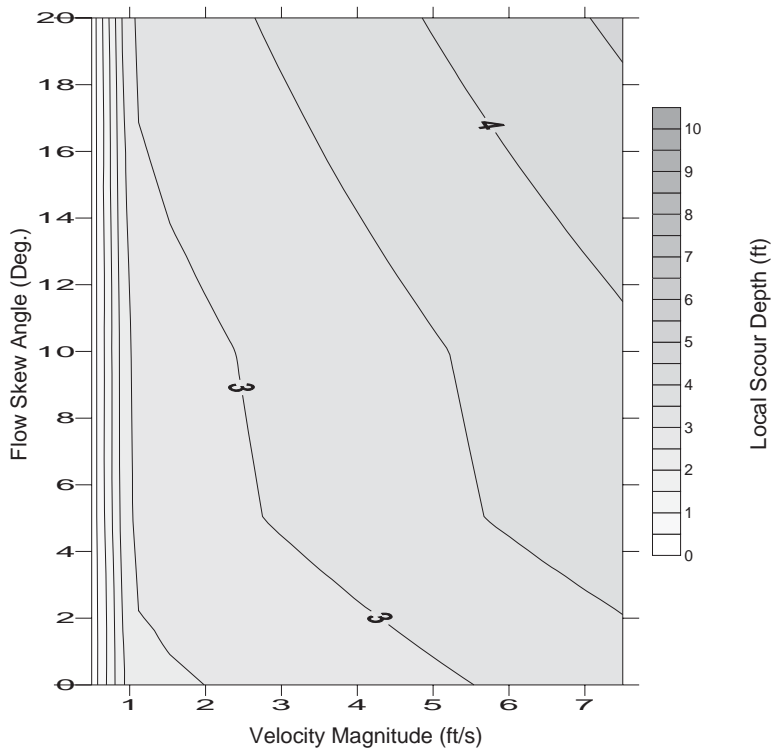
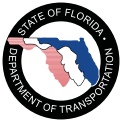


Figure 52 Local Scour Plot for a Group of Four 16' Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

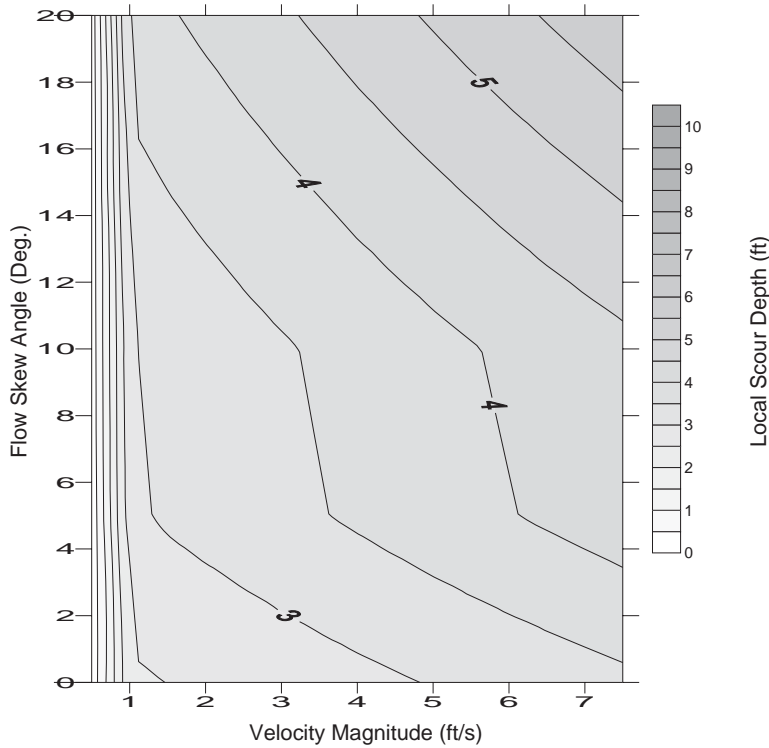


Figure 53 Local Scour Plot for a Group of Six 16' Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

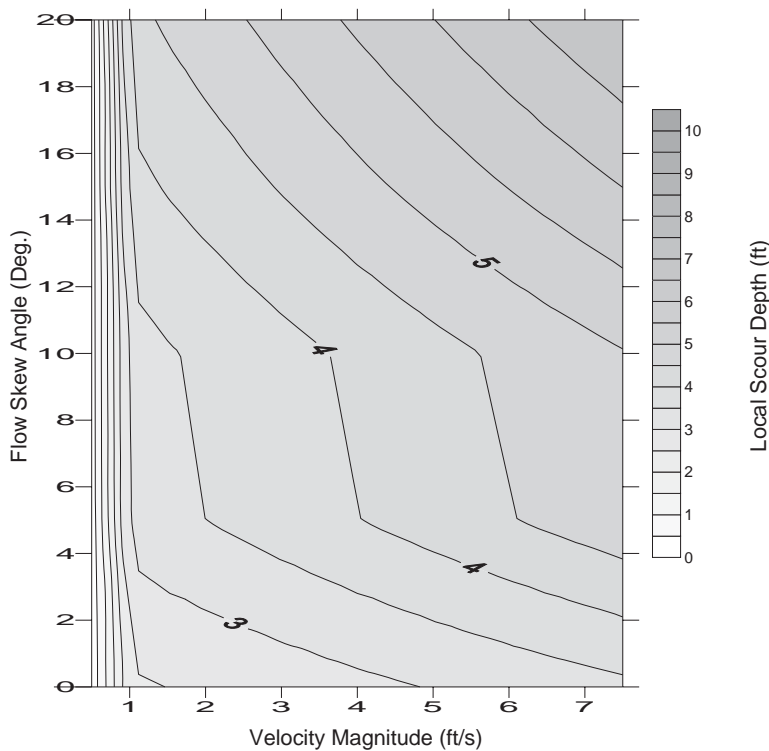
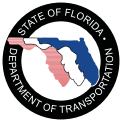


Figure 54 Local Scour Plot for a Group of Eight 16' Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

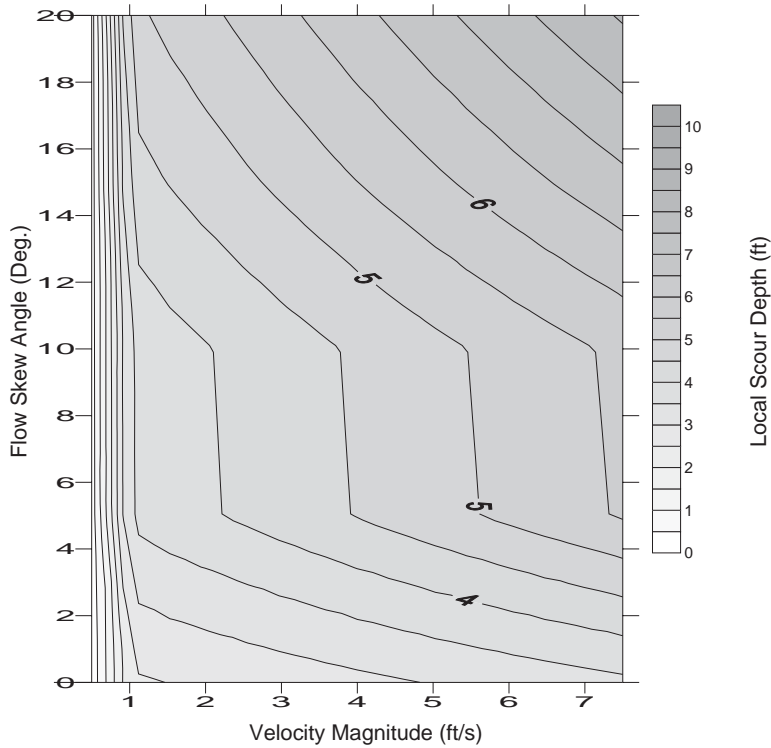


Figure 55 Local Scour Plot for a Group of Ten 16" Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

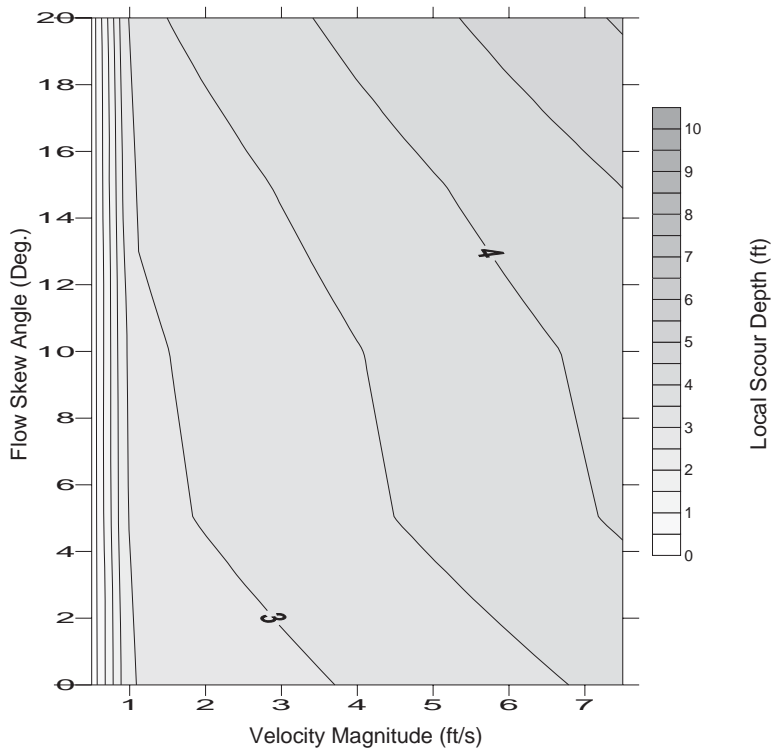
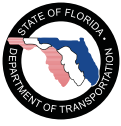


Figure 56 Local Scour Plot for a Group of Four 18" Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

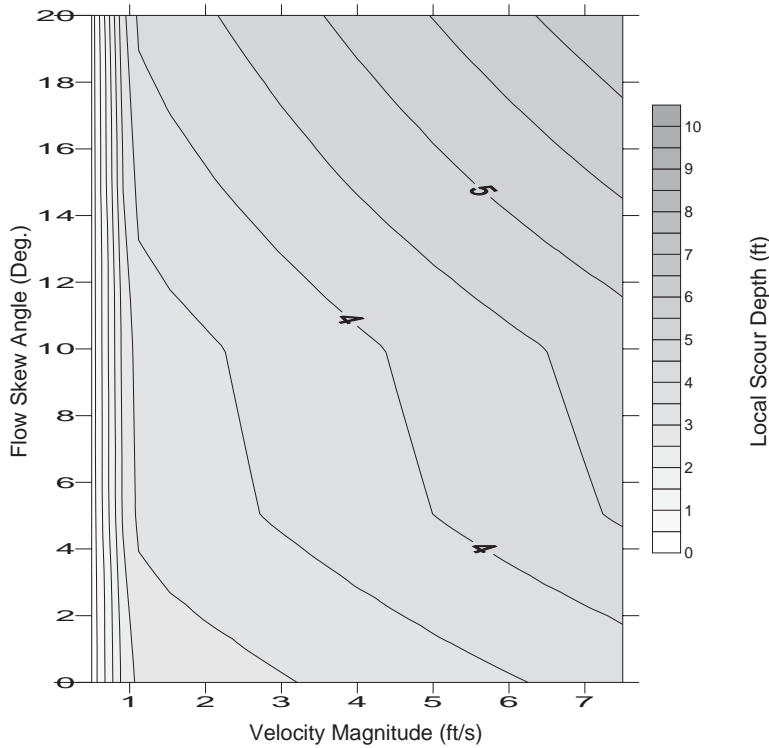


Figure 57 Local Scour Plot for a Group of Six 18'' Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

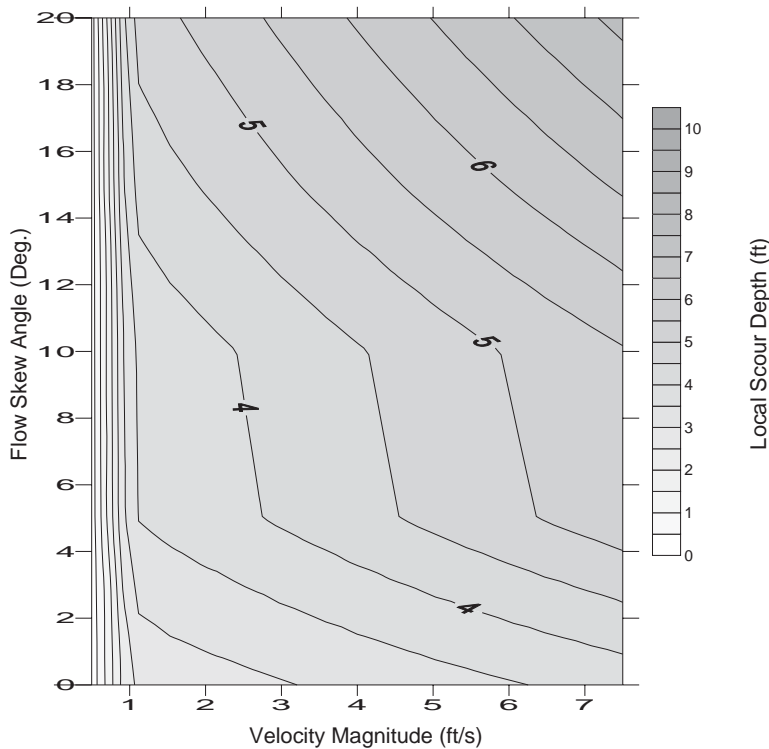
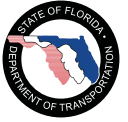


Figure 58 Local Scour Plot for a Group of Eight 18'' Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

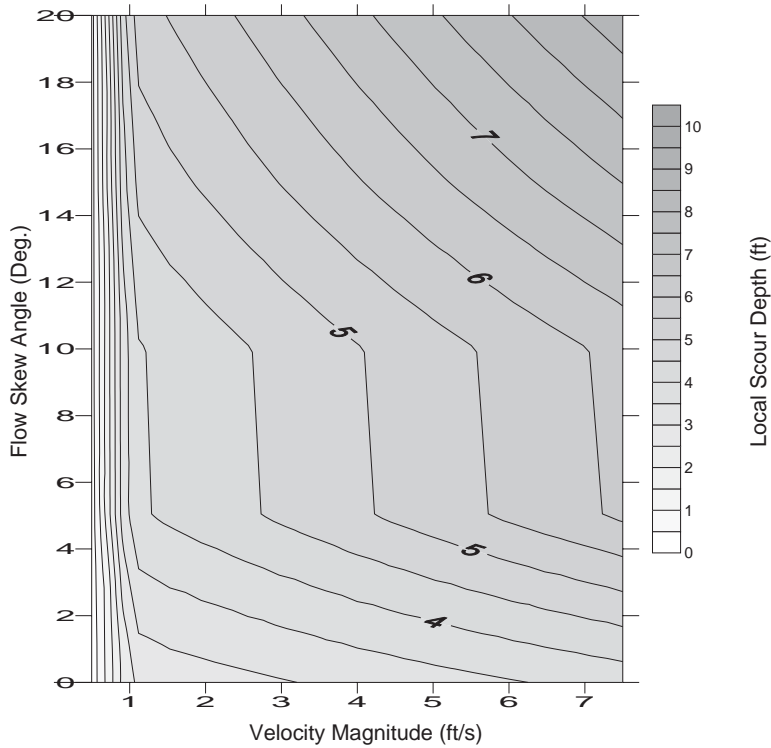


Figure 59 Local Scour Plot for a Group of Ten 18" Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

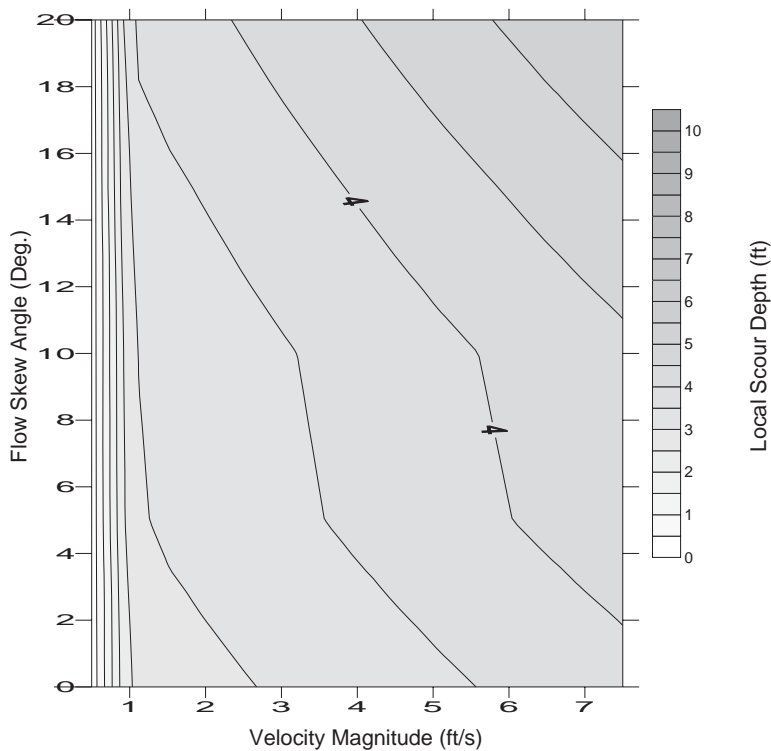
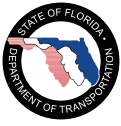


Figure 60 Local Scour Plot for a Group of Four 20" Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

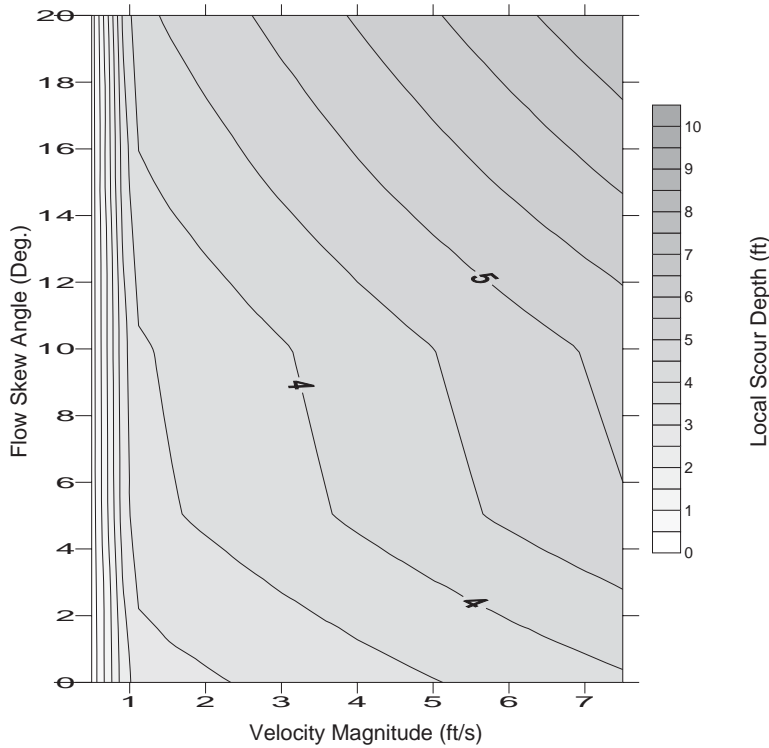


Figure 61 Local Scour Plot for a Group of Six 20' Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

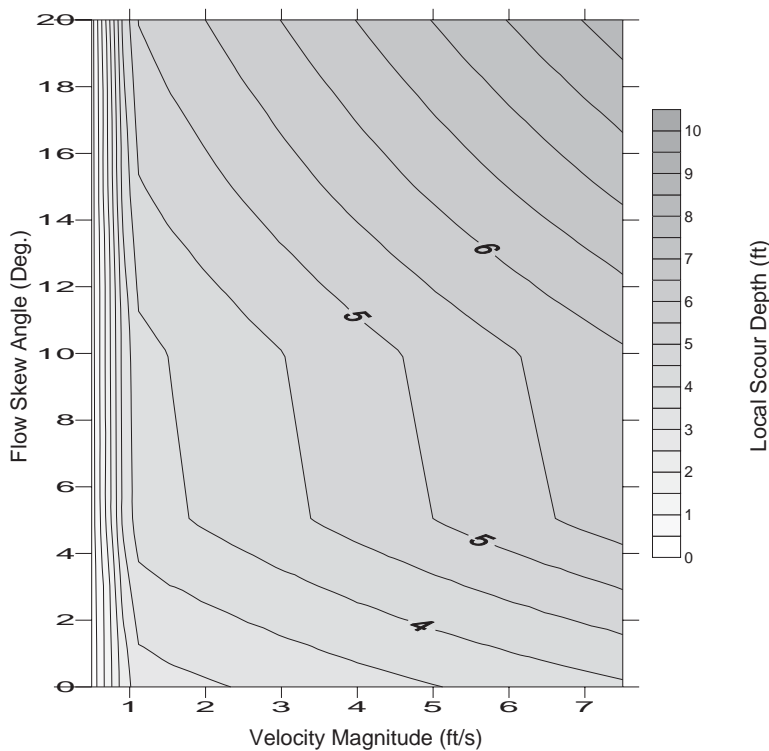
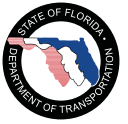


Figure 62 Local Scour Plot for a Group of Eight 20' Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

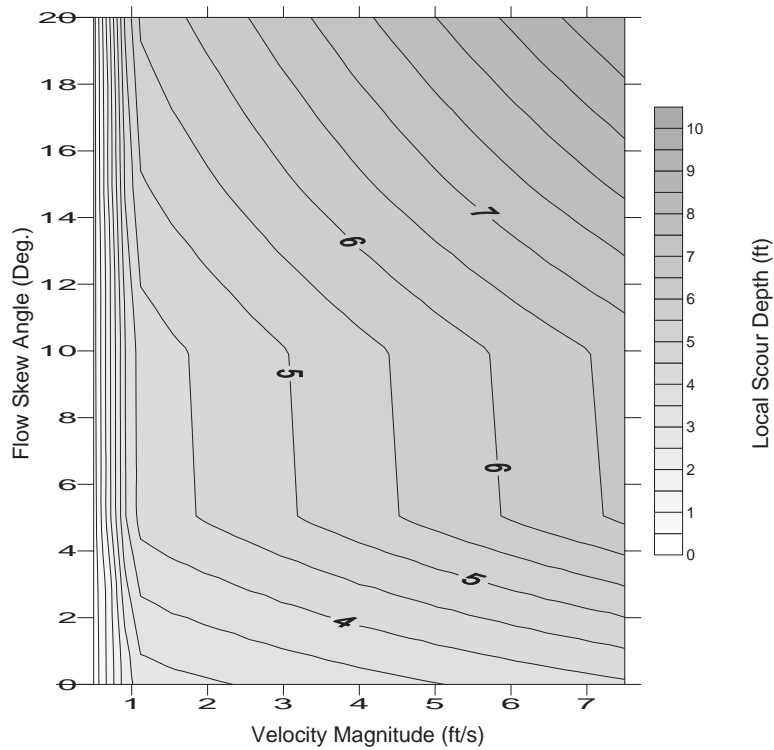


Figure 63 Local Scour Plot for a Group of Ten 20" Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

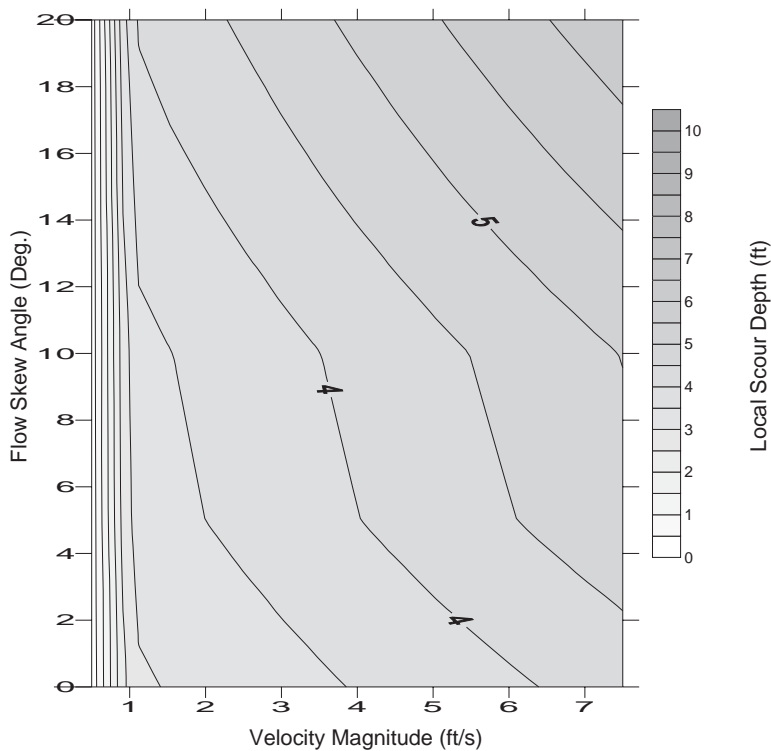
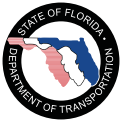


Figure 64 Local Scour Plot for a Group of Four 24" Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

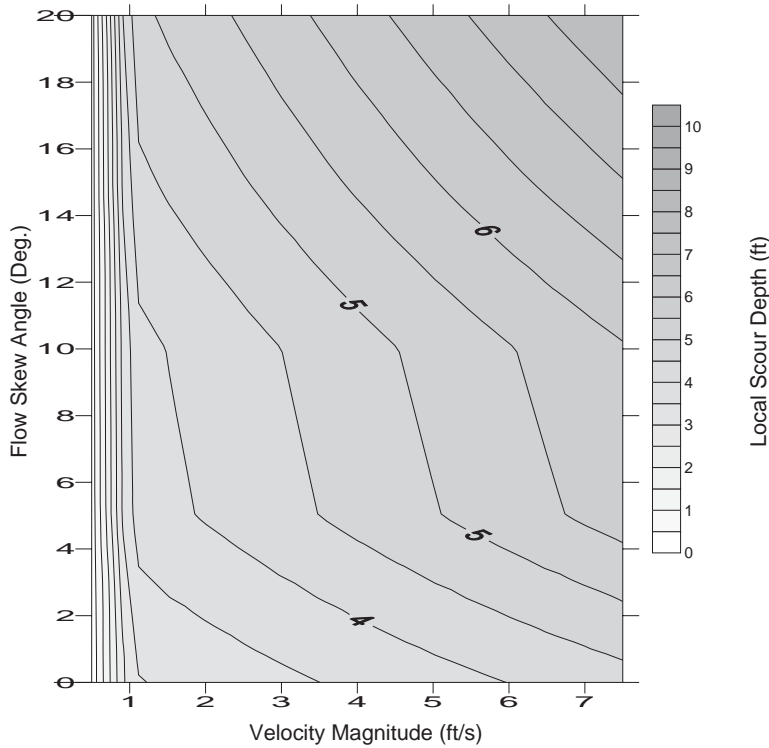


Figure 65 Local Scour Plot for a Group of Six 24" Piles ($D_{50} = 0.30$ mm)

Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

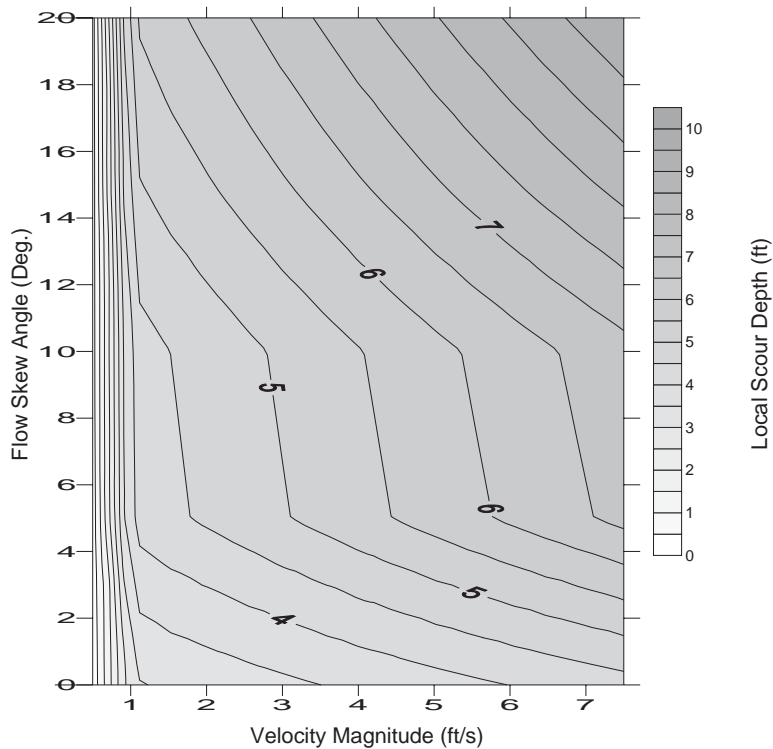
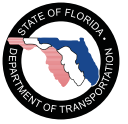


Figure 66 Local Scour Plot for a Group of Eight 24" Piles ($D_{50} = 0.30$ mm)



Local Scour Depth as a Function of Flow Skew Angle and Flow Velocity

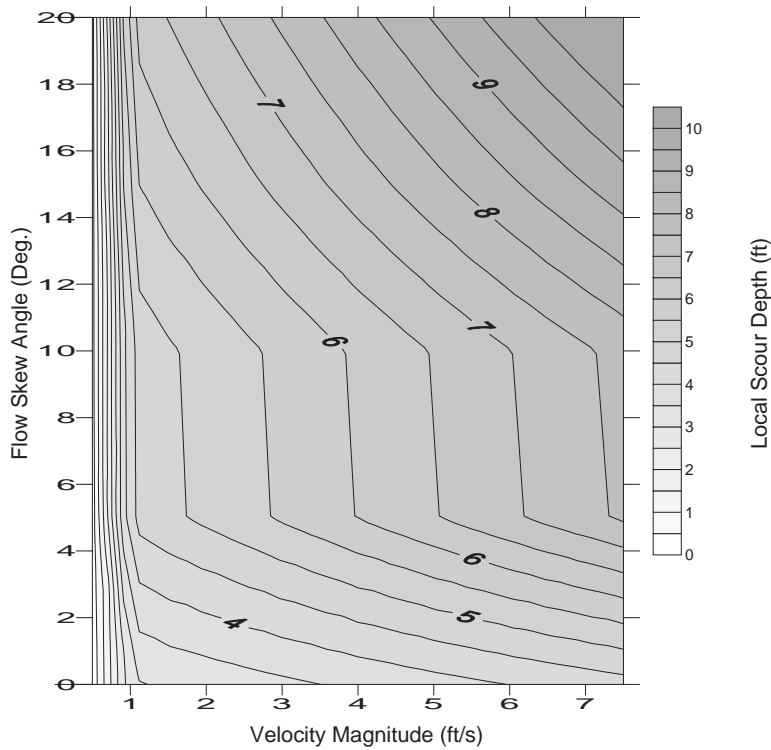


Figure 67 Local Scour Plot for a Group of Ten 24" Piles ($D_{50} = 0.30$ mm)

